AR TARGET SHEET

The following document was too large to scan as one unit, therefore, it has been broken down into sections.

EDMC#:

0061511

SECTION:

2 OF 5

DOCUMENT #:

RPP-13774, Rev 002

TITLE:

SST System Closure Plan

- Specification for Pressure Vessel Design and Fabrication, 24590-WTP-3PS-MV00-TP001 1
- 2 • Seismic Qualification Criteria for Pressure Vessels, 24590-WTP-3PS-MV00-TP002
- 3 • Specification for Pressure Vessel Fatigue Analysis, 24590-WTP-3PS-MV00-TP003

- Piping and Pipe Support Design
- 6 The design code of the WTP piping and pipe supports is ASME B31.3 Code (ASME 1996), as
- well as the DOE seismic requirements. In compliance with DOE seismic requirements (DOE 7
- 8 1996), response spectrum method or UBC (UBC 1997) static method is used for the seismic
- 9 analysis of the piping systems.

10

- 11 Additional information for piping and pipe support design is included in the following 12
 - documents, which are included in DWP Attachment 51 Appendices as indicated:

13

- 14 • Ancillary Equipment Material Selection for Ancillary Equipment Description, 15 24590-WTP-PER-M-02-002 (Appendix 7.9)
- Piping Material Class Description, 24590-WTP-PER-PL-02-001 (Appendix 4) 16
- 17 • Ancillary Equipment Pipe Support Design, 24590-WTP-PER-PS-02-001 (Appendix 7.5)

18

19 The codes and standards that will be followed for design and construction of the piping and 20 supports are identified below:

21

- 22 □ASME B31.3 Code Chemical Plant and Petroleum Refinery Piping (ASME 1996)
- □ASME Section III Code—Rules for Construction of Nuclear Facility Components (ASME) 23 24 1995)
- 25 □Code Case N 411 Alternative Damping Values for Response Spectra Analysis of Classes 1, 2, 26 and 3 Piping, ASME Section III Code (ASME 1998)
- 27 ☐ Uniform Building Code (UBC 1997)
- 28 □ASME/ANSI B16.5 - Pipe Flanges and Flanged Fittings (ASME 1999)
- 29 □DOE-STD-1020-94 (DOE 1996)

30

31 Table 4-13 summarizes the seismic-categories and design standards for piping and pipe supports.

32 33

- 4.2.2.1.2 Physical Information for Tanks
- 34 Tables 4-3 through Table 4-6 list current tank design information (capacity, materials of 35 construction, and dimensions). The tank systems are grouped by plant and process system.

36

- 37 Tank operation is generally automated. However, operator intervention can be used when
- 38 human decisions or approval are required for initiation and termination of a process operation.
- 39 Descriptions of tank system operation for major WTP process systems are identified in 40 sections 4.1 and 4.2.2.

1 4.2.2.2 Ancillary Equipment Requirements [D-2a(1)]

2 Information concerning ancillary equipment is provided in the following subsections.

4.2.2.2.1 Transfer or Pressure Control Devices

Several fluid transfer devices will be used in the WTP. These devices include: mechanical pumps, reverse flow diverters, and steam ejectors. Breakpots and seal pots, although not fluid transfer devices, are an important component of vessel operations. These components are discussed in the following sections.

Mechanical Pumps

Mechanical pumps will be used for operations that require high-flow pumps (such as through the evaporator circuits) or high-pressure head pumps (such as for pumping a waste stream through ultrafiltration circuits). Mechanical pumps will be located in process cells, process rooms, or caves. In general, mechanical pumps will be repaired in place, or removed to a maintenance area. However, remotely maintained pumps will be used in areas where maintenance activities would result in a significant radiation dose to the operators.

For normal process operating sequences, mechanical pumps and associated valves will be controlled by the process control system. In systems where off-normal conditions would require pump shutdown, the design will include an alarm mechanism which that will also trip the transfer device. The pump system is designed to allow for the drainage of liquid from the pump, and for the introduction of flush liquids at the end of transfers to reduce residual contamination.

Reverse Flow Diverters

Reverse flow diverters will provide for the maintenance-free pulsed or metered transfer of liquids or slurries throughout the treatment process. A reverse flow diverter does not need to be fully submerged in order to remove the contents of a vessel, and it maintains a small and predictable volume of tank contents following its use. Operation of the reverse flow diverter is cyclical, following timed phases: suction phase, drive phase, and blowdown. Figure 4A-120 and The following paragraphs and figures in Attachment 51 describe and illustrate a typical reverse flow diverter system arrangement. Figure 4A-121 illustrates a typical flow diverter.

<u>Suction phase</u>: In the suction phase, the secondary automatic valve A is open, admitting air to the suction jet pump. Valve B is shut and liquid is drawn from the supply tank through the reverse flow diverter and into the charge vessel. The suction ejector is designed so that it cannot produce a vacuum capable of lifting liquid higher than a certain valve known as the "suction lift". After a short time, the liquid reaches this "suction lift" height and stops, then valve A is shut.

<u>Drive phase:</u> When valve A is shut, valve B is opened, admitting air to the drive nozzle. Air passes through the nozzle and pressurizes the charge vessel. Liquid is forced across the reverse flow diverter and into the delivery pipe. The delivery pipe is quickly filled with liquid that flows into the delivery vessel.

<u>Blowdown phase</u>: When the charge vessel is nearly empty, valve B is shut; no air is supplied to either jet pump. The compressed air in the charge vessel passes back through the paired jet pumps, down the vent pipe, and into vessel vent system.

Shortly after blowdown begins, the pressure in the charge vessel falls below the delivery head, and the flow of liquid into the delivery vessel is halted. The liquid in the delivery vessel then falls back down the pipe, across the reverse flow diverter, and into the charge vessel. After a short time, the pressure in the charge vessel falls to zero (gauge). The cycle is now complete.

Steam Ejectors

Steam ejectors are used to transfer process liquids, or to reduce the operating pressure of a system by gas removal. They empty liquid from vessels by means of suction lift, using a simple control system. A typical arrangement of a steam ejector-system is shown in Figure 4A-122Attachment 51.

An automated control valve supplies high-pressure steam to the steam ejector. This steam accelerates through a nozzle, creating a differential pressure along a submerged suction leg within the vessel. The pressure than forces the liquid up the suction pipe. This effect is known as *striking*. The steam then conveys the liquid to the destination vessel, normally via a breakpot. Control is established using liquid level instrumentation in the vessel being emptied, and using a temperature indicator, such as a thermocouple, within the breakpot.

Seal Pots

A seal pot is a type of hydraulic seal. A hydraulic seal is used primarily to maintain a separation between vessel vent or off gas offgas systems for feed and receipt vessels. This separation is necessary to prevent migration of airborne contamination between the vessels. Without the seal, airflow could occur due to the different pressures in the vent systems. The seal is a slug of liquid in the interconnecting pipeworkpipe work that remains after each liquid transfer is completed, blocking airflow between vessels.

The seal can be provided by constructing a simple "U" shape in the piping. Different piping arrangements are used for different purposes. A seal pot is a small vessel with one (inlet or outlet) pipe submerged in the liquid slug in the lower part of the pot, while the other pipe terminates in the top of the pot, above the static liquid level. The pot may be provided with a level indicator or alarm, if necessary, to ensure adequate liquid level. Periodic liquid additions may be needed to maintain the seal, especially if the pipeline is infrequently used. Figure 4A-123 illustrates An illustration of a typical seal pot is provided in Attachment 51.

Breakpots

The main function of the breakpot is to reduce the amount of radioactive-mixed waste material entrained into the vessel ventilation system. Breakpots are provided on transfer lines that use steam ejectors for moving radioactive liquors liquids by pressure flow. These types of transfers create the potential for higher containment of radioactive-mixed waste contamination. Breakpots function to convert steam from pressure-flow to liquid gravity flow, thereby reducing both the effluent loading on the downstream vessel ventilation treatment system and the radioactive

mixed waste contamination levels in the vessel vent ductwork. Breakpots also serve a secondary purpose by providing a siphon break for other transfer systems where siphoning could occur. A diagram of a breakpot is shown provided in Figure 4A 124Attachment 51.

Breakpots are typically placed at a high point in the discharge line from the steam ejector. Liquid will be pumped into the breakpot through an inlet nozzle in its wall. The incoming liquid will be directed towards a baffle. Within the baffle, non-condensed steam and gases will disengage. The breakpot will be self-draining; the liquid will drain through the breakpot discharge pipe to the destination vessel.

Above the inlet nozzle(s) will be a packed bed where disentrainment of the gas stream will occur. The exiting gas from the packed section will pass into the vessel ventilation system. The packed bed can be washed periodically using a wash ring permanently installed above the packed bed. Within the packed bed, a thermocouple will be located inside a sheath to measure temperature.

4.2.2.2.2 Bulges

Bulges are intended for systems/to allow hands-on maintenance enof equipment that are not radioactively "hot" after process fluids are flushed from the bulge piping and components to allow hands-on maintenance. Bulges provide shielding to personnel during process operation and allows vulnerable or failure prone components to be located outside the process environment. The cell wall provides shielding between the cell and the bulge interior. The bulge includes shielding and contamination control as needed, depending on the process fluid within the bulge piping. A typical bulge consists of a metal frame attached to the cold-side wall of a process cell; the frame is used to support the piping and components as well as the shielding plates (usually steel), which are bolted to the frame.—A diagram of a typical bulge is shown in Figure 4A-127Attachment 51.

 There are two classifications of bulges used at the WTP. One is a "process" bulge; the other is a "service" bulge. The process bulge contains valves, pumps, piping, etc. The service bulge contains valves used to transfer reagents, steam, etc., to the in-cell process equipment. The design of the two bulges is similar.

Bulges are equipped with several wash systems, facilitating washing both internal and external piping, components, and bulge confinement surfaces. Decontamination of the equipment internals and associated piping is achieved by externally connecting a flushing system located on the outside of the bulge. Wash fluids could be water or more aggressive media such as nitric acid, provided compatibility with the bulge materials is ensured. bulges are internally lined with a stainless steel liner and are equipped with a sump, drain, and sump level instrumentation. The drains are connected to the plant wash-system.

Additional information on process bulges may be found in *Process Bulge Design and Eabrication* (24590-WTP-3PS-MX00-TP001), located in DWP Attachment 51, Appendix 7.7.

4.2.2.2.3 Description of WTP Piping System

- 2 Detailed information on piping is included in Piping Material Class Description
- 3 (24590-WTP-PER-PL-02-001), located in DWP Attachment 51, Appendix 4.

45 Interplant Piping Transfer Lines

Waste feed from the DST system will be transported to the WTP via the waste transfer lines.

7
8 The waste <u>feed</u> transfer lines will be a-double-walled pipe. The inner pipe will be constructed of stainless steel, while the outer pipe will be constructed of carbon steel. The carbon steel outer

- pipe will be coated with a corrosion-resistant material. In addition, the coated outer pipe for the
- waste transfer lines from the DST to the pretreatment plant will be surrounded by insulation and
- 12 a seamless high-density polyethylene outer shell. This extra layer of protective material will
- 13 isolate the waste transfer lines from soil. The waste transfer lines between the pretreatment plant
- and the other WTP process plants will not have this extra barrier from the soil, but will be
- cathodically protected as described later in this section.
- 17 A leak detection system will be provided for the entire length of the waste transfer line.
- Pumping will be terminated, and reception of waste feed from the DST system unit will stop,
- when a leak is sensed identified by the leak detection system.

The inner pipe will be supported by guides, saddles, support keys, or anchors within the outer pipe. The inner pipe will transport waste and maintain the pressure boundary, while the outer pipe will provide secondary containment for the inner pipe. The piping system will be buried

24 under a minimum depth of soil for radiation shielding. The minimum depth of soil will be

finalized at the detail design phase and will be not less than the 2 foot freeze depth. A heat trace system is not required for pipes buried below freeze depth.

27 28

29

16

20

1

- The piping system will have a continuous slope down toward the pretreatment plant. Released liquids resulting from leaks to the outer pipe can be removed as required by
- WAC-173-640(4)(b). The piping system will be designed to allow water flushing to occur in both directions.

32 33

- Liquid Effluent Transfer Lines
- 34 Liquid effluent generated at the WTP will be routed to the pretreatment plant for recycling
- 35 through the WTP or disposal to the LERF and ETF. An effluent line will be routed from the
- 36 pretreatment plant to the LERF and ETF. This line is a buried pipe, constructed of materials that
- are compatible with the waste, under a minimum two feet2 ft of soil serving as freeze protection.
- 38 The pipes will have a continuous downwards slope towards the LERF and ETF, and will be
- designed to maintain structural integrity. A leak detection system will be provided for the
- 40 <u>LERF/ETF waste transfer lines.</u>

- 42 Intraplant Piping
- Within plants, the pipelines associated with the tank system will be single-walled. Secondary
- 44 containment will be provided for piping within the plants by double-walled pipe or <u>partially</u> lined
- process cells, process rooms, or caves. If needed, other containment methods such as a bulge or

concrete ducts with liners will be provided at appropriate locations. The bulge or concrete ducts will be provided with a low point which will drain to process cells, process rooms, or caves. The leak detection equipment located within the process cells, process rooms, and caves will warn of a piping leak through alarms.

Piping between plants and the two outdoor tanks at the pretreatment plant will be double-walled below grade and below the freeze line, similar to the waste transfer line.

Cathodic Protection

An electrically poweredimpressed current cathodic protection system will be used for eliminating or mitigating corrosion on underground tanks and piping. The cathodic protection system will maintain a negative polarized potential within a range of approximately 0.850 milivolts relative to between the protected pipe and a saturated copper/copper sulfate reference electrode. An automatically controlled, impressed current cathodic protection system is used to maintain the negative polarized potential.

The impressed current cathodic protection system uses direct current provided by a rectifier that is powered from the site Pplant's normal 120 volt alternating current or 480 volt Vac power system. The direct current from the rectifier flows to is connected across the buried or submerged impressed current anode wire and the protected pipe. The current then flows from the anode wire, (which is positive, terminal) through the electrolyte, to the eathodeprotected pipe, (which is negative, terminal) completing the electrical circuit.

An annual survey, recommended by <u>NACE International (formerly</u> the National Association of Corrosion Engineers), standards will be performed on the overall system. Additional information on inspections is provided in Chapter 6 of this application. Test stations will be located to in the fieldprovided to facilitate permit testing via potential measurements readings. Additional information on inspections is provided in Chapter 6.

The following waste transfer lines use the are provided with cathodic protection system at the WTP. The waste transfer lines are double encased and constructed of materials that are compatible with the waste:

□Incoming waste feed lines to the pretreatment plant

- Mixed waste transfer lines between the pretreatment plant and the HLW vitrification plant
- Mixed waste transfer lines between the pretreatment plant and the LAW vitrification plant
- Mixed waste transfer line between the analytical laboratory and the pretreatment plant
- The incoming DOE waste feed pipelines that interface with the WTP pipelines are not cathodically protected; therefore, the waste feed lines routed between the DOE interface point and the pretreatment plant (which are similarly configured) are not intentionally cathodically protected. They are, however, bonded at the crossing of the plant service air piping between the pretreatment plant and the HLW vitrification plant on the opposite end (which is adjacent protected piping). The waste feed lines, therefore, may receive small amounts of protective cathodic protection current in the area where they are bonded. This

- area is defined as the "zone of influence". Bonding is required to eliminate stray electrical currents that may occur in the zone of influence and thereby eliminate the possible corrosion process. The waste feed lines are also provided with test stations at both ends to allow potential tests that will indicate if corrosion is a concern.
 - Radioactive/dangerous waste effluent transfer lines to the ETF/LERF

4.2.2.2.4 Description of Foundations

Tank systems containing mixed waste that will be located indoors in process cells or caves, which will be integral parts of the pretreatment plant, analytical laboratory, the LAW vitrification plant, and the HLW vitrification plant with the exception of two outdoor tanks.

Therefore, the design requirements of the tank systems will be met by the structural integrity of the plants. WTP compliance with Uniform Building Code-UBC seismic design requirements, found in DWP Attachment 51, Chapter 4, Supplement 1 Supplement 1, provides the seismic design requirements for the WTP. The outdoor tanks will be located outside of the pretreatment

plant on a protectively-coated concrete pad and concrete berm. The concrete pad for these tanks will be sufficient to support the tanks.

Additional information on the design criteria, load definitions, load combinations, and methodology for the structural design and analysis may be found in *Secondary Containment Design* (24590-WTP-PER-CSA-02-001), located in DWP Attachment 51, Appendix 7.5.

4.2.2.3 Integrity Assessments [D-2a(2)]

This section discusses assessment of the structural design of the tanks and foundation.

A written assessment of the adequacy of the design, and the structural integrity and suitability of tank systems, including ancillary equipment, will be prepared. The assessment will be reviewed and certified by an independent qualified registered professional engineer, consistent with Page II-5 of OSWER Policy Directive #9483.00-3, to attest that the tank systems are adequately designed for managing dangerous waste. The assessment will and miscellaneous treatment systems will be prepared on a system-by-system basis. Separate reports are prepared for tanks, tank system ancillary equipment, and associated secondary containment systems. Each assessment will be reviewed and certified by an independent, qualified, registered professional engineer to attest that the tank and miscellaneous treatment systems are adequately designed for managing dangerous waste. Each assessment will include an evaluation of the foundation, structural support, seams, connections, pressure controls, compatibility of the waste with the materials of construction, and corrosion controls for each mixed waste tank management system, as appropriate. Assessment reports are located in DWP Attachment 51, Appendix 8.11 for the pretreatment plant, Appendix 9.11 for the LAW vitrification plant, and Appendix 10.11 for the HLW vitrification plant. The certification will read as follows:

"I certify under penalty of law that I have personally examined and am familiar with the information submitted in this document and all attachments and that, based on my inquiry of those individuals immediately responsible for obtaining the information, I believe that the

information is true, accurate, and complete. I am-aware that there are significant penalties for submitting false information, including the possibility of fine and imprisonment."

2 3 4

5

The tank systems will be located indoors, except the vessels located outside the pretreatment plant (process condensate vessels, V45028A/B). The two outdoor tanks will be located on a concrete pad with concrete secondary containment.

6 7. 8

Information regarding the Tank-System Design Assessment is included in Appendices 8.10, 9.10, 10.10, 11.10, and 12.10.

9 10 11

4.2.2.4 Additional Requirements for Existing Tanks [D-2a(3)]

12 Tanks and vessels to be permitted in the WTP will be newly constructed; pre-existing tanks will not be used. Therefore, the requirements of this section do not apply. 13

14 15

4.2.2.5 Additional Requirements for New Tanks [D-2a(4)]

Installation of tank systems will be performed in a manner designed to prevent damage to the 16 17

tank system. The WTP will-uses an independent, qualified installation inspector, or an independent qualified registered professional engineer (IQRPE) to perform tank system 18

installation inspections. Inspection activities will include testing tanks for tightness, verifying 19

20 protection of ancillary equipment against physical damage and stress, and evaluating evidence of

corrosion. The inspections will document weld breaks, punctures, coating scrapes, cracks, 21

corrosion, and other structural defects. Installation inspections will conform to 22

23 consensus-recognized standards. Inspection findings and corrective actions, as appropriate, will 24

be documented in a-post-inspection reports. Additional information is provided in Appendices

-25 8.11, 9.11, 10.11, 11.11, and 12.11.

26 27

28

29 30

Additional information describing the installation of tank systems and associated how inspections of tank systems are performed is provided in Installation of Tank Systems,

(24590-WTP-PER-CON-02-001)., located in DWP-Attachment 51, Appendix 8.12. Details on tank system installations for the pretreatment plant, LAW and HLW vitrification plants, and the

analytical laboratory are provided in DWP Attachment 51.

31 32 33

34

35

4.2.2.5.1 Additional Requirements for New On-Ground or Underground Tanks [D-2a(5)]

The majority of the tanks and vessels to be constructed in the WTP will be located within the pretreatment plant, the analytical laboratory, the LAW vitrification plant, and the HLW vitrification plant. Therefore, the requirements of this section do not apply to the indoor tanks.

36 37 38

39

40

41

42

The two outdoor process Process Ceondensate tanks Tanks located at the pretreatment plant (RLD-TK-00006A/B) will be located within a bermed and lined secondary containment system and will not be in direct contact with soil. The design of the outdoor tanks' concrete pad will address backfill, soil saturation, seismic forces, and freeze thaw effects. The ancillary piping for the unit will be in contact with the soil, and the effects of corrosion on the piping will be addressed in the final design.

1 4.2.2.6 Secondary Containment and Release Detection for Tank Systems [D-2b]

- This section provides information about the secondary containment for tank systems that will contain mixed waste in the WTP. Descriptions of equipment and procedures used for detecting and managing releases or spills from tank systems are also provided.
- A number of documents are provided in appendices to DWP Attachment 51 that provide detailed information regarding the design of the secondary containment system. These documents include the following:
- Secondary Containment Design, 24590-WTP-PER-CSA-02-001, located in Appendix 87.5

 Metanicl School of the Parish of the
- Material Selection for Building Secondary Containment/Leak Detection,
 24590-WTP-PER-M-02-001, located in Appendix 87.9

5

23 24

25

26 27

28

29

30 31

- Leak Detection Sump Level Measurement in Secondary Containment Systems,
 24590-WTP-PER-J-02-001, located in Appendix 97.5
- Flooding Volume for PT Facility, 24590-PTF-PER-M-02-005, located in Appendix 8.8
- 16 Sump Data for PT Facility, 24590-PTF-PER-M-02-006, located in Appendix 8.5
- Flooding Volume for 28 Ft Level of PT Facility, 24590-PTF-PER-M-03-001, located in
 Appendix 8.8
- 19 Flooding Volume for LAW Facility, 24590-LAW-PER-M-02-003, located in Appendix 9.8
- 20 LAW Facility Sump Data, 24590-LAW-PER-M-02-001, located in Appendix 9.8
- Flooding Volume for HLW Facility, 24590-HLW-PER-M-02-003, located in Appendix 10.8
- 22 HLW Facility Sump Data, 24590-HLW-PER-M-02-001, located in Appendix 10.5

4.2.2.6.1 Secondary Containment System Requirements [D-2b(1)]

- Most of the tanks systems containing mixed waste will be located within the plants, although two tanks will be located outside the pretreatment plant. Tank systems containing mixed waste that are located within the plants will be arranged within various stainless steel-lined process cells, process rooms, or caves that will act as provided with secondary containment liners or coatings. The outside tanks will be located on a coated, bermed, concrete pad within concrete berms that will act as provide secondary containment.
- The secondary containment systems will be designed, installed, and operated to prevent migration of waste or accumulated liquid to soil, groundwater, or surface water. The piping associated with the tank systems will be located in the process cells, process rooms, caves, berms, or bulges. Secondary containment for piping systems will be incorporated into the design.
- The following subsections provide detailed descriptions of typical secondary containment systems that will be used at the WTP.

1 Process Cells

Process cells will be located within process plants. Process cells will typically be constructed of concrete walls to protect plant operators and the environment from radiological exposure and to prevent migration of waste or accumulated liquid to soil, groundwater, or surface water. The process cells will house equipment and pipe work designed to require little or no maintenance for the duration of the WTP. Operator access to the process cells will not be allowed during normal radioactive operations.

The process cells floors and portions of walls will be lined with stainless steelwill be provided with secondary containment as required. The floor will be sloped to a collection sump to allow for collection and removal of accumulated liquid within the sump.

Process Rooms

Process rooms will be located in the LAW vitrification plant and will be very similar to process caves. Access to process rooms will not be allowed during normal radioactive-operations. However, access will be allowed for certain areas within WTP for non-routine operations such as equipment replacement or maintenance. Process rooms will have a stainless-steel liner on the floor and portions of the walls, and/or will be sealed with a protective coating. The LAW melter gallery area will have a protective coating on the concrete floor and wallsbe provided with secondary containment as required. Systems within process rooms that manage mixed waste will have secondary containment (for example, the locally shielded melter and piping).

Caves

Caves will be located within process plants. Caves will typically be constructed with concrete walls thick enough to protect personnel from radiological exposure to mixed waste. Caves will house mechanical handling equipment designed for remote operation and maintenance. They will generally have sealed lead glass viewing windows and closed circuit television to allow observation of the cave operations and for overseeing remote maintenance. The cave floors and portions of the walls will be lined with stainless steelprovided with secondary containment as required. The floor of the cave will be sloped to a collection sump to allow for collection and removal of accumulated liquid within the sump.

Berms

Concrete berms will be used at the LAW facilityplant for the eCondensate eCollection tTank (LVP-TK-00001) and the two outside pretreatmentoutdoor pProcess eCondensate tTanks (RLD-TK-00006A/B) at the pretreatment plant. The berms will be of sufficient structural strength and height to contain the 100 percent-% of the volume of the largest tank plus the amount of precipitation that results from the 24-hour, 25-year storm event. A protective coating will be applied to the concrete pad and a portion of the berms to prevent contaminant penetration into the concrete. The containment system will be designed to allow for the discharge of storm water after visual or other testing.

Sump and Secondary Containment Drain Systems

The sump and secondary containment drain systems for the three process plants and the analytical laboratory are described in the following sections. Systems will monitor and collect

liquids managed in the system. Sumps and secondary containment drains will be provided with a stainless steel liner or equivalent to act as the secondary containment. The sumps within the process areas will provide a low point for each secondary containment. Wash rings may be provided within some process areas for equipment, vessel, and cell washing and decontamination operations. The sumps will serve the following functions:

- Low point containment
- Removal of material by means of sump emptying ejectors or pumps
- Sampling of material by means of sump sampling ejectors

The following sections describe in detail the two-types of sumps used at the WTP and the secondary containment drains. Tables 4-7 through 4-10 summarize WTP sump information by plant.

Dry Type I Sumps

Mechanical process areas dealing with mechanical handling operations and containing dry material will be provided with Type I sumps. The sump and stainless steel lining will provide secondary containment for areas managing mixed waste. In addition, some LAW vitrification plant process rooms will be equipped with Type I sumps. The sump will provide a low point collection for the infrequent washing of machinery or the cave floor, for general cleanliness or decontamination prior to maintenance or deactivation. In some caves, these sumps will also collect leakage from effluent system transfer pipes associated with or passing through the cave. Type I sumps are generally fitted with a leak detection device with alarm. Their contents are removed using mechanical or fluidic pumps. A diagrammatic representation of this sump type is shown in Figure 4A-125. Dry sumps are part of the secondary containment system provided for tank systems and wet miscellaneous treatment systems. Sumps are located at a low point in the secondary containment systems, and are equipped with leak detection instrumentation and corresponding alarm. Mechanical or fluidic pumps are used to remove liquid that may accumulate in the sump. Details of each sump are included in the sump data documents identified at the beginning of section 4.2.2.6.

Type II Sumps

These sumps will serve as the low point collection system for the stainless steel containment in a cell or mechanical cave where tank systems are present. The sump and stainless steel lining will provide secondary containment for the tanks and piping containing mixed waste. Type II sumps will be provided with a level detection and alarm device and a washout and emptying pump. Type II sumps are generally associated with a high radiation cell environment containing treatment tanks and piping. They are provided with maintenance-free fluidic emptying systems, such as ejectors or reverse flow diverters. These are wet sumps in which water will always be present to provide liquid-level detection via a pneumacator and trigger high and low-level alarms, if necessary. A diagrammatic representation of a cell sump is shown in Figure 4A 126.

It should be noted that a number of process pipe transfer duct drains will provide drainage back to a suitable cell or Type II sump. Waste pipes will be routed to various destinations within the plant. Some of these routes will require the use of concrete ducts, to provide radiation shielding and secondary containment coverage for the piping. The transfer ducts will be provided with stainless steel lining that drains to a low point within the duct, which will be drained to a suitable cell or wet mechanical sump to provide leak detection and sampling access. The transfer ducts will be provided with wash systems for area cleanup in the event of a pipe leak.

Secondary Containment Drains

Many of the bulges and some process rooms areas will have secondary containment drains with remotely-removable plugs. This type of liquid collection system will be located in a low spot in the cell formed by the sloping floor. Liquid detection instrumentation will be present on the top of a remotely removable plug. After the plug is removed, liquid collected will gravity-drain to a collection vessel with a tank level indicator. The liquid managed could be waste released from a tank system, including ancillary equipment, or water used to wash the exterior of tanks or the walls of the room. Liquid managed in the sump system could also be infrequently generated from the wash down of cell walls or tank exteriors.

Design Requirements

 The process cells, process rooms, or caves with mixed waste vessel or Tank systems and wet miscellaneous treatment systems will be partially lined with stainless steel, which will cover the floor and extend up the sides of the process cell or cave to a heightprovided with secondary containment that can contain 100 percent % of the volume from the largest tank within the process cell or cavecontainment area. Fire suppression water is included as appropriate in determining the height of the secondary containment. The height of the liners will not take into account fire suppression material, as the tanks will not manage ignitable waste. The concrete surfaces of the ceiling and the wall above the liner will be covered with a coating that is compatible with the waste feed to provide a splash shield zone. A scalant, compatible with the liner and the waste feed and wall coating, will be used to scal the liner to wall interface.

Table 4-11 presents summarizes the calculated minimum liner height at the four process plants. Calculations for the liner size necessary in each cell and cave are available upon request The flooding volume documents identified above present the secondary containment height for each facility plant.

 A concrete berm with protective coating will be used for the pretreatment plant outdoor tanks. This secondary containment area will be capable of holding 100 percent-% of the volume from the largest tank within the berm, plus the precipitation from a 25-year, 24-hour rainfall event, as required under WAC 173-303-640(4)(e)(i)(B).

The WTP uses consensus-recognized standards to ensure that the process cells, process rooms, eaves, or berms provide secondary containment with systems have sufficient strength, thickness, and compatibility with waste. The design includes an engineered structural base to protect the cells, caves, berms and tank systems against failure resulting both from excess force applied

during catastrophic events or settlement, and from the stress of daily operation. In the event of a spill or release, the <u>structural and foundationsecondary containment</u> design for tank and process cells, process rooms, caves and berms will prevent released mixed waste from reaching the environment, and will safely contain the waste until it can be transferred to an appropriate collection tank.

4.2.2.6.2 Management of Release or Spill to Sump and Secondary Containment Drain Systems [D-2b(1)]

Sumps collect vessel leakage, vessel overflow, and decontamination solutions used in cell and equipment wash down. The sump and cladding are provided to satisfy secondary containment requirements for vessels and piping containing liquid mixed waste. The WTP uses two-types of sumps for different process conditions. If a cell has a personnel entrance and houses vessels, tanks, and piping that manage dangerous waste, a Type I, single lined sump is placed in the cell. If the cell is a non-accessible process cell and has welded piping, a Type II sump is utilized. In Type II sumps, water is always present, to ensure that sump level indicators are working. Additionally, water provides a ventilation seal that prevents airflow from entering vessel overflow piping when a vessel overflows to a sumpa dry sump as part of the secondary containment and leak detection systems. Wash rings allow for sump wash down.

 Sumps have three level thresholds: high operational control; high level alarm; and cell high high level alarm. When these level thresholds are reached, the process control systemare instrumented to informs the operator to investigate the cause of the rising liquid level. The cell liners Secondary containment systems are sloped to direct flow of leaks, or spills, or liner wash solutions to the sump. Process cell liners are made of stainless steel or equivalent material that satisfies regulatory requirements, and design life requirements. To remove liquid from the sumps in a timely fashion, sumps will be equipped with steam ejectors mechanical or fluidic pumps.

If a Type II sump is used, a small amount of water will be maintained in the sump during normal operating conditions. During normal operation, the water level will be maintained between the low and high operational controls. The operation control band limits will be set as close to each other as possible, and the alarm will be set above the high operational control to detect unusual level rises. The sump level will be constantly monitored. Typically, a moderate leak will generate a larger liquid volume than the amount of liquid that might be lost due to evaporation.

Abnormal rising of the liquid level in the sump will be investigated to determine its cause. In all cases, the cause for material in the sump will be determined. Mixed waste released from the primary system and collected in the sumps will be removed within 24 hours, or in as timely a manner as possible. If the released material cannot be removed within 24 hours, Ecology will be notified. After the sump content has been removed, the sump surfaces will be decontaminated using a wash-down system. Based on best management practices, a water flushing volume of approximately six sump volumes will be used to remove residual process water.

If a Type I sump is used, it will be equipped with a moisture probe to detect leakage. If liquid is 1 detected in the Type I sump, similar procedures as described above for Type II sumps will be 2 3 used to remove the content and decontaminate the sump surfaces.

4 5

If liquid is detected in the secondary containment drain, similar procedures to those described above for Type II sump will be used to remove drain contents and decontaminate drain surfaces.

6 7 8

4.2.2.6.3 Additional Requirements for Secondary Containment [D-2b(2)]

9 These requirements pertain to tanks in vault systems and double-walled tanks, which will not be used at the WTP. These requirements are not applicable at the WTP. 10

11

Ancillary equipment such as piping is addressed within Section 4.2.2. Other types of ancillary 12 13 equipment such as pumps, seal pots, and reverse flow diverters, are either located in 14 stainless steel lined process rooms/cells or caves or are designed to provide their ownprovided with secondary containment. Inspection of ancillary equipment is addressed in Chapter 6. 15

16 17

4.2.2.7 Variances from Secondary Containment Requirements [D-2b(2)(c)]

No variances from secondary containment requirements are sought for the WTP tank systems. 18 19 Tank systems will be provided with secondary containment in the form of partially steel lined or

20 protectively coated process cells or rooms, caves and berms, as as identified in the flooding

21 volume documents described in the previous sections.

22 23

4.2.2.8 Tank Management Practices [D-2d]

The following provides the basic philosophy for the WTP vessel overflow systems. Three types 24 25 of barriers exist to prevent overfill of process equipment: preventive controls, detectors, and regulators. Preventive controls promote controlled filling within normal process ranges.

26 27 Detectors recognize if a vessel is being overfilled and alert an operator. Lastly, if preventive

28 controls and detectors fail to stop overfill from occurring, regulators trip a control sequence that 29

stops inflow and/or initiates outflow. The principle principal design concept to control vessel

overflow is to prevent an overflow from occurring. The engineering design will minimize the 30 31 likelihood of tank, ancillary equipment, and containment system overflows, and

over-pressurization, ruptures, leaks, corrosion, and other failures.

32 33 34

35

36

37

38

In general, overflows will be prevented by inventory control in conjunction with level monitoring. The fluid levels in a vessel will be maintained within low- and high-level ranges. Appropriate alarm settings will be used to note deviations from the designed settings. Automatic trip action will be designed to shut down feed to the vessel when the high-level settings are exceeded. These automatic trip actions will be provided for vessels with the potential for high operational and environmental impact in case of an accident or release.

39 40

Most of the WTP tank systems will be designed to incorporate minimal or zero maintenance 41 42 requirements and will be based on a design life of approximately 40 years. Intrusively, The 43 design emphasis of zero maintenance will minimize the likelihood of spills and overflows in the 44 tank systems. In the event that the process controls fail to prohibit vessel overfilling, engineered

overflows will be provided to prevent liquid from entering the vessel ventilation systems. 1

2 Non-pressure-Vessels that are (nominally operating at atmospheric pressure) will have a suitable

gravity or engineered overflow system, unless an overflow can be shown not to be possible.

Vessels or systems that normally operate at above atmospheric pressures will not be provided 4

5 with overflows.

б

3

The following principles apply when designing an engineered overflow system:

7 8 9

- The overflow system for vessels must be instantaneously and continuously available for use.
- Overflowed process streams must be returned to the waste treatment process. 10
- 11 Overflow systems must meet the requirements of the WAC 173-303, Dangerous Waste Regulations, Section 640, Tank Ssystems. In meeting these requirements, overflowing direct 12 to the cell floor will only be considered as the last overflow in a cascaded system. Where an 13 14 overflow is from a vessel to the cell, the overflow system will maintain segregation of the 15 cell and vessel ventilation systems. The compatibility of the overflowing liquid and the 16 recipient vessel will be considered.
- 17 A vessel overflow line is sized to handle the maximum inflow to the vessel without the liquid 18 level in the overflowing tank reaching an unacceptably high level. No valves or other restrictions are permitted in the overflow line. This line is also designed to prevent the 19 buildup of material that could cause blockages. 20
- 21 The overflow receiver is sufficiently sized to contain the overflow.
- 22 Inspections will be performed on the various tank and overflow systems, using the example 23 schedules described in DWP Chapter 6.

24

26

27

28

29

30

25

4.2.2.9 Labels or Signs [D-2e]

Accessible Tanks (i.e., the Pretreatment plant process condensate vessels, V45028A and V45028B) holdingmanaging mixed or dangerous waste will be labeled according to the requirements of DWP permit conditions DWP III.10.E.5.e, for routinely non-accessible tanks, and DWP III.10.E.5.f, for tanks not addressed in DWP III.10.E.5.e. will be labeled provided with stainless steel engraved nameplates. They will inform employees and emergency personnel of the types of waste present, warn of the identified risks, and provide other pertinent information.

31 32 33

4.2.2.10 Air Emissions [D-2f] and [D-8]

This section describes air emissions from vessel ventilation systems and reverse flow diverter 34 exhausts. Organic emissions from vents associated with evaporator or distillation units are also 35 36 discussed.

37 38

4.2.2.10.1 Tank System Emissions [D-2f]

Most of the tanks will be connected to a vessel ventilation system to collect vapors. Vessel vents 39 will be located on major tanks, breakpots, and other small vessels. Exhaust from reverse flow 40 41 diverters and pulse jet mixers will also be collected.

4.2.2.10.2 Process Vents [D-8a]

- 2 The air emission regulations, specified under WAC 173-303-690 and 40 CFR Part-264
- Subpart AA, apply to process vents associated with distillation, fractionation, thin-film 3
- 4 evaporation, and air or steam stripping operations that manage mixed waste with total organic
- 5 carbon concentrations of at least 10 parts per million by weight. The WTP does not use these
- regulated processes; therefore, this regulation does not apply to the WTP. 6

7 8

1

4.2.2.10.3 **Equipment Leaks [D-8b]**

- 9 Regulations provided in WAC 173-303-691 and 40 CFR Part-264 Subpart BB contain the "Air
- 10 Emission Standards for Equipment Leaks". These air emission standards do not apply to the
- WTP because waste feed entering the WTP contains less than 10 percent % total organic carbon 11
- 12 by weight and is excluded under 40 CFR 264.1050(b).

13 14

4.2.2.10.4 Tanks and Containers [D-8c]

- 15 The regulations specified under WAC 173-303-692 and 40 CFR Part 264 Subpart CC do not
- 16 apply to the WTP mixed waste tank systems and containers. These tanks and containers qualify
- 17 as waste management units that are "used solely for the management of radioactive dangerous
- 18 waste in accordance with applicable regulations under the authority of the Atomic Energy Act
- 19 and the Nuclear Waste Policy Act" and are excluded under 40 CFR 264.1080(b)(6). Containers
- 20 bearing nonradioactive, dangerous waste, such as maintenance and laboratory waste, that is not
- 21 excluded under 40 CFR 264.1080 (b)(2) or 40 CFR 264.1080(b)(8), will comply with the tank
- 22 and container standards specified under 40 CFR Part 264 Subpart CC.

23 24

25

4.2.2.11 Management of Ignitable, Reactive and Incompatible Waste in Tanks [D-2g] and [D-2h]

- 26 Mixed waste from the DST system unit will initially be designated as both ignitable (D001) and
- 27 reactive (D003). The D001 and D003 waste numbers will be as described in the waste analysis
- 28 plan in DWP Attachment 51, Chapter 3, Appendix 3A. The vessels will be located in a manner
- that meets the National Fire Protection Association (NFPA) buffer zone requirements for vessels, 29
- 30 as contained in Tables 2-1 through 2-6 of the NFPA-30 Flammable and Combustible Liquids
- 31 Code (NFPA 1981). The vessels will be designed to store the waste in such a way that it will be
- 32 protected from materials or conditions that could cause the contents to ignite or react. Vessel
- contents will be constantly mixed and will be actively vented to process stacks, which will be 33
- equipped with vapor collection and treatment systems that will manage emissions. Further 34
- 35 information on waste numbers is contained in DWP Attachment 51, Chapter 3, Appendix 3A.

36

- 37 Ignitable or reactive waste may be generated from laboratory or maintenance activities. This
- 38 waste will be accumulated and managed in compliance with regulatory requirements, in
- 39 approved containers. Potentially incompatible waste generated from laboratory or maintenance
- 40 activities will not be stored in the tank systems.

- 1 A potential for incompatibility may exist, for example when nitric acid is used to elute waste
- 2 components from ion-exchange column resins that were previously regenerated with sodium
- 3 hydroxide. To minimize a reaction, water flushes will be performed between batches.

6

7

Process reagents that could react with waste in the tank systems will be stored in areas that are separated by physical barriers from process tanks. Potentially incompatible wastes generated from laboratory or maintenance activities will not be stored in proximity to each other in the tank

8 systems.

9 10

11

4.2.3 LAW and HLW Miscellaneous Unit Treatment Sub-Systems [WAC 173-303-680 and WAC 173-303-806(4)(i)]

- 12 This section describes LAW and HLW melter operations conducted at the WTP. The thermal
- 13 treatment miscellaneous units will be melters and will be used to immobilize dangerous and
- 14 radioactive waste constituents by vitrification. There will be three miscellaneous units in the
- 15 LAW vitrification plant (LAW-melters 1, 2, and 3) and one miscellaneous unit in the
- 16 FILW vitrification plant (HLW melter).
- 17 The LAW vitrification system and HLW vitrification system consist of the vitrification melters,
- 18 offgas treatment equipment, and associated equipment. The melters immobilize mixed waste in
- 19 a glass matrix. The LAW vitrification systems and the HLW vitrification system contain two
- 20 <u>melters each. The following sections provide additional information on the vitrification systems.</u>

21

22 Other miscellaneous treatment sub-systems, and their associated process control features, are described in section 4.2.2.

24 25

4.2.3.1 Melter Capacity and Production

- For the LAW melters, throughput is defined on the basis of quantity of glass waste produced. In
- turn, the quantity of glass waste produced depends on the degree to which the LAW-feed can be incorporated into the glass waste matrix. The maximum design throughput of the LAW melter
- 29 Melter systems will be approximately 15 metric tons per day of glass waste for each melter and
- 30 approximately 45-30 metric tons per day as maximum possible throughput for the LAW
- 31 vitrification plant. The maximum operating production rate of the HLW melters Melters is
- 32 approximately 3 metric tons per day for each melter and approximately melter 1.56 metric tons

33 per day throughput.

34 35

41

4.2.3.2 Description of Melter Units [WAC 173-303-806(4)(i)(i)]

- 36 The LAW melter systems are located in a the melter galleriesy and the HLW mMelters is
- 37 are housed within a the melter caves as shown depicted in the general layout arrangement plan
- 38 and section permit drawings, which are found in <u>DWP Attachment 51</u>, Appendix 9.4 for the
- 39 <u>LAW vitrification plant and Appendix 10.4 for the HLW vitrification plantAppendix 4A.</u> The

40 following subsections provide detailed descriptions of the melter units.

- 42 Low-Activity Waste Melter Units
- 43 Figure 4A-48 provides a sketch of an LAW Melter. The Each LAW melter Melter
- 44 (LMP-MLTR-00001/2) is a rectangular furnace, lined with refractory material, with an outer

- 1 steel casing. An additional outer steel casing with access panels will be provided to enclose the
- LAW melter Melter. This outer steel casing is designed to provide local shielding and 2
- 3 containment. Each LAW Mmelter has a nominal design capacity of approximately 10 to
- 15 metric tons of glass waste per day. Each will have a molten glass surface area of 4
- approximately 108 ft². Each of the three two LAW melters has external dimensions of 5
- 6 approximately $26 \times 19 - 21 \times 16$ ft high, and weighs approximately 450 - 270 metric tons empty-
- 7 and 475-290 metric tons with glass. The operating temperature of the melter is between 950
- 8 1100 °C and 1.2501200 °C.

- 10 The locally shielded LAW melter Melter (LMP-MLTR-00001/2) will be operated and
- maintained in a personnel access area. The melter will be maintained at a lower pressure than 11
- 12 the surrounding room to prevent escape of contaminants. Consumable melter parts will be
- 13 replaced through access panels. The melters will be transported in and out of the gallery on a rail
- 14 system. A transporter will move the melters to and from the LAW vitrification plant.

15

16 The melter refractory package is designed to serve as a mechanical, thermal, and electrical 17 barrier between the molten glass residing in the melter and the melter shell.

18

- 19 The refractory package is housed in a steel shell and provides ultimate containment for the
- 20 molten glass. Active cooling on the exterior of the melter is provided by water jackets. The
- 21 water jackets will be in the intermediate loop of a two-loop system that will transfer heat from
- the LAW melter through heat exchangers to cooling towers. The intermediate loop 22
- 23 containing the water jacket will be a closed system that isolates the water circulating through the
- 24 water jacket from the water in the cooling water loop circulating to the cooling tower.
- 25 Radioactive-Mixed waste material leaking into the intermediate loop cooling water will be
- 26 prevented from becoming an inadvertent discharge via the cooling tower. The refractory
- package will provide adequate containment if there is a temporary loss of cooling. Penetrations 27
- in the melter system are sealed using appropriate gaskets and flanges. This system is designed 28
- 29 for plenum temperatures of up to 1,100 °C. The LAW melter lid is composed of steel and 30 refractory material layers.

31

- 32 Each LAW melter (LMP-MLTR-00001/2) will use two independent discharge chambers.
- 33 An air lift pumps molten glass from the bottom of the melter pool, through a riser, into a
- 34 discharge chamber, and poureds it into an ILAW container. The ILAW is then allowed to cool, 35
 - forming a highly durable borosilicate glass waste form within the container.

36

- 37 Waste Spent LAW mMelters will initially be managed within the LAW locally shielded melter 38 gallery containment building unit. Waste-Spent LAW Mmelters will be removed from the melter
- 39 gallery and transported using a bogie transport and rail system. If necessary, the melter exterior
- 40. surfaces will be decontaminated. The waste melters will be stored at the melter storage area 1 or
- 41 2-prior to disposal at prior to transfer to a Hanford Site TSD unit.

- 43 High-Level Waste Melter Units
- Figure 4A-54 provides a sketch of an HLW Melter. The Each HLW melter Melter 44
- (HMP-MLTR-00001/2) is a rectangular furnace, lined with refractory material, with an-outer 45

steel-casings. It has They have four compartments: a glass tank, two discharge chambers, and a plenum just above the glass tank. The tanks is are lined with refractory material designed to withstand corrosion by molten glass.

1 2

The HLW melter systems consists of one-two melters with the capability for a second melter. Each HLW mMelter (HMP-MLTR-00001/2) is designed for glass production rates up to 3 metric tons per day (MTG/d). The HLW melter system has a nominal design capacity of 1.5 metric tons of glass waste per day and a maximum capacity of three metric tons per day. The operating temperature of the melter is between 950 °C and 1,250 °C. The HLW melters Melters haves a molten glass surface area of approximately 40 ft². The HLW mMelters haves external dimensions of approximately $12 \times 15 \times 12$ ft 11 ft Hhigh \times 14 ft² Ddeep \times 14² ft Wwide. The glass contained in a full HLW melter has a volume of approximately 145 ft³ and weighs approximately 9.1 metric tons. The An entire melter, including the supporting structure and transport mechanism, weighs approximately 90 metric tons empty, and approximately 99 metric tons full.

The HLW melters (HMP-MLTR-00001/2) haves been designed to be remotely operated and maintained. Remote maintenance will be performed by a power manipulator, overhead crane, and auxiliary hoist, or by through-wall master-slave manipulators. The melter will be positioned within the HLW vitrification plant for ease of access and viewing of both discharge chambers during operations, and for viewing access to the melter lid to facilitate removal and replacement of subcomponents, if needed. A rail and bogie transport system will facilitate remote removal and replacement of the entire melter structure.

 The HLW melters (HMP-MLTR-00001/2) will use a refractory package similar to the LAW melter to contain the molten glass. The refractory package is designed to serve as a mechanical, thermal, and electrical barrier between the molten glass inside the melter and the melter shell.

 The HLW melters Melters will also use an steel outer shell, which, with the refractory package, will contain the molten glass and melter offgas. Active cooling on the exterior of the melter will be provided by a water jacket, which will be in a two-loop system that will transfer heat from the HLW melter Melter through heat exchangers to cooling towers. The loop containing the water jacket will be a closed system that isolates the water circulating through the water jacket from the water in the cooling water loop circulating to the cooling tower. Radioactive Mixed waste material leaking into the intermediate loop cooling water will be prevented from becoming an inadvertent discharge through the cooling tower. The refractory package will provide adequate containment should there be a loss of cooling. The HLW melter Melter lid will be constructed of a steel outer shell and insulated from the melter plenum by refractory material.

The HLW melter will use two independent discharge chambers. Discharge will be achieved by transferring the molten glass from the bottom of the melter pool, through a riser, from which it will be poured into a stainless steel IHLW container canister. Glass waste transfer will be accomplished through air lifting. The IHLW will then be allowed to cool, forming a highly durable borosilicate glass waste form.

 Waste <u>HLW mM</u>elters will be removed from the melter cave and placed in an overpack. The spent melter will be treated as newly generated waste, and will initially be managed within the HLW melter containment buildings. If necessary, the overpack will be decontaminated using a dry process. Waste <u>HLW mM</u>elters will be stored in the HLW or LAW out of service melter storage facility.

4.2.3.3 Automatic Waste Feed Cut-Off System

The LAW and HLW melters will be equipped with the ability to cut off waste feed.

Automatic waste feed cut_off systems terminate feed to the melter Melter if a specified operating condition is exceeded.

This design approach is consistent with the WAC 173-303-680 regulatory requirements.

The LAW (LMP-MLTR-00001/2) and HLW (HMP-MLTR-00001/2) melters Melters are fed via air displacement slurry pumps that utilize pressurized air as the motive force. It supplies These pumps supply feed to the melters in slugs which that act to keep lines from plugging. The feed is injected into the melters through the feed nozzles on top of the melter-Melter creating a "cold cap", where waste feed undergoes several physical and chemical changes. The glass product in the melter is then "air lifted" through the discharge chamber and into the glass container. Melter offgas is generated from the vitrification of LAW and HLW of which the rate of generation is dynamic and not steady state. The offgas is then carried away and treated via a dedicated offgas system.

The melter systems are designed to minimize the need for automatic waste feed cut_off functions. Control of melter level and plenum pressure, process alarming, and optimized operating procedures will be in place to reduce the occurrences of interlocking. Given the processing speeds and the relatively slow rates of change in the operating states of the melter, operations operators should have adequate time to react to upset conditions. An example of the slow rate of change can be seen in the volume of feed per air displacement slurry pump feed cycle when increasing melter level. Each pump cycle adds approximately one 1 gallon of slurry into the melter. At one-1 gallon of volume, the liquid level rises no greater than 0.01 in. inside the melter. This provides ample time for operator response.

 Previous operating experience with similar melters has shown that two types of operating conditions existed that warranted automatic waste feed cut off: (1) high melter pressure, and (2) high melter glass level. These interlocks have been sufficient to allow continued melter operations without inadvertent feed cut off signals, yet provide a sufficient safety margin.

4.2.3.4 Offgas Treatment System

The offgas treatment system will remove steam, aerosols, entrained particulates, decomposition products, and volatile contaminants that are generated from the vitrification processes and the vessel ventilation systems. The <u>principal constituents contained in the melter offgas</u> stream are as follows:

1 ☐Air in-leakage and purges into the melter 2 3 Water vapor evaporated from the melter feed □Acid gases generated from anion decomposition (i.e., nitrogen oxide and sulfur oxide) 4 5 Acrosols from dried melter feed and melter cold cap reaction solids 6 • Nitrogen oxides from decomposition of metal nitrates in the melter feed 7 Chloride, fluoride, and sulfur as oxides, acid gases, and salts Radionuclide pParticulates and aerosols 8 9 • Entrained feed material and glass 10 A detailed description of the current offgas treatment trains for the LAW (LMP-MLTR-00001/2) 11 and HLW (HMP-MLTR-00001/2) melters Melters is provided in sSections 4.1.4 and 4.1.5, 12 13 respectively. 14 4.2.3.5 Maximum Achievable Control Technology (MACT) Standards Reserved 15 16 The WTP melter systems are thermal treatment units classified as miscellaneous units in 17 Washington Administrative Code (WAC) 173-303-680. The dangerous waste regulations require that permits for miscellaneous units include such terms, conditions, and provisions that 18 are necessary to protect human health and the environment and are appropriate for the 19 20 miscellaneous unit being permitted. Ecology has determined that regulations that are most appropriate to apply to the melters and offgas systems are found in applicable sections of the 21 22 incinerator requirements (WAC 173-303-670). These standards are known as Maximum 23 Achievable Control Technology (MACT) and were promulgated by the EPA in September 1999 (64-FR-52828). In April 2001, Ecology provided guidance to the WTP regarding the regulatory 24 standards they will be applying to the melter systems, including certain requirements contained 25 in the MACT rule for hazardous waste combustors (Ecology 2001). The requirements are 26 27 outlined in the following: 28 29 Pollutant-Ecology-directed requirement 30 Principle Organic Dangerous -99.99% destruction and removal efficiency -Constituents 31 32 dscm 33 34 □Emissions corrected to 7% exygen basis 35 TEQ is toxicity equivalence defined in 40 CFR 63.1201(a) 36 Edsem is dry standard cubic meter 37 □ppmv is parts per million by volume 38 □Rolling average is the average of all one minute averages over the averaging period [40 CFR 63.1202(a)] 39 40 41 On July 24, 2001, the United States Court of Appeals, District of Columbia (D.C.) Circuit,

51-4-184

emission standards (United States Court of Appeals, D.C. Circuit 2001a). On October 26, 2001,

vacated the MACT rule for hazardous waste combustors and ordered the EPA to rewrite the

the EPA, together with other litigants, filed a joint motion asking the Court to delay issuance of a mandate that would vacate the MACT emission standards for hazardous waste combusters (United States Court of Appeals, D.C. Circuit 2001b). On November 1, 2001, the Court granted the joint motion. As a result, the mandate to vacate the emission standards has been stayed to February 14, 2002.

6 7

8

9

10

11

DOE intends that the melter systems be designed and constructed so that they operate in compliance with the appropriate and applicable standards. Environmental performance demonstrations during cold commissioning of the HLW and LAW vitrification plants will be used to verify compliance with the DRE and other as applicable air emission standards. Ecology's guidance also indicated that some periodic demonstration testing will need to be performed after the WTP has begun processing radioactive wastes (Ecology, 2001).

12 13 14

15

16

The WTP contractor has undertaken a review of the requirements outlined above to determine the feasibility of implementing them in a radioactive environment. A proposal regarding compliance with the MACT requirements will be prepared by the date identified in the DWPA Completion Schedule.

17 18 19

4.2.3.6 Physical and Chemical Characteristics of Waste [WAC 173-303-680(2)(a)(i)]

A description of the waste characteristics of the LAW and HLW feeds is presented in <u>DWP</u>

Attachment 51, Chapter 3 (see Appendix 3A). The immobilized waste generated by the vitrification processes will be in the form of glass that maintains its chemical and physical integrity during long-term storage. The waste analysis plan (Appendix 3A) describes the types and frequency of analysis that will be performed on the glass waste.

25 26

4.2.3.7 Treatment Effectiveness Report [WAC 173-303-806(4)(i)(iv)]

27 A treatment effectiveness report evaluating the performance of the miscellaneous unitstreatment sub-systems, and their effectiveness in treating the LAW and HLW, is provided will be located in 28 29 DWP Attachment 51, Appendices Appendix 9-16 for LAW and Appendix 10 for HLW-16. 30 Sampling and analyses to be performed on the glass waste are described in the waste analysis 31 plan (Appendix 3A). Air monitoring and analysis requirements are addressed in the WTP air 32 permitsThe report will use the results of the environmental performance demonstration and the 33 risk assessment activities to document treatment effectiveness of miscellaneous treatment 34 sub-systems.

35 36

4.2.3.8 Environmental Performance Standards for Melter Systems [WAC 173-303-680(2)]

- An environmental performance demonstration will be conducted to demonstrate the efficiency of the LAW and HLW melter Melter systems and their respective air pollution control systems.
- 39 Emissions from the LAW and HLW systems will be sampled and analyzed during an
- 40 environmental demonstration performed during cold commissioning. The data developed during
- 41 the environmental performance demonstration will support the screening-level risk assessment,
- which will support the development of environmental performance standards for the LAW and HLW melter systems.

The operational activities of the WTP include methods intended to ensure proper performance of equipment and processes. These methods include sampling of materials, use of direct process controls, development of equipment life specifications and ongoing maintenance.

4.2.3.8.1 Protection of Groundwater, Subsurface Environment, Surface Water, Wetlands and Soil Surface [WAC 173-303-680(2)(a) and (b)]

The LAW melters will be located in the LAW melter gallery (L-0112) within the LAW vitrification plant. The HLW melters Melters will be located in the HLW melter caves (H-0117, H-0106) within the HLW vitrification plant. Both plants are designed to comply with standards that ensure protection of the surface and subsurface environments. The vitrification plants will be completely enclosed and are designed to have sufficient structural strength and corrosion protection to prevent collapse or other structural failure. In addition, the melter systems, melter feed systems, and related piping will be provided with secondary containment, to minimize the potential for release. The LAW melter gallery (L-0112) and the HLW melter caves (H-0117, H-0106) will be permitted as containment buildings and are described in Section 4.2.4.

Floors within the vitrification plants will be protected in a manner consistent with the intended usage of the space. The process room floor and walls of the LAW melter gallery will be protectively coated. The floor and portions of the walls of HLW melter Melter cave will be partially lined with stainless steel. Nonradioactive materials usage areas requiring heavy equipment will have concrete floors with hardener and sealer finishes.

The Hanford Facility Dangerous Waste Permit Application General Information Portion, Ssection 5.4 (DOE-RL 1998), provides climatological data, topography, hydrogeological and geological characteristics, groundwater flow quantity and direction, groundwater quality data, and surface water quantity and quality data for the area around the WTP.

4.2.3.8.2 Protection of the Atmosphere [WAC 173-303-680(2)(c)]

A risk assessment will be performed to evaluate the impacts of the WTP emissions on human and ecological receptors. Actual offgas emissions will be measured during an environmental performance demonstration that will be performed as part of the WTP commissioning activities. The data will be used during a screening—level risk assessment that will be performed to determine ecological and human health risk. The emissions data, and the results of the screening level risk assessment, will be used to establish operating conditions for the melters that do not endanger human health and the environment.

4.2.3.9 Approach to Risk Assessment [WAC 173-303-680(2)-(c)(i) through (vii)]

A screening levelpre-demonstration test risk assessment is being conducted to evaluate the
environmental impacts any possible human health and ecological resource consequences posed
by the thermal treatment of miscellaneous mixed units wastes. It The risk assessment will provide
information about the potential terrestrial, aquatic, and food pathways for exposure of human and
ecological receptors to dangerous waste constituents. This risk assessment will present the
quantitative methods, detailed assumptions, and numerical parameters that will be used to
estimate the nature, extent, and magnitude of potential impacts risks from operation of the WTP,

and will identify the the approach and computations will be in accordance with the government's guidance documents used in performing the such risk assessments.

2 3 4

Treated air emissions through the stack will be the only planned direct releases into the environment from the WTP-released directly into the environment. Other waste streams will be transferred to a permitted facility and will not be released directly into the environment. Thus, the screening level pre-demonstration test risk assessment will focus primarily on air emissions.

Major components of the <u>human health and ecological</u> risk assessment process for evaluating airborne emissions will be as follows:

- Risk assessment work plan
- Preliminary-Pre-demonstration test risk assessment
- Final risk assessment

The overall approach for the risk assessment will be to identify potential risks associated with various receptors, their locations, exposure pathways, and activity patterns in two broad exposure scenarios, as follows:

- Plausible exposure scenario
- Worst-case exposure scenario

The plausible exposure scenarios will be based on where potential receptors currently exist or may reasonably be expected to exist within the foreseeable future. The worst-case exposure scenario will be based on worst-case assumptions regarding the will be based on locations of receptors, exposure pathways, and activity pattern. The plausible exposure scenario will be based on more realistic assumptions regarding the location of maximum concentration even though it is not expected that such receptors will ever actually exist at these locations. It will both scenarios will reflect current uses of the surrounding land and habitat, and reasonable assumptions about future uses of the land and habitat.

During the environmental performance demonstration, emission samples will be collected and analyzed, and the data will be used to evaluate risk to the human (including Native Americans) population and ecological (including such as wildlife) receptors. Operating conditions will be established for the WTP, which limit risks to human health and the environment to acceptable levels.

4.2.4 Containment Buildings

- This section describes how these units are designed and operated, in accordance with the requirements of WAC 173-303-695, which incorporates 40 CFRPart 264 Subpart DD,
- 41 "Containment Buildings", by reference. Regulatory citations in this section list the applicable
- section of the CFR to make it easier for readers to find the requirement. A typical containment
- building is illustrated in Appendix 4A, Figure 4A-59.

3

There will be twelve are a number of twenty containment buildings at the WTP: three four

located within the pretreatment plant; three-six in the LAW vitrification plant; and six-ten in the

4 HLW vitrification plant. The regulated units are:

5

- Pretreatment hot cell containment building (P-0123)
- Pretreatment maintenance containment building (PM0124, P-0121A, P-0122A, P-0123A, P-0124, P-0124A, P-0125A, P-0125A, P-0128A)
- 9 Pretreatment air filtration filter package maintenance containment building (P-0223)
- Pretreatment air filter package containment building (P-0335)
- 11 LAW LSM gallery containment building (L-0112)
- ILAW container finishing containment building (L-0109B/,L-0109C, L-01/09D/, L-0109E,
 L-0115B, L-01/15C, L-01/145D, L-0115E/16A/16B)
- LAW vitrification plant consumable import/export containment building (L-0119B)
- LAW vitrification plant C3 workshop containment building (L-226A)
- LAW pour cave containment building (L-B015A, L-B013C, L-B013B, L-B011C, L-B011B, and L-B009B)
- LAW container buffer storage containment building (L-B025C, L-B025D)
- HLW melter cave no. 1 containment building (H-0117, H-0116B, H-0310A)
- <u>HLW melter cave no. 2-containment buildings containment building (H-0106, H-0105B, and H-0304A)</u>
- IHLW container weld containment building cave containment building (H-0136)
- IHLW container canister decontaminations wabbing and monitoring building cave containment building (H-0133)
- HLW vitrification plant C3 workshop-containment building containment building (H-0311A,
 H-0331/A/B)
- HLW vitrification plant air filtration containment building (H-0103/4)
- 31 HLW pour tunnel no. 1 (H-B032)
- 32 and HLW pour tunnel no. 2 (H-B032 and (H-B005A)
- HLW drum swabbing and monitoring area (H-0126A, H-0126B, and-H-B028)
- HLW waste handling area (H-410, H-410A, H-410B, and H-411)

- Table 4-12 summarizes the units within the WTP. The following figures and drawings found in
- 37 <u>DWP Attachment 51 Appendix 4A</u> provide further detail for the WTP containment buildings: 38
- Typical system Figure 4A-59 depicting common features for each of containment buildings

- Simplified-General arrangement figures and drawings showing locations of containment
 buildings
 - Waste management area figures and drawings showing containment building locations to be permitted
 - ☐Contamination/radiation area boundary figures showing contamination/radiation zones throughout the plants

Control of fugitive emissions from containment buildings is described in *Fugitive Emissions*Control Description (24590-WTP-PER-HV-02-001) located in DWP Attachment 51, Appendix.

The following sections address each of the twelve-containment buildings.

4.2.4.1 Pretreatment Hot Cell Containment Building (P-0123)

- The first containment building in the pretreatment plant is located in the central portion of the pretreatment plant, and stretches nearly the entire length of the building.

 16
- The process equipment is remote handled in case of failure and is removed by an overhead crane or powered manipulator. Manipulators assist in the decontamination and remote repair. The unit also contains a crane and powered manipulator repair area. The failed equipment is placed inside disposal boxes and transported through a series of airlock and shield doors to a truck load—out area on the outside of the building.

 Process equipment, such as pumps, valves, <u>and jumpers</u>, and filters are located in this containment building. Typical waste management activities performed in this containment building include; the removal and staging of failed, remote-handled process equipment prior to decontamination, repair, and/or packaging of waste for disposal. Jumpers connecting process equipment may leak waste when the jumper connection is broken. Although some decontamination capability is present in the pretreatment hot cell containment building, some quantities of waste, especially solids, will remain following decontamination. The design features associated with the pretreatment hot cell containment building, discussed below, ensure the capability to manage residual waste from process jumper leakage throughout the 40-year design lifetime of the pretreatment plant.

Pretreatment Hot Cell Containment Building Design

The pretreatment hot cell containment building is designed as a completely enclosed area within the pretreatment plant. It is designed to prevent the release of dangerous constituents and their exposure to the outside environment. The design and construction of the hot cell, and the pretreatment plant exterior will prevent water from running into the plant. The approximate dimensions of the unit are summarized in Table 4-12.

Pretreatment Hot Cell Containment Building Structure

The pretreatment hot cell containment building will be a concrete-walled structure fully enclosed within the pretreatment plant. Therefore, structural requirements for the containment building will be met by the design standards of the pretreatment plant. The roof of the pretreatment plant

- will consist of metal roofing, roof insulation, and vapor barrier. Rainwater run-off will be collected by roof drains and drainage systems with overflow roof drains. The design will ensure that the unit has sufficient structural strength to prevent collapse or failure. DWP Attachment 51, Chapter 4, Supplement 1 Supplement 1 provides documentation that the The seismic requirements for the pretreatment plant are presented in the RPP WTP Compliance with meet or exceed the Uniform Building Code Seismic Design Requirements identified in Attachment 51, Chapter 4, Supplement 1.
- 9 Pretreatment Hot Cell Containment Building Materials

16

23 24

- 10 The pretreatment hot cell containment building will be constructed of steel-reinforced concrete.
- 11 The interior floor and a portion of the walls of the unit will be partially lined with stainless steel.
- 12 The balance of the walls will have an impervious coating. The roof of the pretreatment plant will
- 13 consist of metal roofing, roof insulation, and vapor barrier. Rainwater run off will be collected
- by roof drains and drainage systems with overflow roof drains.
 - Use of Incompatible Materials in the Pretreatment Hot Cell Containment Building
- 17 A partial stainless steel liner will be provided for this unit. Stainless steel will be compatible
- with the equipment waste that will be managed, which will include failed pumps, ultrafilters, and
- 19 valves containing a minimal amount of waste constituents. Activities in the unit will include, but
- 20 not be limited to, to ddecontamination, size reduction, and packaging the waste components into
- 21 drums or waste boxes. Treatment reagents that could cause the liner to leak, corrode, or
- 22 otherwise fail will not be used within the unit.
 - Primary Barrier Integrity in the Pretreatment Hot Cell Containment Building
- 25 The pretreatment hot cell containment building is designed to withstand loads from the
- 26 movement of personnel, wastes, and handling equipment. The seismic design criteria identified
- in Supplement 1DWP Attachment 51, Supplement 1, ensures that appropriate design loads, load combinations, and structural acceptance criteria are employed at the WTP.
- 29
 30 <u>Certification of Design for the Pretreatment Hot Cell Containment Building</u>
- 31 Prior to startup of operations, a certification by a qualified registered professional engineer that
- 32 the pretreatment hot cell containment building meets the design requirements of
- 33 40 CFR 264.1101(a), (b), and (c) will be obtained.
- 35 Operation of the Pretreatment Hot Cell Containment Building
- Operational and maintenance controls and practices will be established and followed to ensure containment of the waste within the pretreatment hot cell containment building as required by
- 38 40 CFR 264.1101(c)(1).
 - Maintenance of the Pretreatment Hot Cell Containment Building
- The <u>partial</u> stainless steel lining of the unit will be constructed and maintained in a manner that
- will be free of significant cracks, gaps, corrosion, or other deterioration. The partial stainless
- 43 steel liner will remain free of corrosion or other deterioration because it is compatible with
- 44 materials that will be managed in the containment building. The failed equipment that will be

managed in the containment building unit will be compatible with stainless steel. Only 1 2 decontamination chemicals that are compatible with the liner will be used. 3 4 Measures to Prevent Tracking Wastes from the Pretreatment Hot Cell Containment Building The pretreatment hot cell containment building is designed to isolate failed equipment from the 5 6 accessible environment and to prevent the spread of contaminated materials. Very little dust is 7 expected to be generated in the unit. Personnel access to the unit, which is classified as a C5 8 contamination area, will be restricted due to radiological concerns. Waste leaving the unit may 9 or may not be enclosed within containers. If necessary, these containers may be decontaminated 10 in the unit prior to transportation to another permitted storage area. Equipment leaving the unit will be decontaminated before being released for removal. 11 12 13 Control of Fugitive Dust from the Pretreatment Hot Cell Containment Building The following measures will be used to prevent fugitive dust from escaping the pretreatment hot 14 15 cell-containment building: 16 17 □ A cascading air flow from areas of least to greatest potential contamination (i.e., C2 to C3 to 18 C5) 19 Greater negative air pressure in the unit compared to adjacent C2 units, to pull air into the unit 20 and prevent backflow 21 □Intake air through controlled air in bleed units, with backflow prevention dampers, and air 22 gaps around shield doors sized to prevent backflow □Dual HEPA filtration of exhaust air before discharge to the atmosphere through a monitored 23 24 25 □ A multiple fan extraction system designed to maintain negative pressure and cascading air 26 flow, even during fan maintenance and repair 27 28 Procedures in the Event of Release or Potential for Release from the Pretreatment Hot Cell 29 Containment Building 30 The design and operation of the unit makes it very unlikely that releases will occur. The design 31 and operational measures will minimize the generation of dust and contain it within the unit. 32 The ventilation system will also use negative air pressure to keep contamination from spreading 33 to areas of lesser contamination, and will use two-stage HEPA filtration to reduce the release of particles. The ventilation system is designed with backup HEPA filters to provide redundant 34 35 controls and to facilitate repairs or replacement. Offgas will be routed to the pretreatment 36 ventilation system. 37 38 Inspections will identify conditions that could lead to a release. Such conditions will be 39 corrected as soon as possible after they are identified. In the unlikely event that a release of 40 dangerous wastes from the containment building is detected, actions required by 41 40 CFR 264.1101(c)(3)(i) through (iii) will be taken. Specific administrative and operating 42 methods that will be used to satisfy this requirement will be developed prior to the start of

operations. These methods will be followed to repair conditions that could lead to a release.

43

1 Inspections of the Pretreatment Hot Cell Containment Building

2 An inspection program will be established to detect conditions that could lead to a release of 3

wastes from the pretreatment hot cell containment building. The inspection and monitoring

4 schedule and methods that will be used to detect releases from the unit is are included in Chapter 5 6.

6 7

8 9

10

11 12

13

14

15

16

4.2.4.2 Pretreatment Maintenance Containment Building (PM0124, P-0121A, P-0122A, P-0123A, P-0124, P-0124A, P-0125, P-0125A, P-0128, P-0128A)

The pretreatment plant will have a second area that meets the definition of a containment building. The pretreatment maintenance containment building comprises the majority of the east end of the building. Typical waste management activities performed in this containment building include; equipment maintenance, including decontamination, size reduction, and packaging of spent equipment. This unit consists of the interim storage, lag storage, manipulator decontamination and repair, resin handling, waste packaging, tool cribs, and sub-change, and filter overpack lidding rooms. The unit will include hatches to import or export spent equipment. An overhead crane will facilitate movement of equipment and removal or placement of the spent equipment in the waste containers.

17 18 19

20

21

22

23

24

25

Pretreatment Maintenance Containment Building Design

The pretreatment maintenance containment building is designed as a completely enclosed area within the pretreatment plant. The unit is designed to prevent the release and exposure of dangerous constituents to the outside environment. The design and construction of the pretreatment plant exterior will prevent water from running into the plant. The roof of the pretreatment plant will consist of metal roofing, roof insulation, and a vapor barrier. Rainwater run-off will be collected by roof drains and drainage system with overflow roof drains. The approximate dimensions of the unit are summarized in Table 4-12.

26 27 28

29 30

31

32

33

34 35

36

Pretreatment Maintenance Containment Building Structure

The pretreatment maintenance containment building will consist of several rooms within the concrete-walled, fully enclosed pretreatment plant. Therefore, structural requirements for the containment building will be met by the design standards of the pretreatment plant. The design will ensure that the unit has sufficient structural strength to prevent collapse or failure. DWP Attachment 51, Chapter 4, Supplement 1 provides documentation that the seismic requirements for the pretreatment plant meet or exceed the Uniform Building Code Seismic Design Requirements. The seismic requirements of the pretreatment plant are presented in the RPP-WTP Compliance with Uniform Building Code Scismic Design Requirements, as identified in Supplement 1.

37 38 39

40

41

42

43

Pretreatment Maintenance Containment Building Materials

The pretreatment maintenance containment building will be constructed of steel-reinforced concrete. The interior floor and portions of the walls of the unit will be -lined with stainless steel. The balance of the walls will have an impervious coating. The roof of the pretreatment plant will consist of metal roofing, roof insulation, and a vapor barrier. Rainwater run off will be collected by roof drains and drainage system with overflow roof drains.

- 1 Use of Incompatible Materials in the Pretreatment Maintenance Containment Building
- 2 A partial stainless steel liner will be provided for the unit. Stainless steel will be compatible with
- the equipment wastes that will be managed, which will include failed pumps, ultrafilters, and 3
- valves. Activities in the unit will be limited to decontamination, size reduction, and packaging 4
- the waste components into drums or waste boxes. Treatment reagents that could cause the liner 5
- to leak, corrode, or otherwise fail will not be used within the unit. 6

- Primary Barrier Integrity in the Pretreatment Maintenance Containment Building
- The pretreatment maintenance containment building is designed to withstand loads from the 9
- movement of personnel, wastes, and handling equipment. The seismic design criteria identified 10
- in Supplement 1DWP Attachment 51, Supplement 1, ensures that appropriate design loads, load 11
- combinations, and structural acceptance criteria are employed at the WTP. 12

13 14

- Certification of Design for the Pretreatment Maintenance Containment Building
- Prior to startup of operations, certification by a qualified registered professional engineer that the 15
- pretreatment maintenance containment building meets the design requirements of 16
- 17 40 CFR 264.1101(a), (b), and (c) will be obtained.

18 19

- Operation of the Pretreatment Maintenance Containment Building
- 20 Operational and maintenance controls and practices will be followed to ensure containment of
- the waste within the pretreatment maintenance containment building as required by 21
- 22 40 CFR 264.1101(c)-(1).

23 24

- Maintenance of the Pretreatment Maintenance Containment Building
- The stainless steel lining of the unit will be constructed and maintained in a manner that will be 25
- free of significant cracks, gaps, corrosion, or other deterioration. The stainless steel liner will 26
- remain free of corrosion or other deterioration because it will be compatible with materials that 27
- will be managed in the containment building, which will include failed equipment. Only 28 decontamination chemicals that are compatible with the liner will be used.
- 29

30

- 31 Measures to Prevent Tracking Wastes from the Pretreatment Maintenance Containment Building
- The pretreatment maintenance containment building is designed to isolate failed equipment from 32
- 33 the accessible environment and to prevent the spread of contaminated materials. A dust cleanup
- system will minimize the potential for dust to be tracked from the unit by humans or equipment. 34
- The containment building will be classified as a C3/C5 contamination area and, therefore, 35
- personnel access will be limited, and may be restricted due to radiological concerns. Wastes 36
- leaving the unit may be enclosed within containers. If necessary, these containers will be 37
- 38 decontaminated in the unit prior to transportation to another permitted storage area. Equipment
- leaving the unit will be decontaminated before being released for removal from the cell. 39

40

- Control of Fugitive Dust from the Pretreatment Maintenance Containment Building 41
- The following measures will be used to prevent fugitive dust from escaping the pretreatment 42 43 maintenance containment building.

1 2	☐A cascading air flow from areas of least to greatest potential contamination (i.e., C2 to C3 to C5)
3 4	☐ Greater negative air pressure in the unit compared with adjacent C2 units, to pull air into the unit and prevent backflow
5 6	☐ Intake air through controlled air in-bleed units, with backflow prevention dampers, and air gaps around shield doors sized to prevent backflow
7 8	□Dual HEPA filtration of exhaust air before discharge to the atmosphere through a monitored stack
9 10	☐A multiple fan extraction system designed to maintain negative pressure and cascading air flow, even during fan maintenance and repair
l1 l2	☐Personnel ingress and egress through airlocks and subchange rooms
 [4	Procedures in the Event of a Release or Potential Release from the Pretreatment Maintenance Containment Building
15 16 17 18 19	The design and operation of the unit makes it very unlikely that releases will occur. The design and operational measures that will be used will minimize the generation of dust and contain it within the unit. The ventilation system will also use negative air pressure to keep contamination from spreading to areas of lesser contamination and will use two stage HEPA filtration to reduce the release of particles.
21 22 23 24	Inspections will identify conditions that could lead to a release. Such conditions will be corrected as soon as possible after they are identified. The ventilation system is designed with backup HEPA filters to provide redundant controls and to facilitate repairs or replacement.
25 26 27 28 29	In the unlikely event that a release of dangerous wastes from the containment building is detected, actions required by 40 CFR 264.1101(c)(3)(i) through (iii) will be taken. Specific administrative and operating methods that will be used to satisfy this requirement will be developed prior to the start of operations. These methods will be followed to repair condition that could lead to a release.
31 32 33 34 35 36	Inspections of the Pretreatment Maintenance Containment Building An inspection program will be established as required under WAC 173-303-695 to detect conditions that could lead to the release of wastes from the pretreatment maintenance containment building. Such conditions will be corrected as soon as possible after they are identified. The inspection and monitoring schedule and methods that will be used to detect a release is are included in Chapter 6.
38 ± 39	4.2.4.3 Pretreatment Air Filtration Filter Package Maintenance Containment Building (P-0223)
10 11 12 13	The pretreatment air filtration filter package maintenance containment building is the third containment building within the pretreatment plant, located in the southeast portion of the plant. Typical waste management activities performed in this containment building include, waste storage, size reduction, decontamination, and equipment repair. A crane transports spent HEPA

- and HEME filters to a size reduction station and then places them inside a disposal container. 1 2 The disposal container is then transported via cart, through an air lock and shield doors and to a load-out area for storage pending final disposal. The containment building also houses a 3 4 hands-on crane decontamination and repair area. 5 6 Pretreatment Air FiltrationFilter Package Maintenance Containment Building Design 7 The pretreatment air filtrationfilter package maintenance containment building will be 8 completely enclosed within the pretreatment plant, and will be designed to prevent the release 9 and exposure of dangerous constituents to the outside environment. The design and construction 10 of the pretreatment plant exterior will prevent water from running into the plant. The roof of the pretreatment plant will consist of metal roofing, roof insulation, and a vapor barrier. Run-off 11 12 will be collected by roof drains and a drainage system with overflow drains. The interior floor 13 and a portion of the walls will be lined with a protective coating. The approximate dimensions 14 of the containment building are summarized in Table 4-12. 15 16 Pretreatment Air FiltrationFilter Package Maintenance Containment Building Structure 17 Because the pretreatment air filtration filter package maintenance containment building will be a 18 concrete-walled structure fully enclosed within the pretreatment plant, its requirements will be 19 met by the design standards of the pretreatment plant. The design will ensure that the unit has 20 sufficient structural strength to prevent collapse or failure. DWP Attachment 51, Chapter 4, 21 Supplement 1 provides documentation that the seismic requirements for the 22 pretreatment plant meet or exceed the Uniform Building Code Seismic Design Requirements. The 23 seismic requirements for the pretreatment plant are presented in the RPP-WTP Compliance with 24 Uniform Building Code Seismic Design Requirements, contained in Supplement-1. 25 26 Pretreatment Air FiltrationFilter Package Maintenance Containment Building Materials 27 The pretreatment air filtration filter package maintenance containment building will be 28 constructed of steel-reinforced concrete. A protective coating will be provided for the 29 containment building. The interior floor and a portion of the walls will be lined with a protective 30 ceating. The roof of the pretreatment plant will consist of metal roofing, roof insulation, and a vapor-barrier. Run-on will be collected by roof drains and a drainage system with overflow 31 32 drains. 33 34 Use of Incompatible Materials for the Pretreatment Air Filtration Filter Package Maintenance 35 Containment Building A protective coating will be provided for the containment building. The protective coating will 36 be compatible with the wastes that will be managed in the unit, which will include spent HEPA 37 38 and HEME filters. Activities in the unit will be limited to size reduction and waste packaging. 39 Treatment reagents that could cause the protective coating to leak, corrode, or otherwise fail will not be used within the unit. 40 41
- 42 Primary Barrier Integrity in the Pretreatment Air FiltrationFilter Package Maintenance
- 43 <u>Containment Building</u>
- 44 The pretreatment air filtration filter package maintenance containment building will be designed
- 45 to withstand loads from the movement of personnel, wastes, and handling equipment. The

seismic design criteria found in Supplement 1DWP Attachment 51, Supplement 1, ensures that 1 appropriate design loads, load combinations, and structural acceptance criteria are employed at 2 3 the WTP. 4 5 Certification of Design for the Pretreatment Air FiltrationFilter Package Maintenance 6 Containment Building Prior to the start of operations, certification by a qualified registered professional engineer that 7 the pretreatment air filtrationfilter package maintenance containment building meets the design 8 requirements of 40 CFR 264.1101(a) and (c) will be obtained. The requirements of 40 9 CFR 264.1101(b) do not apply to this design because waste containing liquids will not be 10 managed in the unit and waste will not be treated with liquids. 11 12 13 Operation of the Pretreatment Air FiltrationFilter Package Maintenance Containment Building Operational and maintenance controls and practices will be established to ensure containment of 14 the waste within the pretreatment air filtration filter package maintenance containment building, 15 16 as required by 40 CFR 264.1101(c)(1). 17 Maintenance of the Pretreatment Air FiltrationFilter Package Maintenance Containment Building 18 The protectively-coated concrete floor and walls of the unit will be constructed and maintained 19 in a manner that will be free of significant cracks, gaps, corrosion, or other deterioration. The 20 protective coating will be compatible with materials that will be managed in the containment 21 building, which will include spent HEPA and HEME filters. No decontamination chemicals that 22 are incompatible with the coated concrete will be used. 23 24 Measures to Prevent Tracking Wastes from the Pretreatment Air FiltrationFilter Package 25 26 Maintenance Containment Building The pretreatment air filtration filter package maintenance containment building is designed to 27 manage spent HEPA and HEME filters. Conducting these activities in a C5 zone will prevent 28 the spread of contaminated materials. Restricted personnel access and controlled movement of 29 equipment into and out of the unit will decrease the possibility that waste will be tracked from 30 31 the unit. 32 Personnel access to the pretreatment plant air filtration filter package maintenance containment 33 building, which is classified as a C5 contamination area, will be restricted due to radiological 34 concerns. Access to the unit will be allowed only under limited circumstances, thereby limiting 35 the potential for contacting the waste and tracking it from the unit. 36 37 38 Control of Fugitive Dust from the Pretreatment Air Filtration Containment Building 39 The following measures will be used to prevent fugitive dust from escaping the pretreatment air 40 filtration containment building unit: 41 □A cascading air flow from areas of least to greatest potential contamination (i.e., C2 to C3 to 42

Greater negative air pressure in the unit, compared with adjacent C2 units, to pull air into the

43

44 45

unit and prevent backflow

1	UIntake air through controlled air in bleed units, with backflow prevention dampers, and air
2	gaps around shield doors sized to prevent backflow
3 4	□Dual HEPA filtration of exhaust air before discharge to the atmosphere through a monitored stack
5	A multiple fan extraction system designed to maintain negative pressure, and cascading air flow, even during fan maintenance and repair
7	©Personnel ingress and egress through airlocks and subchange rooms
8	an analysis and agreed and agreement and adoling 1001115
9	Procedures in the Event of Release or Potential for Release from the Pretreatment Air
10	FiltrationFilter Package Maintenance Containment Building
11	Conditions that could lead to a release from the pretreatment air filtration filter package
12	maintenance containment building will be corrected as soon as possible after they are identified-
13	The ventilation system and airlocks, the most likely sources of potential releases, will be
14	designed with backup HEPA filters to facilitate repairs and replacement.
15	
16	In the unlikely event of a release of dangerous wastes from the containment building, actions
17 10	required by 40 CFR 264.1101(c)(3)(i) through (iii) will be taken. Specific administrative and
18 19	operating methods that will be used to satisfy this requirement will be developed prior to the start of operations.
20 ·	of operations.
21	Inspections of the Pretreatment Air-FiltrationFilter Package Maintenance Containment Building
22	An inspection program will be established to detect conditions that could lead to a release of
23	wastes from the pretreatment air filtration filter package maintenance containment building. The
24	inspection and monitoring schedule, and methods that will be used to detect releases from the
25	unit, are included in Chapter 6.
26	
27	4.2.4.4 Pretreatment Air Filter Package Containment Building (P-0335)
28	The pretreatment air filter package containment building is the fourth containment building
29	within the pretreatment plant, in the southeast portion of the plant. Typical waste management
30	activities performed in this containment building include waste storage, size reduction,
31	decontamination, and equipment repair. A crane transports the spent HEPA and HEME filters to
32	a size reduction station and then places them inside a disposal container. The disposal container
33	is then transported via cart through an air lock and shield doors and to a load-out area for storage
34	pending final disposal. The containment building also houses a dedicated crane maintenance
35	area.
36	Duraturaturant Ain Filter David
37 38 -	Pretreatment Air Filter Package Containment Building Design The pretreatment air filter package containment building ill be a least to the pretreatment of the pretrea
39	The pretreatment air filter package containment building will be completely enclosed within the
40	pretreatment plant, and will be designed to prevent the release and exposure of dangerous constituents to the outside environment. The design and construction of the pretreatment plant
41	exterior will prevent water from running into the plant. The roof of the pretreatment plant will
42	consist of metal roofing, roof insulation, and a vapor barrier. Run-off will be collected by roof

1	drains and a drainage system with overflow drains. The approximate dimensions of the
2 3	containment building are summarized in Table 4-12.
4	Pretreatment Air Filter Package Containment Building Structure
5	Because the pretreatment air filter package containment building will be a concrete-walled
6	structure fully enclosed within the pretreatment plant, its requirements will be met by the design
7	standards of the pretreatment plant. The design will ensure that the unit has sufficient structural
8	strength to prevent collapse or failure. DWP Attachment 51, Chapter 4, Supplement
9	1Supplement 1 provides documentation that the seismic requirements for the pretreatment plant
10	meet or exceed the Uniform Building Code Seismic Design Requirements. The seismic
11	requirements for the pretreatment plant are presented in RPP WTP Compliance with Uniform
12	Building Code Scismic Design Requirements, provided in Attachment 51, Chapter 4, Supplement
13	1.
14	
15	Pretreatment Air Filter Package Containment Building Unit Materials
16	The pretreatment air filter package containment building will be constructed of steel-reinforced
17	concrete. The interior floor and a portion of the walls will be lined with a protective coating.
18	The roof of the pretreatment plant will consist of metal roofing, roof insulation, and a vapor
19	barrier. Run on will be collected by roof drains and a drainage system with overflow drains.
20	
21	Use of Incompatible Materials for the Pretreatment Air Filter Package Containment Building
22	AThe protective coating will be provided for the containment building. The coating will be
23	compatible with the wastes that will be managed in the unit, which will include spent HEPA and
24	HEME filters. Activities in the unit will be limited to size reduction and waste packaging.
25	Treatment reagents that could cause the protective coating to leak, corrode, or otherwise fail will
26	not be used within the unit.
27	
28	Primary Barrier Integrity in the Pretreatment Air Filter Package Containment Building
29	The pretreatment air filter package containment building will be designed to withstand loads
30	from the movement of personnel, wastes, and handling equipment. The seismic design criteria
31	found in DWP Attachment 51, Chapter 4, Supplement 1 Supplement 1 ensures that appropriate
32	design loads, load combinations, and structural acceptance criteria are employed at the WTP.
33	
34	Certification of Design for the Pretreatment Air Filter Package Containment Building
35	Prior to the start of operations, certification by a qualified, registered professional engineer that
36	the pretreatment air filter package containment building meets the design requirements of
37 .	40 CFR 264.1101(a) and (c) will be obtained. The requirements of 40 CFR 264.1101(b) do not
38	apply to this design because waste containing liquids will not be managed in the unit and waste
39	will not be treated with liquids.
4 0	
11	Operations of the Pretreatment Air Filter Package Containment Building
12	Operational and maintenance controls and practices will be established to ensure containment of
13	the waste within the pretreatment air filter package containment building, as required by
14	40 CFR 264.1101(c)(1).
15	

- 1 Maintenance of the Pretreatment Air Filter Package Containment Building
- The protectively coated concrete floor and walls of the unit will be constructed and maintained in 2
- 3 a manner that will be free of significant cracks, gaps, corrosion, or other deterioration. The
- protective coating will be compatible with materials that will be managed in the containment 4
- building, which will include spent HEPA and HEME filters. No decontamination chemicals that 5
- are incompatible with the coated concrete will be used. 6

- 8 Measures to Prevent Tracking Wastes from the Pretreatment Air Filter Package Containment
- 9 Building
- The pretreatment air filter package containment building is designed to manage spent HEPA and 10
- HEME filters. Conducting these activities in a C5 zone will prevent the spread of contaminated 11
- materials. Restricted personnel access and controlled movement of equipment into and out of 12
- 13 the unit will decrease the possibility that waste will be tracked from the unit.

14

- 15 Personnel access to the pretreatment air filter package containment building, which is classified
- as a C5 contamination area, will be restricted due to radiological concerns. Access to the unit 16
- 17 will be allowed only under limited circumstances, thereby limiting the potential for contacting
- 18 the waste and tracking it from the unit.

19

- 20 Procedures in the Event of Release or Potential for Release from the Pretreatment Air Filter
- 21 Package Containment Building
- Conditions that could lead to a release from the pretreatment air filter package containment 22
- building will be corrected as soon as possible after they are identified. In the unlikely event of a 23
- 24 release of dangerous wastes from the containment building, actions required by 40 CFR
- 264.1101(c)(3)(i) through (iii) will be taken. Specific administrative and operating methods that 25
- will be used to satisfy this requirement will be developed prior to the start of operations. 26

27

- 28 Inspections of the Pretreatment Air Filter Package Containment Building
- An inspection program will be established to detect conditions that could lead to a release of 29
- waste from the pretreatment air filter package containment building. The inspection and 30
- monitoring schedule and methods that will be used to detect releases from the unit are included 31 in DWP Attachment 51, Chapter 6. 32

33 34

4.2.4.5 LAW LSM Gallery Containment Building (L-0112)

- 35 There will be three fivesix containment buildings in the LAW vitrification plant. The first is the
- LAW locally shielded melter (LSM) gallery containment building, which will house the three 36
- 37 two LAW melters Melters. The LAW mMelters are designed to include a roller or wheel
- assembly that will be used to move the melters in and out of the containment building. 38
- Out of service Spent LAW mMelters will be disconnected from the offgas system, feed lines, 39
- electrical lines, and instrumentation. Open ports will be sealed. The sealed exterior of the melter 40
- will be decontaminated, if needed, prior to removal from the containment building-41
- 42 Out-of-service melters will be transported out of the unit to melter storage area 1 or 2.

LAW LSM Gallery Containment Building Design

The LAW LSM gallery containment building will be completely enclosed within the LAW vitrification plant. The unit will be designed to prevent the release and exposure of dangerous constituents to the outside environment. The design and construction of the LAW vitrification plant exterior will prevent water from running into the plant. The roof of the LAW vitrification plant will consist of metal roofing, roof insulation, and a vapor barrier. Rainwater run-off will be collected by roof drains and a drainage system with overflow drains. The approximate dimensions of the unit are summarized in Table 4-12.

The melter feed slurry will be introduced to the LAW melters through single-double-walled stainless steel feed lines. The feed lines will also be provided with bulges that will function as secondary containment. A low point within the bulge will be incorporated into the design to allow drainage to a sump located in the adjacent process room.

The only other sources of liquids that will be present in the cave are the waterline to the two film cooler pipe washout spray rings, and the melter water jacket and connecting piping. These clean water lines will be instrumented to detect leaks automatically. A rupture of either water line or a waste feed line would be an abnormal event and the liquid would be contained within the outer melter shield box and corrective measures would be initiated. Corrective action would start with closure of the supply line and draining of remaining water outside the melter shield box, and could require feed cutoff and melter idling or shut down. The amount of water that could be released into the containment building would be unlikely to exceed a few gallons, which would rapidly evaporate into the ambient air due to the high temperature in the cave under normal operating conditions.

LAW LSM Gallery Containment Building Structure

The LAW LSM gallery containment building will be a concrete walled structure-fully enclosed within the LAW vitrification plant. Therefore, structural requirements for the containment building will be met by the design standards of the LAW vitrification plant. The design will ensure that the unit has sufficient structural strength to prevent collapse or failure. The seismic requirements for the LAW vitrification plant are presented in the RPP WTP Compliance with Uniform Building Code Seismic Design Requirements, found in Supplement 1. Within the containment building will be partitions between the LSMs. DWP Attachment 51, Chapter 4, Supplement 1 provides documentation that the seismic requirements for the LAW vitrification plant meet or exceed the Uniform Building Code Seismic Design Requirements.

LAW LSM Gallery Containment Building Materials

The LAW LSM gallery containment building will be constructed of steel-reinforced concrete.

The interior floor and the walls of the unit will be covered with a protective coating. The roof of the LAW vitrification plant will consist of metal roofing, roof insulation, and a vapor barrier.

Rainwater run-on will be collected by roof drains and a drainage system with overflow drains.

- Use of Incompatible Materials for the LAW LSM Gallery Containment Building
- 44 A protective coating will be applied to the concrete floor and walls of the unit. The coating will
- 45 be compatible with the wastes that will be managed in the containment building. The wastes to

be managed will include LAW LSM melters and consumables, which may be metallic parts and failed equipment. Very little or no glass waste is expected to be present on the exterior of the LSM, due to the design of the melter. Reagents that could cause the liner to leak, corrode, or otherwise fail will not be used within the unit.

Primary Barrier Integrity in the LAW LSM Gallery Containment Building

The LAW LSM gallery containment building will be designed to withstand loads from the movement of personnel, wastes, and handling equipment. The seismic design criteria found in Supplement 1DWP Attachment 51, Supplement 1, ensures that appropriate design loads, load combinations, and structural acceptance criteria are employed at the WTP.

Certification of Design for the LAW LSM Gallery Containment Building

Prior to the start of operations, certification by a qualified registered professional engineer that the LAW LSM gallery containment building meets the design requirements of 40 CFR 264.1101(a), (b), and (c) will be obtained.

Operation of the LAW LSM Gallery Containment Building

Operational and maintenance controls and practices will be established and followed to ensure containment of the waste within the LAW LSM gallery containment building, as required by 40 CFR 264.1101(c)(1). Activities in the building will be remotely—conducted.

Maintenance of the LAW LSM Gallery Containment Building

The protectively-coated concrete floor of the containment building will be constructed and maintained in a manner that will be free of significant cracks, gaps, corrosion, or other deterioration. The concrete and protective coating will be free of corrosion or other deterioration because it will be compatible with materials that will be managed in the containment building, including the glass waste and containerized or uncontainerized waste and equipment.

 Measures to Prevent Tracking Wastes from the LAW LSM Gallery Containment Building
The unit is designed to manage LAW melters. The melters will be disconnected from systems when determined to be waste. The ports where the melter was attached to systems will be sealed and glass waste will be contained within the melter. This design will prevent waste from entering the containment building and thus from being tracked from the unit.

The unit will be classified as a C3 contamination area, which allows only limited personnel accessPersonnel access will be limited due to radiological concerns. Access will be required only for non-routine events such as when melters are determined to be waste, once every four 4 to five 5 years, or when equipment must be dismantled. The unit will be classified as a C3 contamination area, which allows only limited personnel access. Dry decontamination methods using cloth will be used.

Control of Fugitive Dust from the LAW LSM Gallery Containment Building

43 Operational controls and the LAW vitrification plant ventilation system will be used to control fugitive dust emissions from the unit to meet the requirements of 40 CFR 264.11101(c)(1)(iv).

The following measures will be used to prevent dust from escaping the LAW LSM gallery 1 2 containment building: 3 4 □A cascading air flow from areas of least to greatest potential contamination (i.e., C2 to C3 to 5 C5) 6 Greater negative air pressure in the unit compared to adjacent C2 units, to pull air into the unit 7 and prevent backflow 8 □Intake air through controlled air in bleed units, with backflow prevention dampers, and air 9 gaps around shield doors sized to prevent backflow □Dual HEPA-filtration of exhaust air before discharge to the atmosphere through a monitored 10 11 stack 12 □A multiple fan extraction system, designed to maintain negative pressure and cascading air 13 flow, even during fan maintenance and repair □Personnel ingress and egress through airlocks and subchange rooms 14 15 16 Procedures in the Event of Release or Potential for Release from the LAW LSM Gallery 17 Containment Building Conditions that could lead to a release from the LAW LSM gallery containment building will be 18 19 corrected as soon as possible after they are identified. The ventilation system and airlocks, the most likely sources of potential releases, are designed with two stages of HEPA filters, with 20 21 backup HEPA filters to facilitate repairs and replacement. 22 23 In the unlikely event of a release of dangerous wastes from the containment building, actions 24 required by 40 CFR 264.1101(c)(3)(i) through (iii) will be taken. Specific administrative and 25 operating methods that will be used to satisfy this requirement will be developed prior to the start of operations. The methods will be followed to repair conditions that could lead to a release. 26 27 28 Inspections of the LAW LSM Gallery Containment Building 29 An inspection program will be established to detect conditions that could lead to release of wastes from the LAW LSM gallery containment building. The inspection and monitoring 30 31 schedule and methods that will be used to detect releases from the unit are included in Chapter 6. 32 33 4.2.4.6 ILAW Container Finishing Line Containment Building (L-0109B, L-01/09C, L/-01 34 09D, L-0109E, L/-0115B, L/-0115C, L-0/15D, L-01/165E/16A/16B) The ILAW container finishing line containment building will be located in the LAW vitrification 35 36 plant. It will be used for managing ILAW containers that have cooled sufficiently to be closed and prepared for finishing. Typical waste management activities performed in this containment 37 38 building include storage of uncontainerized waste and decontamination. An ILAW container is transported from an inert filling room to a and lidding room, to a decontamination room, and 39 40 finally to a swab and monitor room, to a fixative application room as necessary, and then out of the containment building. This sequence of rooms is considered a finishing line. There are two 41 finishing lines within the ILAW container finishing line containment building. 42

- 1 ILAW Container Finishing Containment Building Design
- 2 The ILAW container finishing containment building will be completely enclosed within the
- 3 LAW vitrification plant. It will be designed to prevent the release and exposure of dangerous
- 4 constituents to the outside environment. The design and construction of the LAW vitrification
- 5 plant exterior will prevent water from running into the plant. The roof of the LAW vitrification
- 6 plant will consist of metal roofing, roof insulation, and a vapor barrier. Roof drains and drainage
- 7 system with overflow drains will collect run-off. The approximate dimensions of the unit are
- 8 summarized in Table 4-12.

9 . 10

- ILAW Container Finishing Containment Building Structure
- 11 Because the ILAW container finishing containment building will be a concrete-walled structure
- 12 fully enclosed within the LAW vitrification plant, its structural requirements will be met by the
- design standards of the LAW vitrification plant. The design will ensure that the unit has
- sufficient structural strength to prevent collapse or failure. DWP Attachment 51, Chapter 4,
- 15 Supplement 1 Supplement 1 provides documentation that the seismic requirements for the LAW
- vitrification plant meet or exceed the Uniform Building Code Seismic Design Requirements. The
- 17 seismic requirements for the LAW vitrification plant are presented in the RPP-WTP Compliance
- 18 with Uniform Building Code Scismic Design Requirements, found in Supplement 1.

19 20

- ILAW Container Finishing Containment Building Materials
- 21 The ILAW container finishing containment building will be constructed of steel-reinforced
- 22 concrete. The primary barrier of the inert filling rooms, lid scaling rooms, and swab and
- 23 monitor rooms is the concrete structure of the unit. The interior floor and a portion of the walls
- 24 of the decontamination rooms will be lined with a protective coating.

25 26

The roof of the LAW vitrification plant will consist of metal roofing, roof insulation, and a vapor barrier. Roof drains and drainage system with overflow drains will collect run on.

27 28 29

- Use of Incompatible Materials for the ILAW Container Finishing Containment Building
- The primary barrier will have a protective coating. This coating will be compatible with the waste managed in the unit. The waste to be managed includes vitrified waste glass within the
- waste managed in the unit. The waste to be managed includes vitrified waste glass within the stainless steel containers. This coating will be present in the two inert fill rooms, the fixative
- 33 application room, and the two swab and monitor rooms.

34

- 35 A protective coating will be present in the decontamination rooms. The coating will be
- 36 compatible with the wastes that will be managed, which will include filled ILAW containers. No
- 37 glass waste is expected to be present on the exterior of the containers, due to the design of the
- 38 melter pour stations. The interior is the only portion of the container that will be exposed to the
- 39 glass waste. Additionally, the removal of glass will occur in the inert fill and lidding rooms.
- 40 Carbon dioxide pellets, also compatible with the stainless steel, will be used to remove
- 41 contamination from the container surface.

42

Reagents that could cause the liner to leak, corrode, or otherwise fail will not be used within the unit.

Primary Barrier Integrity in the ILAW Container Finishing Containment Building 1

The ILAW containment building will be designed to withstand loads from the movement of 2 3

- personnel, wastes, and handling equipment. The seismic design criteria found in Supplement
- 4 4DWP Attachment 51, Supplement 1, ensures that appropriate design loads, load combinations,

5 and structural acceptance criteria are employed at the WTP.

6 7

- Certification of Design for the ILAW Container Finishing Containment Building
- 8 Prior to start of operations, certification by a qualified registered professional engineer that the
- ILAW containment building meets the design requirements of 40 CFR 264.1101(a) and (c) will 9
- be obtained. The requirements of 40 CFR 264.1101(b) do not apply to this design because the 10
- waste managed in the unit will not contain free liquids and free liquids will not be used to treat 11
- the waste. 12

13 14

- Operation of the ILAW Container Finishing Containment Building
- 15 Operational and maintenance controls and practices will be established to ensure containment of
- the waste within the ILAW containment building, as required by 40 CFR 264.1101(c)(1). 16
 - Activities in the building will be remotely conducted.

17 18 19

- Maintenance of the ILAW Container Finishing Containment Building
- 20 The protectively coated concrete floor and walls of the of the containment building will be
- 21 constructed and maintained in a manner that will be free of significant cracks, gaps, corrosion, or
- 22 other deterioration. The coated concrete will be free of corrosion or other deterioration because
- 23 it will be compatible with materials that will be managed in the containment building, which will
- 24 include glass waste and containerized waste and equipment.

25 26

- The protective coating in the decontamination rooms will be constructed and maintained in a
- manner that will be free of significant cracks, gaps, corrosion, or other deterioration. The 27
- 28 coating will remain free of corrosion or other deterioration because it will be compatible with
- 29 materials that will be managed in the containment building, which will include failed equipment.
- Wastes managed in the containment building will not be stacked. 30

31

- Measures to Prevent Tracking Wastes from the ILAW Container Finishing Containment 32
- 33 Building
- The ILAW containment building is designed to sample, seal, and decontaminate the filled ILAW 34
- 35 containers. Conducting these activities in a C3 zone prevents the spread of contaminated
- materials from the unit as air flow is managed in the LAW vitrification plant ventilation system. 36
- 37 The containment building is under negative pressure, so no air flow through doors or other
- openings occurs. Air flow through this containment building goes to a C5 air system, which 38
- 39 passes through HEPA filters before exiting the plant stack.

- A vacuum cleanup system, located in the two inert fill rooms, is expected to be infrequently used 41
- 42 to collect dust from the inert filling activities, and thereby minimize the potential for dust to be
- 43 tracked from the unit. The dust will be disposed of as secondary waste. Additionally, personnel
- 44 access to the containment building, which is classified as a C3 contamination area, will be

1	limited due to radiological concerns. Access to the unit will be allowed only under limited
2	circumstances, reducing the potential for contacting the waste and tracking it from the unit.
3	
4	Control of Fugitive Dust from the ILAW Container Finishing Containment Building
5	The following measures will be used to prevent fugitive dust from escaping the containment
6	building:
7	
8	☐A HEPA filtered vacuum system will be dedicated to each decontamination room to collect
9	debris
10 11	☐A caseading air flow from areas of least to greatest potential contamination (i.e., C2 to C3 to C5)
12	Greater negative air pressure in the unit, compared to adjacent C2 units, to pull air into the unit
13	and prevent backflow
14	UIntake air through controlled air in bleed units, with backflow prevention dampers, and air
15	gaps around shield doors sized to prevent backflow
16	□Safety interlocks to shut down C3 extraction fans to prevent backflow if the C5 system shuts
17	down
18	□Dual HEPA filtration of exhaust air before discharge to the atmosphere through a monitored
19	stack
20	☐A multiple fan extraction system, designed to maintain negative pressure and cascading air
21	flow, even during fan maintenance and repair
22	Dersonnel ingress and egress through airlocks and subchange rooms
23	
24	Procedures in the Event of Release or Potential for Release from the ILAW Container Finishing
25	Containment Building
26	Conditions that could lead to a release from the ILAW containment building will be corrected as
27	soon as possible after they are identified. The ventilation system and airlocks, the most likely
28	sources of potential releases, will incorporate two stages of HEPA filters, with backup HEPA
29	filters to facilitate repairs and replacement.
30	
31	In the unlikely event of a release of dangerous wastes from the containment building, actions
32	required by 40 CFR 264.1101(c)(3)(i) through (iii) will be taken. Specific administrative and
33	operating methods to satisfy this requirement will be developed prior to the start of operations.
34	The methods will be followed to repair conditions that could lead to a release.
35	
36	Inspections of the ILAW Container Finishing Containment Building
37	An inspection program will be established to detect conditions that could lead to a release of
38	wastes from the ILAW container finishing containment building. The inspection and monitoring
39	schedule and methods that will be used to detect releases from the unit are included in Chapter 6.
40	

4.2.4.7 LAW Vitrification Plant C3 Workshop Consumable Import/Export Containment Building (L-0119B)

The LAW vitrification plant C3-workshopconsumable import/export containment building will be located in the northwestern portion west end of the LAW vitrification plant on the +3 ft elevation. Typical waste management activities performed in this containment building include,

decontamination, size reduction, and packaging of spent equipment. Simple decontamination of components will be performed to allow contact handling. Waste streams generated within the

workshop will be volume reduced as necessary by means of disassembly or other suitable means 8 to fit standard packaging such as drums and/or small boxes. 9

10 11

1 2

3

4

5

6

7

LAW Vitrification Plant C3 Workshop Consumable Import/Export Containment Building Design

The LAW vitrification plant C3 workshop consumable import/export containment building will 12

be designed as a completely enclosed area within the LAW vitrification plant. It is designed to 13

prevent the release of dangerous constituents and their exposure to the outside environment. The 14 15

design and construction of the LAW vitrification plant exterior will prevent water from running into the plant. The roof of the LAW vitrification plant will consist of metal roofing, roof 16

insulation, and vapor barrier. Rainwater run-off will be collected by roof drains and drainage 17

systems with overflow roof drains. The approximate dimensions of the unit are summarized in 18

19 Table 4-12.

20 21

22

LAW Vitrification Plant C3 Workshop Consumable Import/Export Containment Building Structure

23 The LAW vitrification plant C3-workshopconsumable import/export containment building will

be a concrete-walled structure fully enclosed within the LAW vitrification plant. Therefore, 24 25

structural requirements for the containment building will be met by the design standards of the LAW vitrification plant. The design will ensure that the unit has sufficient structural strength to 26

27 prevent collapse or failure. DWP Attachment 51, Chapter 4, Supplement 1Supplement 1

provides documentation that the seismic requirements for the LAW vitrification plant meet or 28 29

exceed the Uniform Building Code Seismic Design Requirements. The seismic requirements for the LAW vitrification plant are presented in the RPP-WTP Compliance with Uniform Building 30

Code Seismic Design Requirements, as foundlocated in Attachment 51, Chapter 4, Supplement 1.

31 32 33

34

LAW Vitrification Plant C3 Workshop Consumable Import/Export Containment Building Materials

The LAW vitrification plant C3 workshop consumable import/export containment building will 35

be constructed of steel-reinforced concrete. The interior floor and a portion of the walls of the 36

unit will be lined with a protective coating. The roof of the LAW vitrification plant will consist 37

of metal roofing, roof insulation, and vapor barrier. Rainwater run off will be collected by roof 38

drains and drainage systems with overflow roof drains. 39

- Use of Incompatible Materials in the LAW Vitrification Plant C3 Workshop Consumable Import/ 41 42 **Export Containment Building**
- A protective coating will be provided for the floor of this unit. The protective coating will be 43
- eempatible with the wastes that will be managed. Activities in the unit will be limited to 44
- decontamination, size reduction, and packaging the waste components into drums or waste 45

boxes. Treatment reagents that could cause the liner or coating to leak, corrode, or otherwise fail 1 2 will not be used within the unit. 3 4 Primary Barrier Integrity in the LAW Vitrification Plant C3 Workshop Consumable Import/ 5 **Export Containment Building** The LAW vitrification plant C3 workshop consumable import/export containment building will 6 be designed to withstand loads from the movement of personnel, wastes, and handling 7 equipment. The seismic design criteria found in Supplement 1DWP Attachment 51, Supplement 8 1, ensures that appropriate design loads, load combinations, and structural acceptance criteria are 9 10 employed at the WTP. 11 Certification of Design for the LAW Vitrification Plant C3 Workshop Consumable Import/Export 12 13 Containment Building Prior to startup of operations, a certification by a qualified registered professional engineer that 14 the LAW vitrification plant C3 workshop consumable import/export containment building meets 15 16 the design requirements of 40 CFR 264.1101(a), (b), and (c) will be obtained. 17 18 Operation of the LAW Vitrification Plant C3-Workshop Consumable Import/Export Containment 19 Building 20 Operational and maintenance controls and practices will be established and followed to ensure 21 containment of the wastes within the LAW vitrification plant C3 containment building unit as required by 40 CFR 264.1101(c)(1). 22 23 Maintenance of the LAW Vitrification Plant C3 Workshop Consumable Import/Export 24 25 Containment Building The protective coating of the unit will be constructed and maintained in a manner that will be 26 free of significant cracks, gaps, corrosion, or other deterioration. The protective coating will 27 remain free of corrosion or other deterioration because it is compatible with materials that will be 28 29 managed in the containment building. The failed equipment that will be managed in the containment building unit will be compatible with stainless steel or the protective coating. Only 30 decontamination chemicals that are compatible with the liner or coating will be used the concrete 31 32 structure. 33 Measures to Prevent Tracking Wastes from the LAW Vitrification Plant C3 34 35 Workshop Consumable Import/Export Containment Building The LAW vitrification plant C3 workshop consumable import/export containment building will 36 be designed to isolate failed equipment from the accessible environment and to prevent the 37 spread of contaminated materials. Very little dust is expected to be generated in the unit. 38 39 Personnel access to tThe containment building will be limited due to radiological concerns. It 40 will be classified as a C3 contamination area, which allows only limited access by personnel. 41 42 Wastes leaving the unit will be enclosed within containers. If necessary, these containers will be decontaminated in the unit and subjected to radiological survey prior to release and 43

transportation to another permitted storage area. Equipment leaving the unit will be

decontaminated, when necessary, before being released for removal from the cells.

44

1.	
2	Control of Fugitive Dust from the LAW Vitrification Plant C3 Workshop Containment Building
3.	The following measures will be used to prevent fugitive dust from escaping the LAW
4	vitrification plant C3 workshop containment building:
5	,
6	☐A cascading air flow from areas of least to greatest potential contamination (that is, C2 to C3 to
7	C5)
8	□Intake air through controlled air in bleed units, with backflow prevention dampers, and air
9	gaps around shield doors sized to prevent backflow
10	on the control of the
	The HEPA filtration of exhaust air before discharge to the atmosphere through a monitored stack
11	A multiple fan extraction system designed to maintain negative pressure and cascading air
12	flow, even during fan maintenance and repair
13	
14	Procedures in the Event of Release or Potential for Release from the LAW Vitrification Plant C3
15	Workshop Consumable Import/Export Containment Building
16	The design and operation of the unit makes it very unlikely that releases will occur. The design
17	and operational measures will minimize the generation of dust and contain it within the unit.
18	The ventilation system will also use negative air pressure to keep contamination from spreading
19	to areas of lesser contamination, and will use two stage HEPA filtration to reduce the release of
20	particles. The ventilation system is designed with backup HEPA filters to provide redundant
21	controls and to facilitate repairs or replacement.
22	
23	Inspections will identify conditions that could lead to a release. Such conditions will be
24	corrected as soon as possible after they are identified. In the unlikely event that a release of
25	dangerous wastes from the containment building is detected, actions required by
26	40 CFR 264.1101(c)(3)(i) through (iii) will be taken. Specific administrative and operating
27	methods that will be used to satisfy this requirement will be developed prior to the start of
28	operations. These methods will be followed to repair conditions that could lead to a release.
29	
30	Inspections of the LAW Vitrification Plant C3 Workshop Consumable Import/Export
31	Containment Building
32	An inspection program will be established to detect conditions that could lead to a release of
33	wastes from the LAW vitrification plant C3 workshop consumable import/export containment
34	building. The inspection and monitoring schedule and methods that will be used to detect
35	releases from the unit is are included in Chapter 6.
36	40.40
37	4.2.4.8 C3 Workshop Containment Building (L-226A)
38	The C3 workshop containment building will be leasted in the annual side of the Taxxx 's in
39	The C3 workshop containment building will be located in the west side of the LAW vitrification plant at elevation +28 feet.
40	<u>Pictur at 0197 atti011 → 20 1666.</u>
41	Typical waste management activities performed in this containment building include
12	decontamination, size reduction, and packaging of spent equipment. Equipment will be
12	transported to the smit and in 1: 11 11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1

1	workshop, the equipment will be decontaminated to enable "hands-on" maintenance. Spent
2	equipment parts will be bagged and placed in standard waste containers or boxes for disposal.
3	Size reduction may be performed to facilitate packaging. Other spent equipment will be
4	packaged in drums or standard waste boxes.
5	
6	C3 Workshop Containment Building Design
7	The C3 workshop containment building will be a completely enclosed area within the LAW
8	vitrification plant. It will be designed to prevent the release of dangerous waste and their
9	exposure to the outside environment. The design and construction of the LAW vitrification plant
10	exterior will prevent water from running into the plant. The roof of the LAW vitrification plant
11	will consist of metal roofing, roof insulation, and vapor barrier. Rainwater run-off will be
12	collected by roof drains and drainage systems with overflow roof drains. The approximate
13	dimensions of the unit are summarized in Table 4-12.
14	
15	C3 Workshop Containment Building Structure
16	The C3 workshop containment building will be fully enclosed within the LAW vitrification
17	plant. Therefore, structural requirements for the containment building will be met by the design
18	standards of the LAW vitrification plant. The design will ensure that the unit has sufficient
19	structural strength to prevent collapse or failure. DWP Attachment 51, Chapter 4, Supplement
20	1Supplement 1 provides documentation that the seismic requirements for the LAW vitrification
21	plant meet or exceed the Uniform Building Code Seismic Design Requirements. The seismic
22	requirements for the LAW vitrification plant are presented in RPP-WTP Compliance with
23	Uniform Building Code Seismic Design Requirements, found in Supplement 1.
24	
25	C3 Workshop Containment Building Materials
26	The C3 workshop containment building will be constructed of a steel-reinforced concrete floor
27	and plasterboard partition walls. The primary barrier of the pour cave is the concrete structure of
28	the unit. The roof of the LAW vitrification plant will consist of metal roofing, roof insulation,
29 .	and vapor barrier. Rainwater run-off will be collected by roof drains and drainage systems with
30	overflow roof drains.
31	TT CT CT CT CT TT CT CT CT CT CT CT CT C
32	Use of Incompatible Materials in the C3 Workshop Containment Building
33	Activities in the unit will be limited to decontamination, size reduction, and packaging the waste
34	components into drums or waste boxes. Treatment reagents that could cause the liner or coating
35	to leak, corrode, or otherwise fail will not be used within the unit.
36	
37	Primary Barrier Integrity in the C3 Workshop Containment Building
38	The C3 workshop containment building is designed to withstand loads from the movement of
39	personnel, wastes, and handling equipment. The seismic design criteria found in Supplement
40	1DWP Attachment 51, Supplement 1, ensures that appropriate design loads, load combinations,
41	and structural acceptance criteria are employed at the WTP.
42	Contification of Decien for the C2 West-ton Continued Delision
43 44	Certification of Design for the C3 Workshop Containment Building Prior to startup of operations, a certification by a gualified registered professional engineer that

the C3 workshop containment building meets the design requirements of 40 CFR 264.1101(a)

and (c) will be obtained. The requirements of 40 CFR 264.1101(b) do not apply to this design 1 2 because the waste managed in the unit will not contain free liquids or be treated with free liquids. 3 4 Operation of the C3 Workshop Containment Building 5 Operational and maintenance controls and practices will be established and followed to ensure 6 containment of the wastes within the C3 workshop containment building unit as required by 7 40 CFR 264.1101(c)(1). 8 9 Maintenance of the C3 Workshop Containment Building 10 The concrete will be constructed and maintained in a manner that will be free of significant 11 cracks, gaps, corrosion, or other deterioration. The concrete will remain free of corrosion or 12 other deterioration because it is compatible with materials that will be managed in the containment building. The failed equipment that will be managed in the containment building 13 14 unit will be compatible with the concrete. Only decontamination chemicals that are compatible 15 with the concrete will be used. 16 Measures to Prevent Tracking Wastes from the C3 Workshop Containment Building 17 The C3 workshop containment building will be designed to isolate failed equipment from the 18 19 accessible environment and to prevent the spread of contaminated materials. Very little dust is 20 expected to be generated in the unit. 21 22 Personnel access to tThe containment building will be limited due to radiological concerns. It 23 will be classified as a C3 contamination area, which allows only limited access by personnel. 24 Personnel access will be via a C2/C3 subchange room. Equipment will enter and exit the 25 workshop via a C2/C3 airlock. Wastes leaving the unit will be enclosed within containers. If 26 necessary, the containers will be decontaminated in the unit prior to transportation to a permitted storage area. Equipment leaving the unit will be decontaminated, when necessary, before being 27 28 released for removal from the cells. 29 30 Procedures in the Event of Release or Potential for Release from the C3 Workshop Containment 31 Building The design and operation of the unit makes it very unlikely that releases will occur. The design 32 and operational measures will minimize the generation of dust and contain it within the unit. 33 34 The ventilation system will also use negative air pressure to keep contamination from areas of lesser contamination. Offgas will be routed to the LAW offgas treatment system. 35 36 37 Inspections will identify conditions that could lead to a release. Such conditions will be 38 corrected as soon as possible after they are identified. In the unlikely event that a release of 39 dangerous wastes from the containment building is detected, actions required by 40 CFR 264.1101(c)(3)(i) through (iii) will be taken. Specific administrative and operating 40 methods that will be used to satisfy this requirement will be developed prior to the start of 41

51-4-210

operations. These methods will be followed to repair conditions that could lead to a release.

42

1	Inspections of the C3 Workshop Containment Building
2	An inspection program will be established to detect conditions that could lead to a release of
3	wastes from the C3 workshop containment building. The inspection and monitoring schedule
4	and methods that will be used to detect releases from the unit is are included in Chapter 6.
5	
6	4.2.4.9 LAW Pour Cave Containment Building (L-B009B, L-B011B, L-B011C,
7	L-B013B, L-B013C, L-B0415A)
8	The LAW pour cave containment building (rooms L-B009B, L-B011B, L-B011C, L-B013B,
9	L-B013C, L-B0415A) will be located in the LAW vitrification plant, elevation -21 ft. It will be
10	used for managing ILAW containers as they are filled with glass from the LAW mMelters
11	(LAW-MLTR-00001/2). The filled ILAW containers will be allowed to cool with the lids off
12	the container. Cooled ILAW containers will be transferred to the ILAW container finishing line
13	containment building for lidding and preparation for export to a storage facility.
14	
15	LAW Pour Cave Containment Building Design
16	The LAW pour cave containment building will be completely enclosed within the LAW
17	vitrification plant, which will be designed to prevent the release and exposure of dangerous
18	constituents to the outside environment. The design and construction of the LAW vitrification
19	plant exterior will prevent precipitation from entering into the plant. The roof of the LAW
20	vitrification plant will consist of metal roofing, roof insulation, and a vapor barrier. Roof drains
21	and drainage system with overflow drains will collect run-off. The approximate dimensions of
22	the unit are summarized in Table 4-12.
23	
24	LAW Pour Cave Containment Building Structure
25	Because the LAW pour cave containment building will be a concrete-walled structure fully
26	enclosed within the LAW vitrification plant, its structural requirements will be met by the design
27	standards of the LAW vitrification plant. The design will ensure that the unit has sufficient
28	structural strength to prevent collapse or failure. DWP Attachment 51, Chapter 4, Supplement
29	1 Supplement 1 provides documentation that the seismic requirements for the LAW vitrification
30	plant meet or exceed the Uniform Building Code Seismic Design Requirements. The seismic
31	requirements for the LAW vitrification plant are presented in the RPP WTP Compliance with
32	Uniform Building Code Scismic Design Requirements, found in Supplement 1.
33	
34	LAW Pour Cave Containment Building Materials
35	The LAW pour cave containment building will be constructed of steel-reinforced concrete. The
36	primary barrier of the pour caves is the concrete structure of the unit. The roof of the LAW
37	vitrification plant will consist of metal roofing, roof insulation, and a vapor barrier. Roof drains
38	and drainage system with overflow drains will collect run-off.
39	
40	Use of Incompatible Materials for the LAW Pour Cave Containment Building
41	The waste to be managed includes vitrified waste glass within the stainless steel containers. No
42	glass waste is expected to be present on the exterior of the containers, due to the design of the
43 44	melter pour stations. The interior is the only portion of the container that will be exposed to the
4141	mit add within the limit to the failure articles are corrected agual and are singuled within the limit

2	Primary Barrier Integrity in the LAW Pour Cave Containment Building
3	The LAW pour cave containment building will be designed to withstand loads from the
4	movement of personnel, wastes, and handling equipment. The seismic design criteria found in
5	the RPP-WTP Compliance with Uniform Building Code Seismic Design Requirements,
6	Supplement 1DWP Attachment 51, Supplement 1, ensures that appropriate design loads, load
7	combinations, and structural acceptance criteria are employed at the WTP.
8	
9	Certification of Design for the LAW Pour Cave Containment Building
10	Prior to start of operations, certification by a qualified registered professional engineer that the
11	LAW pour cave containment building meets the design requirements of 40 CFR 264.1101(a) and
12	(c) will be obtained. The requirements of 40 CFR 264.1101(b) do not apply to this design
13	because the waste managed in the unit will not contain free liquids and free liquids will not be
14	used to treat the waste.
15	
16	Operation of the LAW Pour Cave Containment Building
17	Operational and maintenance controls and practices will be established to ensure containment of
18	the waste within the LAW pour cave containment building, as required by 40
19	CFR 264.1101(c)(1). Activities in the building will be remotely conducted during normal
20	operation when ILAW containers are present.
21	
22	Maintenance of the LAW Pour Cave Containment Building
23	The concrete will be free of corrosion or other deterioration because it will be compatible with
24	materials that will be managed in the containment building, which will include containerized
25	glass waste and equipment. Wastes managed in the containment building will not be stacked.
26	
27	Measures to Prevent Tracking Wastes from the LAW Pour Cave Containment Building
28	The LAW pour cave containment building is designed to manage the filling and movement of
29	ILAW containers. Conducting these activities in a C5 zone prevents the spread of contaminated
30	materials from the unit as airflow is managed in the LAW vitrification plant ventilation system.
31	The containment building is under negative pressure. Airflow through this containment building
32	goes to a C5 air system, which passes through HEPA filters before exiting the plant stack.
33	Personnel access will be restricted during normal operation since it is classified as a C5
34	contamination area. The containment building may be reclassified as a C3 area for equipment
35	maintenance.
36	
37	Procedures in the Event of Release or Potential for Release from the LAW Pour Cave
38	Containment Building
.39	Conditions that could lead to a release from the LAW pour cave containment building will be
40	corrected as soon as possible after they are identified. In the unlikely event of a release of
41	dangerous wastes from the containment building, actions required by 40 CFR 264.1101(c)(3)(i)
42	through (iii) will be taken. Specific administrative and operating methods to satisfy this
43	requirement will be developed prior to the start of operations. The methods will be developed to
44	repair conditions that could lead to a release.
45	

1	inspections of the LAW Four Cave Contaminent Building
2	An inspection program will be established to detect conditions that could lead to a release of
3	wastes from the LAW pour cave containment building. The inspection and monitoring schedule
4	and methods that will be used to detect releases from the unit are included in Chapter 6.
5	
6	4.2.4.10 LAW Container Buffer Storage Containment Building (L-B025C, L-B025D)
7	The LAW container buffer storage containment building (rooms L-B025C, L-B0025D) will be
8	located in the LAW vitrification plant, elevation -21 ft. It will be used for managing ILAW
9	containers as after they are filled with glass from the LAW Melters (LAW-MLTR-00001/2).
10	The filled ILAW containers will be allowed to cool with the lids off the container. Cooled
11	ILAW containers will be transferred to the ILAW container finishing line containment building
12	for lidding and preparation for export to a storage facility.
13	
14	LAW Container Buffer Storage Containment Building Design
15	The LAW container buffer storage containment building will be completely enclosed within the
16	LAW vitrification plant, which will be designed to prevent the release and exposure of
17	dangerous constituents to the outside environment. The design and construction of the LAW
18	vitrification plant exterior will prevent precipitation from entering into the plant. The roof of the
19	LAW vitrification plant will consist of metal roofing, roof insulation, and a vapor barrier. Roof
20	drains and drainage system with overflow drains will collect run-off. The approximate
21	dimensions of the unit are summarized in Table 4-12.
22	
23	LAW Container Buffer Storage Containment Building Structure
24	Because the LAW container buffer storage containment building will be a concrete-walled
25	structure fully enclosed within the LAW vitrification plant, its structural requirements will be
26 .	met by the design standards of the LAW vitrification plant. The design will ensure that the unit
27	has sufficient structural strength to prevent collapse or failure. DWP Attachment 51, Chapter 4.
28	Supplement 1 provides documentation that the seismic requirements for the LAW
29	vitrification plant meet or exceed the Uniform Building Code Seismic Design Requirements.
30	
31	LAW Container Buffer Storage Containment Building Materials
32	The LAW container buffer storage containment building will be constructed of steel-reinforced
33	concrete.
34	
35	Use of Incompatible Materials for the LAW Container Buffer Storage Containment Building
36	The waste to be managed includes vitrified waste glass within the stainless steel containers. No
37	glass waste is expected to be present on the exterior of the containers. The interior is the only
38	portion of the container that will be exposed to the glass waste. Reagents that could cause
39	corrosion or other failure will not be used within the unit.
40	
41	Primary Barrier Integrity in the LAW Container Buffer Storage Containment Building
42	The LAW container buffer storage containment building will be designed to withstand loads
43	from the movement of personnel, wastes, and handling equipment. The seismic design criteria
44	found in RPP-WTP Compliance with Uniform Building Code Seismic Design Requirements

1	Supplement 1DWP Attachment 51, Supplement 1 ensures that appropriate design loads, load
2	combinations, and structural acceptance criteria are employed at the WTP.
3	
4	Certification of Design for the LAW Container Buffer Storage Containment Building
5	Prior to start of operations, certification by a qualified registered professional engineer that the
6	LAW container buffer storage containment building meets the design requirements of 40
.7	CFR 264.1101(a) and (c) will be obtained. The requirements of 40 CFR 264.1101(b) do not
8	apply to this design because the waste managed in the unit will not contain free liquids and free
9	liquids will not be used to treat the waste.
10	
11	Operation of the LAW Container Buffer Storage Containment Building
12	Operational and maintenance controls and practices will be established to ensure containment of
13	the waste within the LAW container buffer storage containment building, as required by 40
14	CFR 264.1101(c)(1). Activities in the building will be remotely conducted during normal
15	operation when ILAW containers are present.
16	
17	Maintenance of the LAW Container Buffer Storage Containment Building
18	The concrete will be free of corrosion or other deterioration because it will be compatible with
19	materials that will be managed in the containment building, which will include containerized
20	glass waste and equipment. Wastes managed in the containment building will not be stacked.
21	
22	Measures to Prevent Tracking Wastes from the LAW Container Buffer Storage Containment
23	Building
24	The LAW container buffer storage containment building is designed to manage the movement
25	and storage of ILAW containers. Conducting these activities in a C5 zone prevents the spread o
26	contaminated materials from the unit as airflow is managed in the LAW vitrification plant
27	ventilation system. The containment building is under negative pressure. Airflow through this
28	containment building goes to a C5 air system, which passes through HEPA filters before exiting
29	the plant stack. Personnel access will be restricted during normal operation since it is classified
30	as a C5 contamination area. The containment building may be reclassified as a C3 area for
31	equipment maintenance.
32	
33	Procedures in the Event of Release or Potential for Release from the LAW Container Buffer
34	Storage Containment Building
35	Conditions that could lead to a release from the LAW container buffer storage containment
36	building will be corrected as soon as possible after they are identified. In the unlikely event of a
37	release of dangerous wastes from the containment building, actions required by
38	40 CFR 264.1101(c)(3)(i) through (iii) will be taken. Specific administrative and operating
39	methods to satisfy this requirement will be developed prior to the start of operations. The
40	methods will be developed to repair conditions that could lead to a release.
41	
42	Inspections of the LAW Container Buffer Storage Containment Building
43	An inspection program will be established to detect conditions that could lead to a release of
44	wastes from the LAW container buffer storage containment building. The inspection and

monitoring schedule and methods that will be used to detect releases from the unit are included in Chapter 6.

б

1 2

<u>4.2.4.104.2.4.11</u> HLW Melter Cave No. 1 Containment Building (H-0117, H-0116B, H-0310A) and HLW Melter Cave No. 2 Containment Buildings (H-0117, H-0116B, H-0116B, H-0310A and (H-0106, H-0105B, H-0304A)

There are six containment buildings located within the HLW vitrification plant. The HLW melter cave no. 1 and HLW melter cave no. 2 containment buildings are located in the central portion of the HLW vitrification plant. The each of the containment buildings will be compriosed of house an the HLW melter caves, and the an overpack C3/C5 airlocks, and the equipment decontamination area.

Typical waste management activities performed in these containment buildings include, the dismantling and packaging of spent consumables, and decontamination of equipment for hands-on maintenance. The types of spent consumables will include waste recirculators, lid heaters, bubblers, and thermocouples, and jumpers. When spent consumables are ready for change-out, they will be placed on a consumable storage rack while awaiting size reduction. The consumables will be reduced in size by dismantling or cutting the spent equipment, or both. This process will be remotely-conducted on tables in the containment building. The spent consumables will be placed in baskets and lowered into containers in a transfer tunnel that passes under the HLW melter cave no. 1 and 2 containment buildings (H-0117, H-0116B, H-0310A and H-0106, H-0105B, H-0304A). The C3/C5 airlocks eells-will be used for packing or unpacking melters or their components.

In case of a HLW melter failure, the melter will be evaluated for meeting the receiving TSD waste acceptance criteria, particularly in terms of the radiological contamination in the HLW glass residue present in the melter, before it is placed in an overpack.

 The equipment decontamination area located within the melter cave containment building will house the dDecontamination tTanks (HSH-TK-00001/2) where equipment removed from the melter cave will be decontaminated prior to maintenance. The equipment will be initially decontaminated by soaking in the decontamination tank. After evaluation, additional decontamination may be performed using manipulators before the levels are acceptable for hands-on maintenance.

Located within the melter caves containment building will be the HLW melter; the submerged bed scrubber and HEMEs, which will function as part of the melter offgas systems, the feed preparation Preparation tank-Vessels (HFP-VSL-00001/5).; and the HLW Melter Ffeed tank Vessels (HFP-VSL-00002/6). These tank systems will have primary and secondary containment, and are addressed section 4.2.2. Therefore, there is no need for secondary containment within the containment building, as the tank systems meet the requirements of WAC 173 303 640.

HLW Melter Cave No. 1 and HLW Melter Cave No. 2 Containment Building Design 1

The two HLW melter containment buildings are completely enclosed within the HLW 2

- 3 vitrification plant. Each unit of the melter cave containment buildings will comprise thehouse an
- HLW melter cave, and thean overpack C3/C5 airlock cell, and an equipment decontamination 4
- 5 area. Each Both melter cave containment buildings unit is are designed to prevent the release of
- dangerous constituents and exposure to the outside environment. The design and construction of 6
- 7 the HLW vitrification plant exterior will prevent water from running into the plant. The roof of
- 8 the HLW vitrification plant will be metal. Run-off will be collected by roof drains and a
- 9 drainage system with overflow roof drains.

10 11

12

13 14

15

16

17

18

The only other sources of liquids that will be present in the caves is the water line to the two film cooler pipe washout spray rings, and the melter water jacket and connecting piping. These clean water lines will be instrumented to detect leaks automatically. A rupture of either water line would be an abnormal event and would require corrective measures. Corrective action would start with closure of the supply line and draining of remaining water outside the caves, and could require feed cutoff and melter idling or shut down. The amount of water that could be released in the containment building would be unlikely to exceed a few gallons, which would rapidly evaporate into the ambient air due to the high temperature in the caves under normal operating conditions.

19 20 21

22

The containment building design requirements of 40 CFR 264.1101(b) do not apply because the liquid dangerous wastes managed in the HLW melter containment building are addressed under tank systems (see Section 4.2.2).

23 24

HLW Melter Cave No. 1 and HLW Melter Cave No. 2 Containment Building Structure 25 The HLW melter cave no. 1 and 2 containment buildings will be a fully enclosed, 26 concrete-walled structure within the HLW vitrification plant. Therefore, its structural 27 28 requirements will be met by the design standards of the HLW vitrification plant. The design will

29 ensure that the unit has sufficient structural strength to prevent collapse or failure. DWP

- Attachment 51, Chapter 4, Supplement 1 provides documentation that the seismic 30 31
- requirements for the HLW vitrification plant meet or exceed the Uniform Building Code Seismic 32 Design Requirements. The seismic requirements for the HLW vitrification plant are found in the
- RPP-WTP Compliance with Uniform Building Code Scismic Design Requirements; found in 33
- 34 Supplement 1.

35 36

37 38 HLW Melter Cave No. 1 and HLW Melter Cave No. 2 Containment Building Materials The HLW melter cave no. 1 and 2 containment buildings will be constructed of steel-reinforced concrete. The interior floor and a portion of the walls of the unit will be lined with stainless steel, except for the C3/C5 airlock. The height of the lining is summarized in Table 4-11.

39 40 41

The roof of the HLW vitrification plant will consist of metal roofing, roof insulation, and a vapor barrier. Run-off will be collected by roof drains and a drainage system with overflow roof drains.

43 44

Use of Incompatible Materials for the HLW Melter Cave No. 1 and HLW Melter Cave No. 2 1 2 Containment Buildings A partial stainless steel liner will be provided for the containment buildings, except for the 3 C3/C5 airlock. The C3/C5 airlock will be partially lined with a protective coating. The stainless 4 steel will be compatible with the wastes that will be managed, which will include failed spent 5 melters and consumables, including air spargers, metallic parts, and refractory bricks. Treatment 6 7 reagents that could cause the liner to leak, corrode, or otherwise fail will not be used within the 8 unit. 9 10 Primary Barrier Integrity in the HLW Cave No. Melter 1 and HLW Melter Cave No. 2 11 Containment Buildings The HLW melter cave no. 1 and 2 containment buildings are designed to withstand loads from 12 13 the movement of personnel, wastes, and handling equipment. The seismic design criteria found in Supplement 1 DWP Attachment 51, Supplement 1, ensures that appropriate design loads, load 14 combinations, and structural acceptance criteria are employed at the WTP. 15 16 17 Certification of Design for the HLW Cave No. Melter 1 and HLW Melter Cave No. 2 18 Containment Buildings Prior to the start of operations, certification by a qualified registered professional engineer that 19 20 the HLW melter containment building meets the design requirements of 40 CFR 264.1101(a) and (c) will be obtained. The requirements of 40 CFR 264.1101(b) do not apply to this design 21 because liquid dangerous wastes present in the containment building will be managed in tank 22 systems with secondary containment systems, as presented in Section 4.2.2. 23 24 25 Operation of the HLW Melter Cave No. 1 and HLW Melter Cave No. 2 Containment Buildings Operational and maintenance controls and practices will be established and followed to ensure 26 containment of the wastes within the HLW melter containment building, as required by 27 28 40 CFR 264.1101(c)(1). 29 Maintenance of the HLW Melter Cave No. 1 and HLW Melter Cave No. 2 Containment 30 31 **Buildings** The partial stainless steel lining of the containment building will be designed and constructed 32 and maintained in a manner that will be free of significant cracks, gaps, corrosion, or other 33 34 deterioration. The liner will be welded at each seam. The stainless steel liner will be free of 35 corrosion or other deterioration because it will be compatible with materials that will be managed in the containment building, which will include failed spent melters and spent equipment. Only 36 decontamination chemicals that are compatible with the liner will be used. 37 38 Wastes managed in the containment building will not be stacked. In general, waste will be 39 placed in containers and removed from the containment building. 40

- 1 Measures to Prevent Tracking Wastes from the HLW Melter Cave No. 1 and HLW Melter Cave
- 2 No. 2 Containment Building
- 3 The HLW melter cave no. 1 and 2 containment building design and operating methods include
- 4 several measures that will prevent wastes from being tracked from the unit. Measures that will
- 5 be implemented include:

- Limiting the movement of personnel and material from the unit
- Using interlocked shield doors to prevent the inadvertent spread of contamination
- Decontamination ofing materials or containers before they are released from the unit
- 10 Using C5 ventilation used as a primary containment method

Personnel access to the HLW melter caves, which are classified as a C5 contamination area, will be restricted due to radiological concerns. Personnel operating in melter cave C3/C5 airlocks will not be in contact with failed spent melters because they will be encased in overpack containers.

Export of equipment from the melter caves will be kept to a minimum by performing in-cave maintenance to the maximum extent possible. The design of the cave and equipment includes master-slave manipulators, special tools, and a tool import port that will enable maintenance operations to be conducted remotely without removing the equipment from the cave. When equipment must be removed for hands-on maintenance, it will be transferred through shield doors into the dDecontamination \$\frac{1}{2}Tank (HSH-TK-00001/2) or the crane decontamination area (C3/C5) above the C3/C5 airlock—The C3/C5 doors will be interlocked with shield doors to the adjacent maintenance room, to prevent radiological shine and the spread of contamination. The equipment will be transferred to the maintenance room only after it has been decontaminated in dDecontamination \$\frac{1}{2}Tank HSH-TK-00001/2, and in the equipment decontamination area, if needed.

Spent consumables and wastes will be size-reduced in the cave and exported to drums through an air lock, which is designed to provide containment of contamination between the C5 melter cave and the C3 drum transfer tunnel. Export of failed spent melters Melters will be controlled to prevent the spread of contamination. Melters will be transferred into overpack containers that are docked with the shield doors to the C3/C5 airlock.

Control of Fugitive Dust from the HLW Melter 1 and 2 Containment Buildings
Operational controls and the HLW vitrification plant ventilation system will be used to control fugitive dust emissions from the unit to meet the requirements of 40 CFR 264.11101(c)(1)(iv). The following measures will be used to prevent dust from escaping the HLW melter 1 and 2 containment buildings:

- 41 ☐A cascading air flow from areas of least to greatest potential contamination (i.e., C2 to C3 to C5)
 - Greater negative air pressure in the unit, compared with adjacent C3 units, to pull air into the unit and prevent backflow

- 2 ☐ Dual-HEPA filtration of exhaust air before discharge to the atmosphere through a monitored stack
 - A multiple fan extraction system, designed to maintain negative pressure and cascading air flow, even during fan maintenance and repair
 - Personnel ingress and egress through airlocks and subchange rooms

- Procedures in the Event of Release or Potential for Release from the HLW Melter Cave No. 1 and HLW Melter Cave No. 2 Containment Buildings
- 10 Conditions that could lead to a release from the HLW melter cave no. 1 and HLW melter cave
 11 no. 2 containment buildings will be corrected as soon as possible after they are identified. The
 12 ventilation system and airlocks, the most likely sources of potential releases, are designed with
 13 backup HEPA filters to facilitate repairs and replacement.

In the unlikely event of a release of dangerous wastes from either containment building, actions required by 40 CFR 264.1101(c)(3)(i) through (iii) will be taken. Specific administrative and operating methods to satisfy this requirement will be developed prior to the start of operations.

Inspections of the HLW Melter Cave No. 1 and HLW Melter Cave No. 2 Containment Buildings An inspection program will be established, as required under WAC 173-303-695, to detect conditions that could lead to the release of wastes from the HLW melter cave no. 1 and HLW melter cave no. 2 containment buildings. The inspection and monitoring schedule and methods that will be used to detect a release from the unit are included in Chapter 6.

33 -

4.2.4.84.2.4.12 IHLW Container Weld Canister Handling Cave Containment Building (H-0136)

The HLW HHLW container weldcanister handling cave containment building will be located in the southern portion of the HLW vitrification plant. Typical waste management activities performed within this containment building include the storage of uncontainerized waste. Located within the containment building will be two cooling and buffer storage areas and two container welding and rework stations. IHLW containers canisters, which that have cooled enough to leave the miscellaneous unit pour areas, will be transported to the IHLW container weldcanister handling cave containment building by means of an overhead crane. The IHLW glass waste will continue to cool in the buffer storage areas. When adequately cooled, containers canisters will be moved to one of the two weld and rework cells, where the temporary lid that had been placed on the container canister will be removed and the permanent lid will be welded onto the container canister. The IHLW container will then be transported to the IHLW HHLW container canister decontaminationswabbing and monitoring cave containment building. Container management practices are discussed in Section 4.2.1.

IHLW IHLW Container WeldCanister Handling Cave Containment Building Design
The IHLW container weldcanister handling cave containment building will be completely enclosed within the HLW vitrification plant. The design and construction of the HLW vitrification plant exterior will prevent water from running into the plant. The roof of the HLW

vitrification plant will be metal. Run-off will be collected by roof drains and a drainage system 1 with overflow roof drains. The unit is designed to prevent the release and exposure of dangerous 2 3 constituents to the outside environment. Its approximate dimensions are summarized in Table 4 4-12. 5 6 IHLW HHLW Container Weld Canister Handling Cave Containment Building Structure 7 Because the IHLW container weldcanister handling cave containment building will be a 8 concrete-walled structure fully enclosed within the HLW vitrification plant, its structural requirements will be met by the design standards of the HLW vitrification plant. The design will 9 10 ensure that the unit has sufficient structural strength to prevent collapse or failure. DWP 11 Attachment 51, Chapter 4, Supplement 1 provides documentation that the seismic requirements for the HLW vitrification plant meet or exceed the Uniform Building Code Seismic 12 Design Requirements. The seismic requirements for the structure are addressed in the RPP WTP 13 14 Compliance with Uniform Building Code Scismic Design Requirements, found in Supplement 1. 15 16 IHLW IHLW Container Weld Canister Handling Cave Containment Building Unit Materials 17 The IHLW container weldcanister handling cave containment building will be constructed of steel-reinforced concrete. The interior floor and a portion of the walls of the unit will be lined 18 with stainless steel. The height of the lining will be determined as design progresses. The roof 19 20 of the HLW vitrification plant will be metal. Run off will be collected by roof drains and a 21 drainage system with everflow roof drains. 22 23 Use of Incompatible Materials for the IHLW HILW Container Weld Canister Handling Cave 24 Containment Building 25 A The partial stainless steel liner will be provided for the IHLW containment building which that will be compatible with the HLW steel containers canisters that will be managed. Treatment 26 27 reagents that could cause the liner to leak, corrode, or otherwise fail will not be used in the unit. 28 29 Primary Barrier Integrity in the IHLW IHLW Container WeldCanister Handling Cave 30 Containment Building The HLW vitrification plant is designed to withstand loads from the movement of personnel, 31 32 wastes, and handling equipment. The seismic design criteria found in Supplement 1DWP 33 Attachment 51, Supplement 1, ensures that appropriate design loads, load combinations, and 34 structural acceptance criteria are employed at the WTP. 35 Certification of Design for the IHLW IHLW Container Weld Canister Handling Cave 36 37 Containment Building 38 Prior to the start of operations, certification by a qualified registered professional engineer that 39 the IHLW container weldcanister handling cave containment building meets the design 40 requirements of 40 CFR 264.1101(a) and (c) will be obtained. The requirements of 40 CFR 264.1101(b) do not apply to this design because waste containing free liquid wastes-will not 41

be managed in the containment building and the waste will not be treated with free liquids.

42

1	Operation of the IHLW HLW Container WeldCanister Handling Cave Containment Building
2	Operational and maintenance controls and practices will be established to ensure containment of
3	the wastes within the IHLW container weldcanister handling cave containment building, as
4	required by 40 CFR 264.1101(c)(1).
5	
6	Maintenance of the IHLW IHLW Container WeldCanister Handling Cave Containment Building
7	The partial stainless steel lining of the containment building will be constructed and maintained
8	in a manner that will be free of significant cracks, gaps, corrosion, or other deterioration. The
9	stainless steel liner will be welded at each seam, and will be free of corrosion or other
10	deterioration because it will be compatible with materials that will be managed in the
11	containment building, including the stainless steel containers. Only decontamination chemicals
12	that are compatible with the liner will be used.
13	
14	Wastes that will be managed in the containment building will not be stacked higher than the unit
15	wall; however, wastes are not anticipated to be stacked.
16	
17	Measures to Prevent Tracking Wastes from the IHLW IHLW Container WeldCanister Handling
18	Cave Containment Building
19	The IHLW IHLW container weldcanister handling cave containment building is designed to
20	store cooling IHLW glass waste containers and weld the lids onto the containers.
21	
22	The outside of the eontainer canister will be inspected to see whether glass is present on the
23 .	container. If glass is found, it will be removed using a needle gun or other mechanical method.
24	The glass shards will be collected for disposal in a shop-type vacuum and disposed of as a
25	secondary waste. The containment building will be classified as a C5 contamination area, and
26	therefore personnel access will be limited restricted due to radiological concerns. Wastes leaving
27	the unit will be within containers.
28	
29	Control of Fugitive Dust from the IHLW Container Weld Containment Building
30	Operational controls and the HLW vitrification plant ventilation system will be used to control
31	fugitive dust emissions from the unit to meet the requirements of 40 CFR 264.11101(c)(1)(iv).
32	The following measures will be used to prevent dust from escaping the IHLW container weld
33	containment building:
34	
35	☐A cascading air flow from areas of least to greatest potential contamination (i.e., C2 to C3 to
36	C5)
37	Greater negative air pressure in the unit compared with adjacent C3 units, to pull air into the
38	unit and prevent backflow
39	□ Intake air through controlled air in bleed units, with backflow prevention dampers
40	Dual HEPA filtration of exhaust air before discharge to the atmosphere through a monitored
41	stack
42	☐A multiple fan extraction system, designed to maintain negative pressure and cascading air
43	flow, even during fan maintenance and repair
44	☐Personnel ingress and egress through airlocks and subchange rooms

Procedures in the Event of Release or Potential for Release from the IHLW IHLW Container
WeldCanister Handling Cave Containment Building

Conditions that could lead to a release from the <u>IHLW HILW container weldcanister handling</u> cave containment building will be corrected as soon as possible after they are identified. The ventilation system, as the most likely source of potential releases, is designed with backup HEPA filters to facilitate repairs and replacement.

In the unlikely event of a release of dangerous wastes from the containment building, actions required by 40 CFR 264.1101(c)(3)(i) through (iii) will be taken. Specific administrative and operating methods to satisfy this requirement will be developed prior to the start of operations.

Inspections of the IHLW IHLW Container WeldCanister Handling Cave Containment Building An inspection program will be established as required under WAC 173-303-695 to detect conditions that could lead to the release of wastes from the IHLW container weldcanister handling cave containment building. The inspection and monitoring schedule and methods that will be used to detect a release from the unit are included in Chapter 6.

4.2.4.94.2.4.13 IHLW Container Canister Decontamination Swab and Monitoring Cave Containment Building (H-0133)

The IHLW IHLW container canister decontaminations wab and monitoring cave containment building will beis located in the southeast corner portion of the HLW vitrification plant (Rmroom H-0133). Typical waste management activities performed in this containment building include decontamination of the exterior of the filled IHLW containers. The systems associated with the swabbing and monitoring activities in the cave include overhead crane, grapples, power manipulator, swabbing turntable, and swabbing waste storage container.

HHLW containers, which have permanent lids, will be received at the unit. The containers will be washed in a tank with de ionized water to remove loose contamination that may be on the surface of the container. The container will then be washed with ceric nitrate and nitric acid to remove a layer of steel as part of the decontamination process. The tank will be drained and the container will then be sprayed with nitric acid. Additional nitric acid rinses may be conducted, if needed. A deionized water spray will then be performed. Tank activities will occur in permitted tank systems which have secondary containment, as addressed in Section 4.2.2.

After the decontaminationed container in the canister decon vesselDecontamination Tanks (HSH-TK-0001/2), the canister is has dried it will be transferred moved to the canister swabbing station, where its exterior will be swabbed, and the swabs monitored for gamma radiation. When the container is found to meet surface radiological requirements, it will be transferred to the HHLW container storage area and monitoring building and placed on the turntable. The turntable provides a base on which the canister is set and rotated while the surface swabbing is performed. When surface cleanliness has been verified, the canister is placed in the canister storage bogic and transferred to the canister storage cave.

1	IHLW IHLW Container Canister DecontaminationSwab and Monitoring Cave Containment
2	Building Design
3	The IHLWe IHLW container canister decontaminations wab and monitoring cave containment
4	building will be completely enclosed within the HLW vitrification plant, and will be designed to
5	prevent the release of dangerous constituents and their exposure to the outside environment. The
6	design and construction of the HLW vitrification plant exterior will prevent water from running
7	into the plant. The roof of the HLW vitrification plant will consist of metal roofing, roof
8	insulation, and a vapor barrier. Run-off will be collected by roof drains and a drainage system
9	with overflow roof drains. Unit dimensions are summarized in Table 4-12.
10	The containment building design requirements of 40 CFR 264.1101(b) do not apply because
11	there are no liquid wastes managed in the IHLW HILW container canister decontaminations wab
12	and monitoring cave containment building are addressed under tank systems in Section 4.2.2.
13	
14	IHLW IHLW Container Canister DecontaminationSwab and Monitoring Cave Containment
15	Building Structure
16	Because the IHLW IHLW container canister decontaminations wab and monitoring cave building
17	will be a concrete-walled structure fully enclosed within the HLW vitrification plant, its
18	structural requirements will be met by the design standards of the HLW vitrification plant. The
19	design will ensure that the unit has sufficient structural strength to prevent collapse or failure.
20	DWP Attachment 51, Chapter 4, Supplement 1 provides documentation that the
21	seismic requirements for the HLW vitrification plant meet or exceed the Uniform Building Code
22	Seismic Design Requirements. The seismic requirements that the building must address are
23	presented in the RPP-WTP Compliance with Uniform Building Code Seismic Design
24	Requirements, found in Supplement 1.
25	
26	IHLW IHLW Container Canister DecontaminationSwab and Monitoring Cave Containment
27	Building Unit Materials
28	The IHLW tentainer canister decontamination swab and monitoring cave containment
29	building will be constructed of steel-reinforced concrete. The interior floor and a portion of the
30	walls of the unit will be lined covered with stainless steel protective coating. The roof of the
31	HLW vitrification plant will consist of metal roofing, roof insulation, and a vapor barrier.
32	Run off will be collected by roof drains and a drainage system with overflow roof drains.
33	
34	Use of Incompatible Materials for the IHLW IHLW Container Canister Decontamination Swab
35	and Monitoring Cave Containment Building
36	A stainless steel liner will be provided for the containment building and will be compatible with
37	the IHLW containerized wastes that will be managed. Treatment reagents that could cause the
38	liner protective coating to leak, corrode, or otherwise fail will not be used within the unit.
39	
40	Primary Barrier Integrity in the IHLW IHLW Container-Canister DecontaminationSwab and
41	Monitoring Cave Containment Building
42	The HLW container canister decontaminations wab and monitoring cave building is

designed to withstand loads from the movement of personnel, wastes, and handling equipment.

The seismic design criteria found in Supplement 1DWP Attachment 51, Supplement 15 ensures

43

that appropriate design loads, load combinations, and structural acceptance criteria are employed at the WTP.
 Certification of Design for the IHLW IHLW Container Canister DecontaminationSwab and Monitoring Cave Containment Building

Prior to the start of operations, certification by a qualified registered professional engineer that the IHLW container canister decontaminations wab and monitoring cave containment building

8 meets the design requirements of 40 CFR 264.1101(a) and (c) will be obtained. The

requirements of 40 CFR 264.1101(b) do not apply to this design because there are no free liquids managed in the unit are addressed under tank systems in Section 4.2.2.

Operation of the IHLW IHLW Container Canister Decontamination Swab and Monitoring Cave Containment Building

Operational and maintenance controls and practices will be established to ensure containment of the wastes within the IHLW IHLW container canister decontaminations wab and monitoring cave containment building, as required by 40 CFR 264.1101(c)(1).

Maintenance of the IHLW IHLW Container Canister Decontamination Swab and Monitoring Cave Containment Building

The stainless steel liningprotective coating of the containment building will be constructed and maintained in a manner that will be free of significant cracks, gaps, corrosion, or other deterioration. The stainless steel liner will be welded at each seam, and will be free of corrosion or other deterioration because it will be compatible with materials that will be managed in the containment building, as well as the stainless steel containers that will be managed. Only decontamination chemicals that are compatible with the liner will be used. Wastes are not expected to be stacked within the unit.

Measures to Prevent Tracking Wastes from the IHLW IHLW Container Canister DecontaminationSwab and Monitoring Cave Containment Building

The IHLW IHLW decontamination canister swab and monitoring cave containment building is designed to manage containers canisters which that are undergo decontamination in tank systems and to swab the containers bed to determine whether decontamination has been effective they meet the surface radiological requirements. The containment building will be a C5-C3 area. Conducting these activities in a C5 zone will prevent the spread of contaminated materials. The containment building is under negative pressure and therefore no air particulates can escape the unit. The air from the unit passes through HEPA filtration prior to discharge out of the plant stack.

Personnel access to the IHLW container canister decontaminations wab and monitoring cave containment building, which is classified as a C5-C3 contamination area, will be limited due to radiological concerns. Therefore, personnel moving into and out of the unit will not track contamination out of the unit.

1 2	Control of Fugitive Dust from the IHLW Container Decontamination Containment Building Operational controls and the HLW vitrification plant ventilation system will be used to control
3	fugitive dust emissions from the unit to meet the requirements of 40 CFR 264.11101(c)(1)(iv).
ر 4	The following massures will be used to provent finitive dust from accoming the IIII IV.
5	The following measures will be used to prevent fugitive dust from escaping the IHLW container decontamination containment building.
6	decontainment ounding.
7	DA cosceding our flows from orong of lengths amongstations and the second of the secon
8	□A cascading air flow from areas of least to greatest potential contamination (i.e., C2 to C3 to C5)
9	Greater negative air pressure in the unit, compared to adjacent C3 units, to pull air into the unit
.0	and prevent backflow
1	□ Intake air through controlled air in bleed units with backflow prevention dampers
2	☐Safety interlocks to shut down C3 extract fans to prevent backflow if the C5 system shuts down
5	☐Dual HEPA filtration of exhaust air before discharge to the atmosphere through a monitored stack
6 7	☐A multiple fan extraction system, designed to maintain negative pressure and cascading air flow, even during fan maintenance and repair
.8	□Personnel ingress and egress through airlocks and subchange rooms
9	and dubolining looms
10	Procedures in the Event of Release or Potential for Release from the IHLW IHLW Container
21	Canister Decontamination Swab and Monitoring Cave Containment Building
22	Conditions that could lead to a release from the <u>IHLW container canister decontaminations wab</u>
23	and monitoring cave containment building will be corrected as soon as possible after they are
24	identified. The ventilation system, the most likely source of potential releases, is designed with
25	two stages of HEPA filters with backup HEPA filters to facilitate repairs and replacement.
26	two sunges of file is interes with backup first in their to facilitate repairs and replacement.
27	In the unlikely event of a release of dangerous wastes from the containment building, actions
28	required by 40 CFR 264.1101(c)(3)(i) through (iii) will be taken. Administrative and operating
29	methods to satisfy this requirement will be developed prior to the start of operations.
30	mentous to sustery and requirement with be developed piror to the start of operations.
31	Inspections of the IHLW IHLW Container Canister Decontamination Swab and Monitoring Cave
32	Containment Building
3	An inspection program will be established as required under WAC 173-303-695, to detect
34	conditions that could lead to release of wastes from the IHLW container canister
35	decontaminationswab and monitoring cave containment building. The inspection and
6	monitoring schedule and methods that will be used to detect a release is are included in Chapter
3 7 .	6.
88	
39	4.2.4.104.2.4.14 HLW Vitrification Plant C3 Workshop Containment Building
10	(H-0311A, H-0/311A/B)
1	The HLW vitrification plant-C3 workshop containment building will be located in the northeast

side of the HLW vitrification plant at elevation 37 feet.

- Typical waste management activities performed in this containment building include
- 2 decontamination, size reduction, and packaging of spent equipment. Equipment will be
- transported to the unit contained in shielded casks, drums, or in a standard waste box. In the 3
- workshop, the equipment will be decontaminated to enable "hands-on" maintenance. Spent 4
- equipment parts will be bagged and placed in standard waste containers or boxes for disposal. 5
- 6 Size reduction may be performed to facilitate packaging. Other spent equipment will be 7 packaged in drums or standard waste boxes.

- HLW Vitrification Plant-C3 Workshop Containment Building Design
- The HLW vitrification plant-C3 workshop containment building will be designed as a completely 10
- enclosed area within the HLW vitrification plant. It will be designed to prevent the release of 11
- 12 dangerous waste and their exposure to the outside environment. The design and construction of
- 13 the HLW vitrification plant exterior will prevent water from running into the plant. The roof of
- the HLW vitrification plant will consist of metal roofing, roof insulation, and vapor barrier. 14
- Rainwater run-off will be collected by roof drains and drainage systems with overflow roof 15
- drains. The approximate dimensions of the unit are summarized in Table 4-12. 16

17 18

- HLW Vitrification Plant-C3 Workshop Containment Building Structure
- The HLW vitrification plant-C3 workshop containment building will be a concrete-walled 19
- structure fully enclosed within the HLW vitrification plant. Therefore, structural requirements 20
- for the containment building will be met by the design standards of the HLW vitrification plant. 21
- The design will ensure that the unit has sufficient structural strength to prevent collapse or 22
- failure. DWP Attachment 51, Chapter 4, Supplement 1 Supplement 1 provides documentation 23
- that the seismic requirements for the HLW vitrification plant meet or exceed the Uniform 24
- 25 Building Code Seismic Design Requirements. The seismic requirements for the HLW
- vitrification plant are presented in RPP-WTP Compliance with Uniform Building Code Scismic 26 27
- Design Requirements, found in Supplement 1.

28 29

- HLW Vitrification Plant C3 Workshop Containment Building Materials
- The HLW vitrification plant-C3 workshop containment building will be constructed of 30
- steel-reinforced concrete. The interior floor and a portion of the walls of the unit will be lined 31
- with stainless steel or protective coating. The roof of the HLW vitrification plant will consist of 32
- metal roofing, roof insulation, and vapor barrier. Rainwater run off will be collected by roof 33
- 34 drains and drainage systems with overflow roof drains.

35 36

- Use of Incompatible Materials in the HLW-Vitrification Plant C3 Workshop Containment
- 37 Building
- A partial stainless steel liner or protective coating will be provided for this unit. Stainless steel 38
- 39 or the protective coating will be compatible with the equipment wastes that will be managed.
- Activities in the unit will be limited to decontamination, size reduction, and packaging the waste 40
- components into drums or waste boxes. Treatment reagents that could cause the liner or coating 41 to leak, corrode, or otherwise fail will not be used within the unit. 42

Primary Barrier Integrity in the HLW Vitrification Plant C3 Workshop Containment Building
The HLW vitrification plant C3 workshop containment building is designed to withstand loads
from the movement of personnel, wastes, and handling equipment. The seismic design criteria
found in Supplement 1DWP Attachment 51, Supplement 15 ensures that appropriate design
loads, load combinations, and structural acceptance criteria are employed at the WTP.

 Certification of Design for the HLW Vitrification Plant-C3 Workshop Containment Building
Prior to startup of operations, a certification by a qualified registered professional engineer that
the HLW vitrification plant-C3 workshop containment building meets the design requirements of
40 CFR 264.1101(a) and (c) will be obtained. The requirements of 40 CFR 264.1101(b) do not
apply to this design because the waste managed in the unit will not contain free liquids or be
treated with free liquids.

Operation of the HLW Vitrification Plant C3 Workshop Containment Building Operational and maintenance controls and practices will be established and followed to ensure containment of the dangerous wastes within the HLW vitrification plant C3 workshop containment building unit as required by 40 CFR 264.1101(c)(1).

Maintenance of the HLW Vitrification Plant C3 Workshop Containment Building
The stainless steel lining or protective coating of the unit will be constructed and maintained in a
manner that will be free of significant cracks, gaps, corrosion, or other deterioration. The
stainless steel liner or the protective coating will remain free of corrosion or other deterioration
because it is compatible with materials that will be managed in the containment building. The
failed equipment that will be managed in the containment building unit will be compatible with
stainless steel or the protective coating. Only decontamination chemicals that are compatible
with the liner or coating will be used.

Measures to Prevent Tracking Wastes from the HLW Vitrification Plant-C3 Workshop Containment Building

The HLW vitrification plant-C3 workshop containment building will be designed to isolate failed equipment from the accessible environment and to prevent the spread of contaminated materials. Very little dust is expected to be generated in the unit.

 Personnel access to tThe containment building will be limited due to radiological concerns. It will be classified as a C3 contamination area, which allows only limited access by personnel. Personnel access will be via a C2/C3 subchange room. Equipment will enter and exit the workshop via a C2/C3 airlock. Wastes leaving the unit will be enclosed within containers. If necessary, the containers will be decontaminated in the unit prior to transportation to a permitted storage area. Equipment leaving the unit will be decontaminated, when necessary, before being released for removal from the cells.

Control of Fugitive Dust from the HLW Vitrification Plant C3 Workshop Containment Building The following measures will be used to prevent fugitive dust from escaping the HLW vitrification plant C3 workshop containment building:

1 2	☐A cascading air flow from areas of least to greatest potential contamination (i.e., C2 to C3 to C5)
3 -	□Intake air through controlled air in bleed units, with backflow prevention dampers
4 5	Dual HEPA filtration of exhaust air before discharge to the atmosphere through a monitored stack
6 7	☐A multiple fan extraction system designed to maintain negative pressure and cascading air flow, even during fan maintenance and repair
8	□Personnel ingress and egress through airlocks and subchange rooms
9	
10	Procedures in the Event of Release or Potential for Release from the HLW Vitrification Plant C3
11	Workshop Containment Building
12	The design and operation of the unit makes it very unlikely that releases will occur. The design
13 14	and operational measures will minimize the generation of dust and contain it within the unit.
15	The ventilation system will also use negative air pressure to keep contamination from areas of
16	lesser contamination, and will use two stage HEPA filtration to reduce the release of particles.
17	Inspections will identify conditions that could lead to a release. Such conditions will be
18	corrected as soon as possible after they are identified. In the unlikely event that a release of
19	dangerous wastes from the containment building is detected, actions required by
20	40 CFR 264.1101(c)(3)(i) through (iii) will be taken. Specific administrative and operating
21	methods that will be used to satisfy this requirement will be developed prior to the start of
22	operations. These methods will be followed to repair conditions that could lead to a release.
23	
24	Inspections of the HLW Vitrification Plant-C3 Workshop Containment Building
25	An inspection program will be established to detect conditions that could lead to a release of
26	wastes from the HLW vitrification plant C3 workshop containment building. The inspection and
27	monitoring schedule and methods that will be used to detect releases from the unit is are included
28 29	in Chapter 6.
30	4.2.4.114.2.4.15 HLW Vitrification Plant Air Filtration Filter Cave Containment
31	4.2.4.114.2.4.15 HLW Vitrification Plant Air Filtration Filter Cave Containment Building (H-0104)
32	The HLW vitrification plant air filtration filter cave containment building is located in the
33	northwest portion of the plant. The HLW-vitrification plant air filtration filter cave containment
34	building will manage spent HEPA and HEME-filters via an overhead crane. The crane transports
35	the spent filters to a size reduction station and then places them inside a disposal container. The
36	disposal container is then transported via cart, through an air lock and shield doors and to a load-
37	out area for storage pending final disposal. The containment building also houses a hands-on
38	crane decontamination and repair area.
39 40	HI W Vitrification Dlant Air Filters, Till C. C.
41	HLW Vitrification Plant Air FiltrationFilter Cave Containment Building Design The HIW vitrification plant air filtration
42	The HLW vitrification plant air filtration filter cave containment building will be completely
43	enclosed within the HLW vitrification plant, and will be designed to prevent the release and
	exposure of dangerous constituents to the outside environment. The design and construction of

i	the HLW vithilication plant extenor will prevent water from running into the plant. <u>The root of</u>
2	the HLW vitrification plant will consist of metal roofing, roof insulation, and a vapor barrier.
3	Run-on will be collected by roof drains and a drainage system with overflow drains. The
4	approximate dimensions of the containment building are summarized in Table 4-12.
5	
6	HLW Vitrification Plant Air Filtration Filter Cave Containment Building Structure
7	Because the HLW vitrification plant air filtration filter cave containment building will be a
8	concrete-walled structure fully enclosed within the HLW vitrification plant, its requirements will
9	be met by the design standards of the HLW vitrification plant. The design will ensure that the
10	unit has sufficient structural strength to prevent collapse or failure. DWP -Attachment 51,
11	Chapter 4, Supplement 1 provides documentation that the seismic requirements for
12	the HLW vitrification plant meet or exceed the Uniform Building Code Seismic Design
13	Requirements. The seismic requirements for the HLW vitrification plant are presented in the
14	RPP WTP Compliance with Uniform Building Code Seismic Design Requirements, found in
15	Attachment 51, Chapter 4, Supplement 1.
16	
17	HLW Vitrification Plant Air Filtration Filter Cave Containment Building Materials
18	The HLW vitrification plant air filtration filter cave containment building will be constructed of
19	steel-reinforced concrete. The interior floor and a portion of the walls will be lined with a
20	protective coating. The roof of the HLW vitrification plant will consist of metal roofing, roof
21	insulation, and a vapor barrier. Run on will be collected by roof drains and a drainage system
22	with overflow drains.
23	
24	Use of Incompatible Materials for the HLW Vitrification Plant Air Filtration Filter Cave
25	Containment Building
26	A protective coating will be provided for the containment building. The coating will be
27	compatible with the wastes that will be managed in the unit, which will include spent HEPA and
28	HEME-filters. Activities in the unit will be limited to HEPA filter change -out and size reduction
29	and waste packaging. Treatment reagents that could cause the protective coating to leak,
30	corrode, or otherwise fail will not be used within the unit.
31	
32	Primary Barrier Integrity in the HLW Vitrification Plant Air FiltrationFilter Cave Containment
33	Building
34	The HLW vitrification plant air filtration filter cave containment building will be designed to
35	withstand loads from the movement of personnel, wastes, and handling equipment. The seismic
36	design criteria found in Supplement 1 DWP Attachment 51, Supplement 1, ensures that
37	appropriate design loads, load combinations, and structural acceptance criteria are employed at
38	the WTP.
39	
40	Certification of Design for the HLW Vitrification Plant Air FiltrationFilter Cave Containment
41	Building
42	Prior to the start of operations, certification by a qualified registered professional engineer that
43 . 11	the HLW vitrification plant air filtration filter cave containment building meets the design
/1/1	requirements of (iii Like 164 Lillia) and (a) mult be able and. The magnificance of 10

2	CFR 264.1101(b) do not apply to this design because <u>dangerous</u> waste containing free liquids will not be managed in the unit and waste will not be treated with free liquids.
3 4	Operation of the HLW Vitrification Plant Air FiltrationFilter Cave Containment Building
. 5	Operational and maintenance controls and practices will be established to ensure containment of
6	the waste within the HLW vitrification air filtration filter cave containment building, as required
7	by 40 CFR 264.1101(c)(1).
8	3) 10 31 (23 1.1101(3)(1).
9	Maintenance of the HLW-Vitrification Plant Air FiltrationFilter Cave Containment Building
10	The protectively-coated concrete floor and walls of the unit will be constructed and maintained
11	in a manner that will be free of significant cracks, gaps, corrosion, or other deterioration. The
12	protective coating will be compatible with materials that will be managed in the containment
13	building, which will include spent HEPA and HEME filters. No decontamination chemicals that
14	are incompatible with the coated concrete will be used.
15	
16	Measures to Prevent Tracking Wastes from the HILW Vitrification Plant Air FiltrationFilter Cave
17	Containment Building
18	The HLW vitrification plant air filtration filter cave containment building is designed to manage
19	spent HEPA and HEME-filters. Conducting these activities in a C3-C5 zone will prevent the
20	spread of contaminated materials. Limited personnel access and Controlled movement of
21	equipment into and out of the unit will decrease the possibility that waste will be tracked from
22	the unit.
23	Domonwoli anno 4 di TYY YY di Califfa di Cal
24 25	Personnel access to the HLW vitrification plant air filtration filter cave containment building,
25 26	which is classified as a C3 C5 contamination area, will be limited restricted due to radiological
20 27	concerns. Access to the unit will be allowed only under limited circumstances, thereby limiting
28	the potential for contacting the waste and tracking it from the unit.
29	Control of Fugitive Dust from the HLW Vitrification Plant Air Filtration Containment Building
30	The following measures will be used to prevent fugitive dust from escaping the HLW
31	vitrification plant air filtration containment building unit.
32	Vicinication plant an intration contaminent building aimt.
33	☐A cascading air flow from areas of least to greatest potential contamination (i.e., C2 to C3 to
34	C5)
35	
36	☐Greater negative air pressure in the unit, compared with adjacent C2 units, to pull air into the unit and prevent backflow
37	☐ Intake air through controlled air in bleed units, with backflow prevention dampers
38	☐HEPA filtration of exhaust air before discharge to the atmosphere through a monitored stack
39	
<i>39</i> 40	☐A multiple fan extraction system designed to maintain negative pressure, and cascading air flow, even during fan maintenance and repair
41	
	Personnel ingress and egress through airlocks and subchange rooms
42	

- 1 Procedures in the Event of Release or Potential for Release from the HLW Vitrification Plant Air
- 2 FiltrationFilter Cave Containment Building
- 3 Conditions that could lead to a release from the HLW vitrification plant air filtrationfilter cave
- 4 containment building will be corrected as soon as possible after they are identified. The
- 5 ventilation system and airlocks, the most likely sources of potential releases, will be designed

6 with backup HEPA filters to facilitate repairs and replacement.

7 8

9

10

In the unlikely event of a release of dangerous wastes from the containment building, actions required by 40 CFR 264.1101(c)(3)(i) through (iii) will be taken. Specific administrative and operating methods that will be used to satisfy this requirement will be developed prior to the start of operations.

11 12 13

14 15 Inspections of the HLW Vitrification Plant Air FiltrationFilter Cave Containment Building
An inspection program will be established to detect conditions that could lead to a release of
wastes from the HLW vitrification plant air filtration containment building. The inspection and

monitoring schedule, and methods that will be used to detect releases from the unit, are included

in Chapter 6.

18 19

20

21

22

4.2.4.12HLW Vitrification Plant Drum Transfer Tunnel Containment Building

The HLW vitrification plant drum transfer tunnel containment building stretches east to west, nearly the entire length of the HLW vitrification plant. Typical waste management activities performed in this containment building include size reduction, storage of uncontainerized waste, and packaging of failed and spent equipment.

23 24 25

26

27

28

29

HLW Vitrification Plant Drum Transfer Tunnel Containment Building Design

The HLW vitrification plant drum transfer containment building will be completely enclosed within the HLW vitrification plant, and will be designed to prevent the release and exposure of dangerous constituents to the outside environment. The design and construction of the HLW vitrification plant exterior will prevent water from running into the plant. The approximate dimensions of the containment building are summarized in Table 4-12.

30 31 32

HLW Vitrification Plant Drum Transfer Tunnel Containment Building Structure

- Because the HLW vitrification plant drum transfer tunnel containment building will be a

 concrete walled structure fully enclosed within the HLW vitrification plant, its requirements will

 be met by the design standards of the HLW vitrification plant. The design will ensure that the

 unit has sufficient structural strength to prevent collapse or failure. The seismic requirements for
- 37 the HLW vitrification plant are presented in the RPP WTP Compliance with Uniform Building

38 Code Scismic Design Requirements, found in Supplement 1.

- HLW Vitrification Plant Drum Transfer Tunnel Containment Building Materials
- The HLW vitrification plant drum transfer tunnel containment building will be constructed of steel reinforced concrete. The interior floor and a portion of the walls will be lined with a
- 43 protective coating. The roof of the HLW vitrification plant will consist of metal roofing, roof
- 44 insulation, and a vapor barrier. Run on will be collected by roof drains and a drainage system
- 45 with overflow drains.

1 2 Use of Incompatible Materials for the HLW Vitrification Plant Drum Transfer Tunnel 3 Containment Building 4 A protective coating will be provided for the containment building. The coating will be 5 compatible with the wastes that will be managed in the unit, which will include out of service 6 process equipment, including pumps, valve, filters, jumpers, and maintenance equipment. 7 Reagents that could cause the liner to leak, corrode, or otherwise fail will not be used within the 8 unit. 9 10 Primary Barrier Integrity in the HLW Vitrification Plant Drum Transfer Tunnel Containment 11 **Building** 12 The HLW vitrification plant drum transfer tunnel containment building will be designed to 13 withstand loads from the movement of wastes and handling equipment. The seismic design 14 criteria found in Supplement 1, ensures appropriate design loads, load combinations, and 15 structural acceptance criteria are employed at the WTP. 16 17 Certification of Design for the HLW Vitrification Plant Drum Transfer Tunnel Containment 18 Building 19 Prior to the start of operations, certification by a qualified registered professional engineer that 20 the HLW vitrification plant drum transfer tunnel containment building meets the design 21 requirements of 40 CFR 264.1101(a), (b), and (c) will be obtained. 22 23 Operation of the HLW-Vitrification Plant Drum Transfer Tunnel Containment Building 24 Operational and maintenance controls and practices will be established to ensure containment of 25 the waste within the HLW vitrification plant drum transfer tunnel containment building, as 26 required by 40 CFR 264.1101(c)(1). 27 28 Maintenance of the HLW Vitrification Plant Drum Transfer Tunnel Containment Building 29 The protectively-coated concrete floor and walls of the unit will be constructed and maintained 30 in a manner that will be free of significant cracks, gaps, corrosion, or other deterioration. The 31 protective coating will be compatible with materials that will be managed in the containment 32 building, which will include the out-of-service process equipment and containerized waste and 33 equipment. No decontamination chemicals that are incompatible with the coated concrete will 34 be used. 35 36 Measures to Prevent Tracking Wastes from the HLW Vitrification Plant Drum Transfer Tunnel 37 Containment Building 38 The HLW-vitrification plant drum transfer tunnel containment building is designed to provide a 39 means to dispose of spent equipment by providing lifting, holding, and transporting of disposal 40 containers. The unit also supports size reduction and packaging of waste containers. Conducting 41 these activities in a C3 zone will prevent the spread of contaminated materials. Limited 42 personnel access and controlled movement of equipment into and out of the unit will decrease 43 the possibility that waste will be tracked from the unit.

1	Personnel access to the HLW vitrification plant drum transfer tunnel containment building,
2	which is classified as a C3 contamination area, will be limited due to radiological concerns.
.3	Access to the unit will be allowed only under limited circumstances, thereby limiting the
4 5	potential for contacting the waste and tracking it from the unit.
6	Control of Fugitive Dust from the HLW Vitrification Plant Drum Transfer Tunnel Containment
7	Building
8	The following measures will be used to prevent fugitive dust from escaping the HLW
9	vitrification plant drum transfer tunnel containment building unit:
10	1
l1 l2	☐A cascading air flow from areas of least to greatest potential contamination (i.e., C2 to C3 to C5)
13 14	☐ Greater negative air pressure in the unit, compared with adjacent C2 units, to pull air into the unit and prevent backflow
15	□Intake air through controlled air in bleed units, with backflow prevention dampers
16 17	□Dual HEPA filtration of exhaust air before discharge to the atmosphere through a monitored stack
18 19	☐A multiple fan extraction system designed to maintain negative pressure, and cascading air flow, even during fan maintenance and repair
20	Personnel ingress and egress through airlocks and subchange rooms
21	
22	Procedures in the Event of Release or Potential for Release from the HLW Vitrification Plant
23	Drum Transfer Tunnel Containment Building
24	Conditions that could lead to a release from the HLW vitrification plant drum transfer tunnel
25	containment building will be corrected as soon as possible after they are identified. The
26	ventilation system and airlocks, the most likely sources of potential releases, will be designed
27	with backup HEPA filters to facilitate repairs and replacement.
28	
29	In the unlikely event of a release of dangerous wastes from the containment building, actions
30	required by 40 CFR 264.1101(c)(3)(i) through (iii) will be taken. Specific administrative and
31	operating methods that will be used to satisfy this requirement will be developed prior to the star
32	of operations.
33	
34	Inspections of the HLW Vitrification Plant Drum Transfer Tunnel Containment Building
35	An inspection program will be established to detect conditions that could lead to a release of
36	wastes from the HLW vitrification plant drum transfer tunnel containment building. The
37	inspection and monitoring schedule, and methods that will be used to detect releases from the
38 39	unit, are included in Chapter 6.
40	4.2.4.16 HLW Pour Tunnel No. 1 Containment Building (H-B032) and HLW Pour
41	Tunnel No. 2 Containment Buildings (H-B032) and HLW Pour Tunnel No. 2 Containment Buildings (H-B032 and (H-B005A)
-	THE POWER PRINCIPLE DAMPER AND
42	HLW Ppour tunnels No. 1 and No. 2 containment building contain bogies that transport empty

canisters to the melter pour spout. Each of the two pour tunnels are 11 ft² wide by 85 ft² -2²² in.

- long extending from the south end of the melter caves in a north-south direction to an area below
- 2 the canister handling cave. The glass pouring into canisters takes place in the north half of the
- 3 HLW pour tunnels No.1 and No. 2 containment buildings. After filling with glass, the canisters
- 4 are allowed to cool down prior to being transported to the south portion of the HLW pour tunnels
- 5 No.1 and No. 2 containment buildingspour tunnels 1 and 2 and transferred through the hatch to
- 6 the canister handling cave located above. The south portion of the HLW pour tunnels No.1 and
- 7 No. 2 containment buildingspour tunnels 1 and 2 can be used for bogie decontamination, if
- 8 required, prior to handling in the bogie maintenance area. The bogie maintenance area is
- 9 segregated from HLW pour tunnels No.1 and No. 2 containment buildingspour tunnels 1 and 2
- 10 by a shield door. Bogie decontamination is not considered a dangerous waste management
- activity performed within the boundary of HLW pour tunnels No.1 and No. 2 containment
- 12 buildingspour tunnels 1 and 2.

- 14 HLW Pour Tunnel No. 1 and HLW Pour Tunnel No. 2 Containment Building Design
- 15 The HLW pour tunnels No.1 and No. 2 containment buildingspour tunnel containment buildings
- will be completely enclosed within the HLW vitrification plant, and will be designed to prevent
- 17 the release of dangerous constituents and their exposure to the outside environment. The design
- 18 and construction of the HLW vitrification plant exterior will prevent water from running into the
- 19 <u>facility</u>. The roof of the HLW vitrification plant will consist of metal roofing, roof insulation,
- and a vapor barrier. Runoff will be collected by roof drains and a drainage system with overflow
- 21 roof drains. Unit dimensions are summarized in Table 4-12.

22

- 23 The containment buildings' design requirements of 40 CFR 264.1101(b) do not apply because
- 24 there are no liquid dangerous wastes managed in the pour tunnels.

25

- 26 HLW Pour Tunnel No. 1 and HLW Pour Tunnel No. 2 Containment Building Pour Tunnel
- 27 Containment Building Structure
- 28 Because the HLW pour tunnels No.1 and No. 2 containment buildingspour tunnels will be
- 29 concrete-walled structures fully enclosed within the HLW vitrification plant, their structural
- 30 requirements will be met by the design standards of the HLW vitrification plant. The design will
- 31 ensure that the units have sufficient structural strength to prevent collapse or failure. DWP
- 32 <u>Attachment 51, Chapter 4, Supplement 1 Supplement 1 provides documentation that the seismic</u>
- 33 requirements for the HLW vitrification plant meet or exceed the Uniform Building Code Seismic
- 34 Design Requirements. The seismic requirements that the buildings must address are presented in
- 35 RPP WTP Compliance with Uniform Building Code Scismic Design Requirements, provided in
- 36 Attachment 51, Chapter 4, Supplement 1.

- 38 HLW Pour Tunnel No. 1 and HLW Pour Tunnel No. 2 Containment BuildingPour Tunnel
- 39 <u>Containment Building Unit Materials</u>
- 40 The HLW pour tunnels No.1 and No. 2 containment buildingspour tunnel containment buildings
- will be constructed of steel-reinforced concrete. The interior floors and a portion of the walls of the units will be lined with stainless steel to protect the insulation and concrete from the effects
- of high temperatures. The roof of the HLW vitrification plant will consist of metal roofing, roof
- 44 insulation, and a vapor barrier. Runoff will be collected by roof drains and a drainage system
- 45 <u>with overflow roof drains.</u>

L	
2	Use of Incompatible Materials for the HLW Pour Tunnel No. 1 and HLW Pour Tunnel No. 2
3	Containment BuildingsPour Tunnel Containment Buildings
4	There are no liquid dangerous wastes managed within the HLW pour tunnels No.1 and No. 2
5	containment buildingspour tunnel-containment buildings.
6	
7	Primary Barrier Integrity in the HLW Pour Tunnel No. 1 and HLW Pour Tunnel No. 2
8	Containment BuildingsPour Tunnel Containment Buildings
9	The HLW pour tunnels No.1 and No. 2 containment buildingspour tunnel containment buildings
10	are designed to withstand loads from the movement of wastes and handling equipment. The
11	seismic design criteria found in DWP Attachment 51, Chapter 4, Supplement 1Supplement 1
12	ensures that appropriate design loads, load combinations, and structural acceptance criteria are
13	employed at the WTP.
14	
15	Certification of Design for the HLW Pour Tunnel No. 1 and HLW Pour Tunnel No. 2
16	Containment BuildingsPour Tunnel Containment Building
17	Prior to the start of operations, certification by a qualified, registered professional engineer that
18	the HLW pour tunnels No.1 and No. 2 containment buildingspour tunnel containment buildings
19	meet the design requirements of 40 CFR 264.1101(a) and (c) will be obtained. The requirements
20	of 40 CFR 264.1101(b) do not apply to this design because no free liquids are managed in the
21	unit.
22	
23	Operation of the HLW Pour Tunnel No. 1 and HLW Pour Tunnel No. 2 Containment
24	BuildingPour Tunnel Containment Buildings
25	Operational and maintenance controls and practices will be established to ensure containment of
26	the wastes within the HLW pour tunnels No.1 and No. 2 containment buildingspour tunnel
27	containment buildings, as required by 40 CFR 264.1101(c)(1).
28	
29	Maintenance of the HLW Pour Tunnel No. 1 and HLW Pour Tunnel No. 2 Containment
30	BuildingsPour Tunnel Containment Buildings
31 -	AThe partial stainless-steel liner will be installed in the HLW pour tunnels No.1 and No. 2
32	containment buildingspour tunnel containment buildings to protect insulation and concrete from
33	the effects of high temperatures. Waste canisters will not be stacked within the unit.
34	
35	Measures to Prevent Tracking Wastes from the HLW Pour Tunnel No. 1 and HLW Pour Tunnel
36	No. 2 Containment Buildings Pour Tunnel Containment Buildings
37	The HLW vitrification plant C5 HLW pour tunnels No.1 and No. 2 containment buildingspour
38	tunnel containment buildings will be designed to isolate failed equipment from the accessible
39·	environment and to prevent the spread of contaminated materials. Very little dust is expected to
40	be generated in the unit.
41	
42	Personnel access to the HLW pour tunnels No.1 and No. 2 containment buildingseontainment
43	building will not be allowed because of high radiation.

- 1 Control of Fugitive Dust from the HLW Pour Tunnel No. 1 and HLW Pour Tunnel No. 2
- 2 Containment Buildings Pour Tunnel Containment Buildings
- 3 Operational controls of the HLW vitrification plant ventilation system will be used to control
- 4 fugitive dust emissions from the units to meet the requirements of 40 CFR 264.1101(c)(1)(iv).
- 5 The following measures will be used to prevent fugitive dust from escaping the HLW pour
- 6 tunnels No.1 and No. 2 containment buildingspour tunnel containment buildings:

- 8 A cascading air flow from areas of least to greatest potential contamination (i-ethat is-, C2 to C3 to C5)
- Greater negative air pressure in the unit, compared to adjacent C3 units, to pull air into the
 unit and prevent backflow
- Intake air through controlled air in-bleed units with backflow prevention dampers
- Safety interlocks to shut down C3 extract fans to prevent backflow if the C5 system shuts
 down
- Dual HEPA filtration of exhaust air before discharge to the atmosphere through a monitored
 stack
- A multiple fan extraction system, designed to maintain negative pressure and cascading air
 flow, even during fan maintenance and repair
- Personnel ingress and egress through airlocks and subchange rooms

20

- 21 Procedures in the Event of Release or Potential for Release from the HLW Pour Tunnel No. 1
- 22 and HLW Pour Tunnel No. 2 Containment BuildingsPour Tunnel Containment Buildings
- 23 Conditions that could lead to a release from the HLW pour tunnels No.1 and No. 2 containment
- 24 buildingspour tunnel containment buildings will be corrected as soon as possible after they are
- 25 identified. In the unlikely event of a release of dangerous wastes from the containment
- buildings, actions required by 40 CFR 264.1101(c)(3)(i) through (iii) will be taken.
- 27 Administrative and operating methods to satisfy this requirement will be developed prior to the
- 28 start of operations.

29

- 30 <u>Inspections of the HLW Pour Tunnel No. 1 and HLW Pour Tunnel No. 2 Containment</u>
- 31 BuildingsPour Tunnel Containment Buildings
- 32 An inspection program will be established as required under WAC 173-303-695, to detect
- conditions that could lead to the release of wastes from the HLW pour tunnel containment
- 34 <u>buildings</u>. The inspection and monitoring schedule and methods that will be used to detect a
- 35 release are included in DWP Attachment 51, Chapter 6.

36 37

- 4.2.4.17 HLW Drum Swabbing and Monitoring Area Containment Building (H-0126A, H-0126B, and H-B028)
- 39 The HLW drum swabbing and monitoring area containment building is located in the northeast
- 40 section of the HLW vitrification plant. Typical waste management activities performed in this
- containment building include the remote handling of 55 US gallon drums. The drums will be
- 42 swabbed for surface contamination and decontaminated if needed.

1	
2	Upon arrival in the HLW drum swabbing and monitoring area, the 55 US gallon drums are
3	weighed, monitored for activity using a gamma monitor mounted in the cell, and then transferred
4	through a hatch and placed into a shielded cask in the cask handling area.
5	
6	In the cask handling area, drum transport casks are remotely lidded and moved to the truck
7	loading bay for removal from the facility.
8	
9	Drum Swabbing and Monitoring Area Containment Building Design
10	The drum swabbing and monitoring area containment building will be completely enclosed
11	within the HLW vitrification plant, and will be designed to prevent the release of dangerous
12	constituents and their exposure to the outside environment. The design and construction of the
13	HLW vitrification plant exterior will prevent water from running into the plant. The roof of the
14	HLW vitrification plant will consist of metal roofing, roof insulation, and a vapor barrier.
15	Runoff will be collected by roof drains and a drainage system with overflow roof drains. Unit
16	dimensions are summarized in Table 4-12.
17	
18	The containment building design requirements of 40 CFR 264.1101(b) do not apply because the
19	liquid dangerous wastes will not be managed in the drum swabbing and monitoring area. If
20	liquid dangerous wastes are stored in 55 US gallon drums, the drums will be provided with
21	portable secondary containment.
22	
23	HLW Drum Swabbing and Monitoring Area Containment Building Structure
24	Because the HLW drum swabbing and monitoring area will be a concrete-walled structure fully
25	enclosed within the HLW vitrification plant, its structural requirements will be met by the design
26	standards of the HLW vitrification plant. The design will ensure that the unit has sufficient
27	structural strength to prevent collapse or failure. DWP Attachment 51, Chapter 4, Supplement
28	1Supplement 1 provides documentation that the seismic requirements for the HLW vitrification
29	plant meet or exceed the Uniform Building Code Seismic Design Requirements. The seismic
30	requirements that the building must address are presented in RPP WTP Compliance with
31 32	Uniform Building Code Seismic Design-Requirements, provided in Attachment 51, Chapter 4,
	Supplement 1.
33 34	III W Dayne Carolidine and Manifeston Ann. Co. (2)
35	HLW Drum Swabbing and Monitoring Area Containment Building Unit Materials The HLW draw graphing and monitoring Area Containment Building Unit Materials
36	The HLW drum swabbing and monitoring area containment building will be constructed of
37	steel-reinforced concrete. The interior floor and a portion of the walls of the unit will be covered
38	with special protective coating to protect the concrete from radiologicalmixed waste
39	contamination. The roof of the HLW vitrification plant will consist of metal roofing, roof
40	insulation, and a vapor barrier. Runoff will be collected by roof drains and a drainage system with overflow roof drains.
40 41	what over now foot attains.
42	Tise of Incompatible Materials for the UT W. Down Greekling and Marie Inc.
43	Use of Incompatible Materials for the HLW Drum Swabbing and Monitoring Area Containment Building
	L- WINGELLE

There are no liquid dangerous wastes managed within the HLW drum swabbing and monitoring containment building.

1	
\sim	

- Primary Barrier Integrity in the HLW Drum Swabbing and Monitoring Area Containment
 Building
- 4 The HLW drum swabbing and monitoring area containment building is designed to withstand
- 5 loads from the movement of personnel, wastes, and handling equipment. The seismic design
- 6 criteria found in DWP Attachment 51, Chapter 4, Supplement 1 ensures that
- 7 appropriate design loads, load combinations, and structural acceptance criteria are employed at the WTP.

- 10 Certification of Design for the HLW Drum Swabbing and Monitoring Area Containment
- 11 Building
- 12 Prior to the start of operations, certification by a qualified, registered professional engineer that
- 13 the HLW drum swabbing and monitoring area containment building meets the design
- 14 requirements of 40 CFR 264.1101(a) and (c) will be obtained. The requirements of 40 CFR
- 15 264.1101(b) do not apply to this design because free liquids managed in the unit are addressed
- 16 under tank systems in section 4.2.2.

17

- 18 Operation of the HLW Drum Swabbing and Monitoring Area Containment Building
- 19 Operational and maintenance controls and practices will be established to ensure containment of
- 20 the wastes within the HLW drum swabbing and monitoring area containment building, as
- 21 required by 40 CFR 264.1101(c)(1).

22

- 23 Maintenance of the HLW Drum Swabbing and Monitoring Area Containment Building
- 24 Personnel access to the containment building will not be allowed because of high radiation.
- 25 Drums are not normally expected to be stacked within the unit.

26

- 27 Measures to Prevent Tracking Wastes from the HLW Drum Swabbing and Monitoring Area
- 28 <u>Containment Building</u>
- 29 The HLW vitrification plant C5 HLW drum swabbing and monitoring containment building will
- 30 <u>be designed to isolate failed equipment from the accessible environment and to prevent the</u>
- 31 spread of contaminated materials. Very little dust is expected to be generated in the unit.

32

- 33 Control of Fugitive Dust from the HLW Drum Swabbing and Monitoring Area Containment
- 34 <u>Building</u>
- 35 Operational controls of the HLW vitrification plant ventilation system will be used to control
- 36 <u>fugitive dust emissions from the unit to meet the requirements of 40 CFR 264.1001(c)(1)(iv).</u>
- 37 The following measures will be used to prevent fugitive dust from escaping the HLW dDrum
- 38 Sswabbing and Mmonitoring aArea cContainment Bbuilding:

- 40 A cascading air flow from areas of least to greatest potential contamination (i.e.that is, C2 to C3 to C5)
- Greater negative air pressure in the unit, compared to adjacent C3 units, to pull air into the unit and prevent backflow
- Intake air through controlled air in-bleed units with backflow prevention dampers

- Safety interlocks to shut down C3 extraction fans to prevent backflow, if the C5 system shuts
 down
- <u>Dual HEPA filtration of exhaust air before discharge to the atmosphere through a monitored</u>
 <u>stack</u>
 - A multiple fan extraction system, designed to maintain negative pressure and cascading air flow, even during fan maintenance and repair
 - Personnel ingress and egress through airlocks and subchange rooms

5

6

7

- 9 Procedures in the Event of Release or Potential for Release from HLW Drum Swabbing and
- 10 Monitoring Area Containment Building
- 11 Conditions that could lead to a release from the HLW drum swabbing and monitoring area
- containment building will be corrected as soon as possible after they are identified. In the
- 13 unlikely event of a release of mixed or dangerous wastes from the containment building, actions
- required by 40 CFR 264.1101(c)(3)(i) through (iii) will be taken. Administrative and operating
- methods to satisfy this requirement will be developed prior to the start of operations.

16 17

- Inspections of the HLW Drum Swabbing and Monitoring Area Containment Building
- An inspection program will be established as required under WAC 173-303-695, to detect
- 19 conditions that could lead to the release of wastes from the HLW drum swabbing and monitoring
- area containment building. The inspection and monitoring schedule and methods that will be
- 21 used to detect a release are include in DWP Attachment 51, Chapter 6.

22 23

24

4.2.4.18 HLW Waste Handling Area Containment Building (H-410, H-410A, H-410B, and-H-411)

- 25 The HLW waste handling area containment building consists of rooms H 410, H 410A.
- 26 H-410B, and H-411 on the 58 footst elevation of the HLW vitrification plant. Typical waste
- 27 <u>management activities performed in this containment building include waste sorting, segregation,</u>
- 28 and providing temporary storage of mixed waste containers (i.e. that is, spent silver mordenite).
- 29 The HLW waste handling area containment building waste handling room will contain floor
- 30 space for segregated storage of empty and full containers, typically 55 gallon waste drums.
- 31 Tools and equipment will also be stored in this containment building.

32

- 33 HLW Waste Handling Area Containment Building Design
- 34 The HLW waste handling area containment building will be completely enclosed within the
- 35 HLW vitrification plant, and will be designed to prevent the release of dangerous constituents
- 36 and their exposure to the outside environment. The design and construction of the HLW
- 37 vitrification plant exterior will prevent water from running into the plant. The roof of the HLW
- vitrification plant will consist of metal roofing, roof insulation, and a vapor barrier. Runoff will
- 39 be collected by roof drains and a drainage system with overflow roof drains. Unit dimensions
- 40 are summarized in Table 4-12.

The containment building design requirements of 40 CFR 264.1101(b) do not apply because the 1 liquid dangerous wastes will not be managed in the waste handling area. If liquid wastes are 2 stored in 55 US gallon drums, the drums will be provided with portable secondary containment. 3 4 5 HLW Waste Handling Area Containment Building Structure Because the HLW waste handling area containment buildingwaste handling area will be a 6 7 concrete-walled structure fully enclosed within the HLW vitrification plant, its structural requirements will be met by the design standards of the HLW vitrification plant. The design will 8 ensure that the unit has sufficient structural strength to prevent collapse or failure. DWP 9 Attachment 51, Chapter 4, Supplement 1 Supplement 1 provides documentation that the seismic 10 requirements for the HLW vitrification plant meet or exceed the Uniform Building Code Seismic 11 Design Requirements. The seismic requirements that the building must address are presented in 12 RPP-WTP Compliance with Uniform Building Code Scismic Design Requirements, provided in 13 Attachment 51, Chapter 4, Supplement 1. 14 15 HLW Waste Handling Area Containment Building Unit Materials 16 The HLW waste handling area containment building will be constructed of steel-reinforced 17 concrete. The interior floor and a portion of the walls of the unit will be covered with special 18 protective coatings to protect the concrete from radiologicalmixed waste contamination in 19 accordance with ALARA principles. The roof of the HLW vitrification plant will consist of 20 metal roofing, roof insulation, and a vapor barrier. Runoff will be collected by roof drains and a 21 drainage system with overflow roof drains. 22 23 Use of Incompatible Materials for the HLW Waste Handling Area Containment Building 24 There are no liquid dangerous wastes managed within the HLW waste handling area containment 25 26 building. 27 Primary Barrier Integrity in the HLW Waste Handling Area Containment Building 28 The HLW waste handling area containment building is designed to withstand loads from the 29 movement of personnel, wastes, and handling equipment. The seismic design criteria found in 30 DWP Attachment 51, Chapter 4, Supplement 1 Supplement 1 ensures that appropriate design 31 32 loads, load combinations, and structural acceptance criteria are employed at the WTP. 33 Certification of Design for the HLW Waste Handling Area Containment Building 34 Prior to the start of operations, certification by a qualified, registered professional engineer that 35 36 the HLW waste handling area containment building meets the design requirements of 40 CFR 264.1101(a) and (c) will be obtained. The requirements of 40 CFR 264.1101(b) do not 37 apply to this design because free liquids will not be managed in the unit. 38 39 40 Operation of the HLW Waste Handling Area Containment Building Operational and maintenance controls and practices will be established to ensure containment of 41 the wastes within the HLW waste handling area containment building, as required by 42 43 40 CFR 264.1101(c)(1).

- 1 Maintenance of the HLW Waste Handling Area Containment Building
- 2 Wastes are not normally expected to be stacked within the unit.

- 4 Measures to Prevent Tracking Wastes from the HLW Waste Handling Area Containment
 5 Building
- 6 Wastes leaving the HLW waste handling area containment building will be enclosed within
- 7 containers. If necessary, these containers will be decontaminated in the unit prior to
- 8 transportation to another permitted storage, treatment, or disposalTSD facility.

9

- 10 Control of Fugitive Dust from the HLW Waste Handling Area Containment Building
- Operational controls of the HLW vitrification plant ventilation system will be used to control
- fugitive dust emissions from the unit to meet the requirements of 40 CFR 264.1101(c)(1)(iv).
- The following measures will be used to prevent fugitive dust from escaping the waste handling area containment building:

15

- A cascading air flow from areas of least to greatest potential contamination (i.e. that is, C2 to
 C3 to C5)
- Greater negative air pressure in the unit, compared to adjacent C3 units, to pull air into the
 unit and prevent backflow
- Intake air through controlled air in-bleed units with backflow prevention dampers
- Safety interlocks to shut down C3 extraction fans to prevent backflow if the C5 system shuts
 down
- Dual HEPA filtration of exhaust air before discharge to the atmosphere through a monitored
 stack
- A multiple fan extraction system, designed to maintain negative pressure and cascading air
 flow, even during fan maintenance and repair
- Personnel ingress and egress through airlocks and subchange rooms

28

- 29 Procedures in the Event of Release or Potential for Release from HLW Waste Handling Area
- 30 Containment Building
- 31 Conditions that could lead to a release from the HLW waste handling area containment building
- 32 will be corrected as soon as possible after they are identified. In the unlikely event of a release
- 33 of dangerous wastes from the containment building, actions required by 40 CFR
- 34 264.1101(c)(3)(i) through (iii) will be taken. Administrative and operating methods to satisfy
- 35 this requirement will be developed prior to the start of operations.

36

- 37 <u>Inspections of the HLW Waste Handling Area Containment Building</u>
- 38 An inspection program will be established as required under WAC 173-303-695, to detect
- 39 conditions that could lead to the release of wastes from the HLW waste handling area
- 40 containment building. The inspection and monitoring schedule and methods that will be used to
- 41 detect a release are included in DWP Attachment 51, Chapter 6.

4.3 OTHER WASTE MANAGEMENT UNITS

- 2 Sections 4.3.1 through 4.3.5 discuss the applicability of the requirements for waste management
- 3 units that have not been discussed up to this point in the DWPApermit. Sections 4.3.6 through
- 4 through 4.3.9 describe the applicability of air emission controls, waste minimization,
- 5 groundwater monitoring, and functional design requirements to the WTP. References to other
- 6 sections of the DWPA permit are provided as appropriate.

7 8

1

4.3.1 Waste Piles [D-3]

- 9 The operation of the WTP does not involve the placement of dangerous waste in waste piles.
- Therefore, the requirements of WAC 173-303-660, "Waste Piles", do not apply to the WTP.

11 12

4.3.2 Surface Impoundments [D-4]

- 13 The operation of the WTP does not involve the placement of dangerous waste in surface
- 14 impoundments. Therefore, the requirements of WAC 173-303-650, "Surface Impoundments",
- do not apply to the WTP.

16 17

4.3.3 Incinerators [D-5]

- 18 The WTP does not include a dangerous waste incinerator. Therefore, the requirements of
- 19 WAC 173-303-670, "Incinerators", do not apply to the WTP.

20

21 4.3.4 Landfills [D-6]

- The operation of the WTP does not involve the placement of dangerous waste in landfills.
- 23 Therefore, the requirements of WAC 173-303-665, "Landfills", do not apply to the WTP.

24

25 4.3.5 Land Treatment [D-7]

- 26 The operation of the WTP does not involve the land treatment of dangerous waste. Therefore,
- 27 the requirements of WAC 173-303-655, "Land Treatment", do not apply to the WTP.

28

29 4.3.6 Air Emissions Control [D-8]

30 Information regarding air emissions control is provided in the following sections:

31

- Pretreatment plant vessel ventilation system description process and exhaust system (PVP/
 PVV) Section 4.1.2.17
- LAW vitrification offgas treatment system description <u>sSection 4.1.43.3</u>
- HLW vitrification offgas treatment system description <u>sSection 4.1.54.3</u>
- Process vents— (40 CFRPart 264 Subpart AA) sSection 4.2.2.10.2
- Equipment leaks (40 CFRPart 264 Subpart BB) section 4.2.2.10.3
- Tanks and containers (40 CFRPart 264 Subpart CC) sSection 4.2.2.10.4

2	Waste minimization information is presented in Chapter 10 of the permit-application.						
4	4.3.8 Groundwater Monitoring for Land-Based Units [D-10]						
5 6 7 8 9	The groundwater monitoring requirements found in WAC 173-303-645, "Releases from regulated units,", do not apply to the WTP, since it is not operated as a regulated dangerous waste surface impoundment, landfill, land treatment area or waste pile, as defined in WAC 173-303-040. Therefore, groundwater monitoring is not required.						
10	4.3.9 Functional Design Requirements						
11	The WTP will be designed to comply with applicable design codes and specifications. The Basis						
12	of Design (BNI 2001) provides the design basis for the structures, systems, and components of						
13	the WTP documents referenced in this chapter and contained in DWP Attachment 51 identify the						
14	codes and standards to which the WTP system, structures, and components are being						
15	constructed.						
16							

Waste Minimization [D-9]

4.3.7

```
Table 4-1 Example Piping Material Service Class Index
1
     Table 4-1 has been deleted and replaced superceded by Piping Material Class Description.
2
     (24590-WTP-PER-PL-02-001), located in (DWP, Attachment 51, Appendix 4).
3
4
     Table 4-1
                     Example Piping Material Service Class Index
     Class (Old) Design Code/Service Press/Temp Limits Psig @ °F Flange Pressure Class Corrosion/
5
     Erosion Allow (in.) Pipe Large Fittings Small Fittings Valve Body Valve Trim Casket
6
7
     B<sub>19</sub>A
     (BB) Uniform Plumbing Code
8
9.
     (WV) Potable Water Based on Design
     130 @ 200 --- CL 150
10
     B16.24 0.240 Copper 3/8" 4", Type L Cast Copper Alloy Cast Copper Alloy Cast Bronze/ Cast Iron
11
12
            Bronze Neoprene/Red Rubber/EPDM
13
     C12A
14
     (CA) - ASME B31.3, Normal Fluid Service
     (GQ) Process Air
15
     (GK) - 150 Psig Air
16
     (GN) Nitrogen
17
18
     (GA) Argon
     (WB) Cooling Water Supply
19
20
     (WC) Cooling Water Return
21
     (WK) Chilled Water Supply
22
     (WL) Chilled Water Return
23
     (ZA) Non Dangerous, Non-Radioactive Liquid Effluent Based on ASME B16.5
     285 @ 20/100
24
25
     <del>200 @ 400 ____</del>
                  -CL-150
26
     B16.5 0.0625 Carbon Steel 1/2" 1 1/2", XS
27
     2"-24", STD 30", STD Carbon Steel Carbon Steel 13CR HFS
                                                                                    304 SS Spiral Wound
28
     /ASME B16.20
29
     C12B
30
     (CB) - ASME B31.3, Normal Fluid Service
31
      (DB, (DC), (DL) Steam
32
     (ZU) Non Radioactive Condensate Based on ASME B16.5
33
      285 @ - 20/100
34
                   -CL-150
      <del>200 @ 400 —</del>
35
     B16.5 0.0625 Carbon Steel 1/2" 1 1/2", XS
36
      2" 24", STD Carbon Steel Carbon Steel 13CR HFS
                                                                           304 SS Spiral Wound /ASME
37
     B16.20
38
      C12D
39
      (CD) — ASME B31.3, Normal Fluid Service
40
      (XM) - Fuel Oil
41
      (XK) Diesel Oil
                          Based on ASME B16.5
42
      <del>285 @ 20/100</del>
43
      260 @ 200 -
                   CL 150
44
      B16.5 0.0625 Carbon Steel 1/2" 1 1/2", XS
45
                                                                            - 304 SS Spiral-Wound / ASME
      2" 4", STD Carbon Steel Carbon Steel 13CR-HFS
46
      B16.20
47
      C12E
      (CE)---NFPA-13
48
49
      (WF) Fire Protection, Aboveground Based on Design
      175 @ 120 CL 150
50
51
      B16.5 0.1000 Carbon Steel.
52
      3/4" 1", Sch. 160
53
      1 1/2 2", XS 3" 20", STD
                                  -Carbon Steel Malleable Iron Cast Bronze
```

```
Cast Iron
                     Bronze
1
      Ductile Iron Neoprene
 3
      C12U
      (CU) -- ASME B31.3, Normal Fluid Service
      (GK) Compressed Air, Underground
6
      (GQ) Ditto Based on ASME B16.5
 7.
      285 @ 20/100
 8
      <del>200.@400---</del>
                     -CL-150
 9
      B16.5 0.0625 Carbon Steel, Externally Coated
10
      1/2" 1 1/2", XS
      2" 24" STD Carbon Steel, Externally Coated Carbon Steel, Externally Coated Carbon Steel, Externally Coated
11
12
                           - 304 SS Spiral-Wound /ASME B16.20
13
      C14A
14

    ASME B31.3, Normal Fluid Service

      <del>(CK)-</del>
15
      (WF) River Water
16
      (WP) Process Water Based on ASME B16.5
      <del>285 @ - 20/100</del>
17
                   __CL 150
18
      <del>200 @ 400__</del>
      B16.5 0.125 Carbon Steel
19
20
      1/2" 2", XS
21
      3" 24", STD Carbon Steel
                                    Carbon Steel Carbon Steel
                                                                    13CR HFS
                                                                                   304 SS Spiral Wound /ASME
22
      B16.20
23
      CK1M
24
      (CM) -- ASME B31.3, Normal Fluid Service
25
      (CH) High Pressure Air
26
      (CN) High Pressure Nitrogen Based on Design
27
      4,000 @ 200 --- CL 2500
28
      B16.5 - 0.0312 - Carbon Steel
29
      1/2" 6", XXS - Carbon Steel-
                                                   -Carbon Steel
                                                                   -13CR-HFS
                                                                                    Soft Iron RTJ/ ASME B16.20
                                     Carbon Steel
30
      CK2N
31
      (CN)
             -ASME-B31.3, Normal Fluid Service
32
      (WQ) High Pressure-Water, 3675 Psig Based on Design
33
      3,675 @ 200 CL 2500
      B16.5 0.0625 Carbon Steel
34
35
      1/2" 6", XXS Carbon Steel Carbon Steel Carbon Steel 13CR-HFS
                                                                                   Soft Iron RTJ/ ASME B16.20
36
      FIOA
37
            -- ASME B31.3, Category M Fluid Service
38
      Radioactive, Dangerous-Liquid Effluent Line-
                                                     Based on Design
39
      150 @ 200
                     CL 150
40
      B16.5 0.000 Double Containment Fiberglass Reinforced Thermosetting Resin

    Double Contain-ment Fiberglass

41
      Reinforced Thermosetting Resin - Double Contain ment Fiberglass Reinforced Thermo-setting Resin - PVDF - EPDM/
42
      Viton EPDM/ Viton
43
      G<sub>12</sub>A
44
      (CW) - Uniform Plumbing Code
45
      (WV) Potable Water Based on Design
46
      200 @ 150
                      CL 150
47
      B16.5 0.050
                     Carbon Steel, Galvanized
      1/2" 3", XS
48
49
      4" 12", STD Ductile Iron, Galvanized Malleable Iron, Galvanized Cast Bronze/ Ductile Iron Bronze EPDM
50
      HOOA
51
             -- Uniform Plumbing Code
      (JB)
      (WV) Potable Water Based on Design
52
53
                      TBD 0.000 Cement Mortar Lined Ductile Iron Pressure Pipe Cement Mortar Lined Ductile Iron
      200 @ 150
. 54
              None -
                      None-
                                     Synthetic Rubber
```

```
LE0A
1
     (JA) NFPA 24
2
     (WF) Fire Protection, Underground Based on Design
3
     175 @ Ambient - CL-125
4
     B16.1 0.000 Cement Mortar Lined Ductile Iron Pressure Pipe Cement Mortar Lined Ductile Iron or Gray Iron
5
6
            None Cast Iron Cast Iron/ Bronze Rubber or Neoprene
7
     N11E
8

    ASME B31.3, Category M-Fluid-Service

9
     Highly Corrosive Process Fluids in High Active Cells Based on Design
                                0.0312 Hastelloy C 276
10
     110@360
                    No Flanges
     1/2" 2", Sch. 40S
11
12
     3" 8", Sch. 10S Hastelloy C 276 Hastelloy C 276 No Valves No Valves

    No Gaskets

13
     NHF
14
     (TF)

    ASME B31.3, Category M Fluid Service

15
      (ZF) Plant Washings Based on Design
     100 @ 200 TBD
                           0.0425 SS AL-6XN
16
17
     (UNS N08367)
18
      1/2" 4", Sch. 40S
19
      6" 24", Sch 10S
20
      30", Sch 10S
                  - SS-AL-6XN
21
      (UNS N08367) SS AL 6XN
22
      (UNS N08367) TBD TBD TBD
23
     N<sub>13</sub>A
24
            ASME B31.3, Category M Fluid Service
25
      TBD Based on Design
                   TBD 0.093 Hastelloy C-22
26
      10 @ 600 -
27
      (UNS N06022) Hastelloy C-22
28
      (UNS N06022) TBD TBD
                                   TBD TBD
29
      N31C
30
      (TC) ASME B31.3, Category M Fluid Service
31
      (TBD) In Cell Process Piping
32
      (TBD)- In-Cell Caustic Lines
                                  Based on Design
      20 @ 520 None 0.0312 Inconel 600
33
      1/2" 2", Sch. 40S
34
35
      3" 6", Sch. 10S Inconel 600
                                  - Inconel 600 -
                                                 No Valves
                                                                 No Valves
36
      P10A
37
      (PA) Uniform Plumbing Code
38
      (WB) Potable Water, Underground
                                           Based on Design
39
      200 @ 73
40
      124@100
41
                    TBD 0.000 PVC
      80@120
42
      1" 2", Sch. 80
43
      3" 12", Pressure Class 200 PVC PVC 1" 2", Bronze
44
      3"-12", Cast Iron/ Internally Coated Bronze Synthetic Rubber/ ASTM F477
45
      P10C
46
      (PC) ASME B31.3, Category D Fluid Service
47
      Underground Services:
48
      (WE) Demineralized Water
49
      (WR) River Water
50
      (WB) Cooling Water Supply
      (WC) - Cooling Water Return
51
52
      (ZA) Non Dangerous, Non-Radioactive Liquid Effluent
53
      (WK) Chilled Water Supply
54
      (WL) - Chilled Water Return
                                   Based on Design
```

```
150 @ 0/100
 2
      B16.5 0.000 PVC
      12" & Smaller, Sch. 80
                             PVC PVC PVC
                                                    -PVC/ Viton-
 5

    ASME B31.3, Category D Fluid Service

 6
      (WY) Sewer Based on Design
 7
      150 @ 73
 8
      <del>60 @ 120</del>
                      -CL 150
 9
      B16.5 - 0.000 - PVC
      12" & Smaller, Sch. 40 PVC PVC PVC PVC/Viton Neoprene
10
11
12
              ASME B31.3, Category D Fluid Service
13
      (WY)-
            -Sanitary Sewer Tile Drain Gravity @ Ambient/120 - CL 150
14
      B16.5 - 0.000 - PVC
15
      4", SDR-35
                    PVC None None None Neoprene
16
      SIOA
17

    ASME B31.3, Category Normal Fluid Service

      (SA)
18

    Instrument Air Based on ASME B16.5

19
      <del>230.@ 20/100</del>
20
      195@200
                     - CL-150
      B16.5 0.000 304LSS
21
22
      1/2" 2", Sch. 40S
23
      3" 24", Sch. 10S
                              304L SS 304L SS 304L SS 316SS HFS 316 SS Spiral Wound / ASME B16.20
24
      SIIB
25
      (SB)
26
              ASME B31.3, Category M Fluid Service
27
      In Cell Piping with < 2% Solids (Process, Services, Reagents, and Vessel Vents) Based on ASME B16.5, Class 150
28
      <del>230 @ - 20/100</del>
29
      <del>166 @ 360</del>
              No Flanges
30
                              -0.0312 316L SS
31
      1/2" 2", Sch. 40S
32
      3" 24", Sch. 10S
                              316L SS 316LSS TBD TBD None
33
      SHC
34
       (SC)
              ASME B31.3, Category Normal Fluid Service
35
      (ZS)
              Process Radioactive Condensate
36
              Suspect Radioactive Condensate
       (ZR)
37
       (WG)
              Re circulated Emergency Cooling Suspect Radioactive
38
              Recirculated Cooling Suspect Radioactive
       (WS)
39
       (WE)
              Demineralized Water
40
       (WD) Inhibited Water
41
       (ZB)
             Biocides
42
              Corresion Inhibitors
       (ZC)
                                      Based on ASME B16.5
43
       230 @ 20/100
44
       166 @ 360-
                    ---CL-150
45
       B16.5 - 0.0312 - 316L SS
46
       1/2" 2", Sch. 40S
47
       3" 14", Sch. 10S
48
       16" 20, 0.250" nom.
49
       24" 0.312" nom. 316L SS 316L SS 316L SS 316SS HFS
                                                              316 SS Spiral Wound /ASME B16.20
50
       S11F
51
             —ASME B31.3, Category M Fluid Service
52
       In Cell Piping with < 2% Solids (Process, Services, Reagents, and Vessel Vents that Contain Nitric Acid) Based on ASME
.53
       B16.5., Class 150
54
       230 @ - 20/100
```

```
<del>166 @ 360</del>
 2
              No Flanges
                              0.0312 304L SS
      1/2" 2", Sch. 40S
 3
 4
      3" -24", Sch. 10S
                              304L SS 304L SS TBD TBD
 5
      SHG
 6

    ASME B31.3, Category Normal Fluid Service

 7
      (XL)
             -Lubricating Oil
 8
      (XH) Hydraulic Oil
 9
              Transformer Oil Based on ASME B16.5
      (XJ)
10
      230 @ - 20/100
11
      195 @ 200
                     -CL-150
      B16.5 0.0312 304L SS
12
      1/2"-2", Sch. 40S
13
14
      3" 10", Sch 10S304L SS 304L SS 316SS HFS
                                                             - 316 SS Spiral Wound /ASME B16.20
15
      S11K
16

    ASME B31.3, Category Norm Fluid Service

17
      (GM)
             -- Ammonia
18
              Calcium Nitrate
      (RC)
19
              Potassium Permanganate
      (RL)
20
      (RK)
              -Sodium Permanganate
21
      <del>(RQ)-</del>
             —1M Strontium Nitrite
22
              -Strontium Carbonate
23
              Ammonium Hydroxide
24
      (RN) - 0.5M Sodium Nitrite
25
      (JS)
              0.5M Sodium Hydroxide
26
             -5M Sodium Hydroxide
      (JS)
27
      (ZK)
              Fresh Ion Exchange [IX] Resin
28

    Off-Specification Resin—Based on ASME B16.5

      (ZM)
29
      230 @ - 20/100 - CL 150
30
      B16.5 0.0312 304LSS
31
      1/2" 2", Sch. 40S
32
      3" 14", Sch. 10S
33
      16" 20", 0.250" nom.
34
      24", 0.312" nom. 304L SS 304L SS 304L SS 316L SS HFS
                                                               316 SS Spiral-Wound /ASME B16.20
35
      S11M
36
      (SM)
              ASME B31.3, Category M Fluid Service
37
      (GV)
              Radioactive Vessel Vent
38
      (PW)
              Radioactive Gas/Vapor
39
      (ZE)
              Plant Wash Solvent
40
              Plant Washings
      (ZF)
41
       (ZH)

    Acidic Effluents

42
      <del>(ZJ)</del>
              Alkaline Effluents
43
              -Spent Ion Exchange Resin
      (ZL)
44
      (ZN)
              Neutralized Effluent
45
             -Scrubber EffluentBased on ASME-B16.5
      (ZY)
46
      230 @ 20/100 CL 150
47
      B16.5 - 0.0312 - 316L SS
48
      1/2" 2", Sch. 40S
49
      3" 24", Seh. 10S
                              316L SS316L SS316L SS316L SS HFS 316 SS Spiral Wound /ASME B16.20
50
      SHP
51

    ASME B31.3, Category M Fluid Service

52
              Thermocouple Sheathed Line In Cell-
                                                       Based on ASME B16.5
53
      230 @ -20/100 None - 0.0312 - 316L SS
```

```
1.
      1/2" 3/4", Sch. 10S
                             None No fitting, Use Type 316L Jointing Sleeve No Valves
 2
      Gaskets
 3
      SHR
 4
      (SR)
              ASME B31.3, Category Norm Fluid Service
 5
      (HN)

    0.5M Nitric Acid

      (HN)
 6
             -2M Nitric Acid
 7
             -5M Nitric Acid
      (HN)
 8
      (HN) 12.2M Nitric Acid
 9
      (HR)-

    Recovered Nitric Acid

10
            --Citric Acid (SDG3)
      (HT)
11
                                     Based on ASME B16.5
      (GU) — Nitric Acid Fume
12
      230@ 20/100 CL 150
13
      B16.5 0.0312 304L SS
14
      1/2" 2", Sch. 40S
15
      3" 14", Sch 10S
16
      16" 20", 0.250" nom.
17
      24", 0312" nom. 304L SS 304L SS 304L SS 304L SS HFS 304SS Spiral-Wound /ASME B16.20
18
      S11¥
19
             - ASME B31.3, Category M Fluid Service
      (SY)
20
      (ZG)
            Pneumercator Line
21
      (ZP)
            - Pneumatic Sample-Line
      (ZQ) Pneumatic Service Line Based on ASME B16.5
22
23
      230 @ 20/100 TBD 0.0312 316L SS
      1/2" 3/4", Sch. 40S None 316L SS No Valves
24
                                                            No Valves
                                                                            No Gaskets
25
      S12A
26
      (LB) ASME B31.3, Category M Fluid Service
27
      In Cell Piping with ≥2% solids (Process, Services, Reagents, and Vessel Vents) Based on ASME B16.5, Class 150
28
      230 @ 20/100
29
      166@360
30
             No Flanges
                             <del>-0.0625 - 316L SS</del>
31
      1/2" -: 2", Sch. 40S
      3" 14", Sch. 10S
32
33
      16" 24", 0250" nom.
                             -316L SS 316L SS TBD --
34
      S12C
35
      (LE)
36
      (>2% solids)

    ASME B31.3, Category M Fluid Service

37
      (PA) - Radioactive Aqueous
38
      (PX) — Radioactive Slurry
                                     Based on ASME B16.5
39
      230 @ 20/100 CL 150
40
      B16.5 0.0625 316L SS
41
      1/2" 2", Sch. 40S
42
      3"-14", Sch. 10S
43
      16" 24", 0.250" nom. 316L SS 316L SS 316L SS 316L SS 316 SS Spiral Wound / ASME B16.20
44
45
      (LF) — ASME B31.3, Category M Fluid Service
46
      In Cell Piping with ≥ 2% Solids (Process, Services, Reagents, and Vessel Vents that Contain Nitric Acid) Based on ASME
47
      B16.5, Class 150
48
      230@ 20/100
49
      166 @ 360
                    -No-Flanges-
                                    -0.0625 304L-SS
50
      1/2" 2", Sch. 40S
51
      3" 14", Seh. 10S
52
      16" 24", 0.250" nom. 304L SS 304L SS TBD
                                                    TBD None
53
54
      (TD) ASME B31.3, Category M Fluid Service
```

```
(FX) Mixed Glass Former
1
2
     Solids high erosion
                          Based on ASME B16.5
3
     230 @ 20/100
     195 @ 200 —
                   -CL-150
     B16.5 0.125 316L SS
5
6
     1/2" 1", Sch. 160
     1-1/2" 2", Sch. 80S
7
8
     3"-12", Sch. 40S-
                          -316L SS316L SS316L SS316L SS HFS - 316 SS Spiral Wound / ASME B16.20
9
     $30J
     (SJ) -- ASME B31.3, Normal Fluid Service
10
11
     Liquid Carbon Dioxide Based on Design
     300 @ 50 CL 300
12
13
     B16.5 - 0.000 - 304L SS
14
      1/2" 2", Sch. 40S
15
      3" 12, Sch. 10S 304L SS 304L SS 304L SS (Later) 316 SS Spiral Wound / ASME B16.20
16
     S31H
17
     (SH)
             ASME B31.3, Category M Fluid Service
18
19
      <2% Solids In Cell Piping (Process and Vessel Vents)</p>
                                                        Based on ASME B16.5
20
      600 @ 20/100
21
      505 @ 200 ·
                    -CL-300
22
      B16.5 - 0.0312 - 316L SS
23
      1/2" 12", Sch. 40S 316L SS316L SSTBD TBD None
24
25
      (ST) ASME B31.3, Category M Fluid Service
26
      Service Bulges, Process Bulges, Cabinets Based on Design
27
      385 @ 400 CL 300
28
      B16.5 0.0312 316LSS
29
      1/2" 12", Sch. 40S 316L SS316L SS316L SS316L SS HFS 316 SS Spiral-Wound /ASME B16.20
      S31U
30
31
      (SU)
32
            ASME B31.3, Category M Fluid Service
33
      < 2% Solids In Cell Piping (Process, and Vessel Vents that Contain Nitric Acid)) Based on ASME B16.5
34
      600 @ 20/100
35
      505 @ 200 CL 300
      B16.5 0.0312 304L-SS
36
37
      1/2" 12", Sch. 40S 304L SS304L SSTBD TBD None
38
      S32A
39
      (LH) ASME B31.3, Category M Fluid Service
40
      ≥ 2% Solids In Cell Piping (Process and Vessel Vents)
                                                          Based on ASME B16.5
41
      600 @ - 20/100
42
      505 @ 200 CL 300
43
      B16.5 0.0625 316L SS
44
      1/2" 12", Sch. 40S
      14", 0.375" nom.
45
46
      16" 18", 0.437" nom.
47
      20", 0.500" nom.
48
      24", 0.562" nom. 316L SS 316L SS TBD TBD None
49
      S32B.
50
      (LW)
51
      (≥ 2% Solids) (PE) Entrained Solids Concentrate;
52
            - HLW Melter Feed;
      (PC) HLW Feed Slurry
53

    Double Containment Pipe

54
             -INNER
```

```
PIPE ASME B31.3, Category M Fluid Service Based on Design
1
2
     400 @ 160 TBD 0.0625 316L SS
     1/2" 4", Sch. 40S
3
                           None Use Bends for Directional Change No Valves
                                                                             No Valves
            OUTER
5
     PPE ASME B31-3, Category D Service Fluid TBD TBD 0.0000 316L SS
6
     4" 8", Sch. 10S Not Permitted Except Where Fitting Radius Equals Bend Radius No Valves
7
            None
8
     S62A
9
     (LU) - ASME B31.3, Category M Fluid Service
10
     ≥ 2% Solids In Cell Piping (Process and Vessel Vents that Contain Nitric Acid) Based on ASME B16.5
     600 @ - 20/100
11
     505@200-
12
                  --- CL 300
13
     B16.5 0.0625 304L SS
     1/2" 12", Sch. 40S
14
15
     14", 0.375" nom.
16
     16" 18", 0.437" nom.
17
     20", 0.500" nom.
18
     24", 0.562" nom. 304L SS304L SSTBD TBD None
19
     SJOE
20
     (SE) ASME B31.3, Category Normal Fluid Service
21
      (GL) Instrument Air Back Up Based on ASME B16.5
22
     3000 @ 20/100
23
     2530 @ 200
                   CL 1500
24
     B16.5 - 0.000 - 304L SS
25
     1/2"-1", Sch. 80S
26
     1-1/2", 0.250" nom 2", 0.312" nom.
27
     3", 0.437" nom. 304L SS 304L SS 304L SS 316SS HFS Soft Iron RTJ/ ASME B16.20
28
     T11A
29
      (ZA) ASME B31.3, Category M Fluid Service
30
      (HC) Cerium De contaminant
      (ZX) Special De contaminant Based on Design
31
      32
33
      (ASTM B337-Gr. 2)
34
      1/2". 2", Sch. 40S
      3" - 6", Sch. 10S Titanium -
35
                                  Titanium-
                                                 No Valves
                                                                No Valves
36
      W31A
37
      (WA)
      (< 2% Solids)
38
39

    Radioactive Effluent (LA Effluents/Process Fluids)

40
             Cs/Tc Concentrate/Intermediate Product — Double Containment Pipe
41
            --INNER
42
      PIPE ASME B31.3, Category M Fluid Service
                                                 -Based on Design
43
      400 @ 160
                  TBD 0.0312 316L SS
44
      1/2" 2", Sch. 40S
      3" 4", Sch. 10S None - Use Bends for Directional Change - No Valves - No Valves - None
45
46
47
      PIPE ASME B31.3, Category D Service Fluid TBD 7BD 0.0000 316L SS
48
      4" 8", Sch. 10S Not Permitted Except Where Elbow Radius Equals Bend Radius No Valves
                                                                                             No Valves
49
            -None
50
      W62F
51
      (XA) DST Transfer Line Double Containment Pipe
52
53
            ASME B31.3, Category M Fluid Service Based on Design
54
      1000 @ 160 None - 0.0625 304L SS
```

1/2" 4", Sch. 80S None Use Bends for Directional Chan	nge No Valves No Valves None
OUTER	
PIPE ASME B31.3, Category D Fluid Service TBD TB: 4"-8", STD Not Permitted Except Where CS Fitting Radius None	BD 0.0000 Carbon Steel, A106 B, Smls Equals Bend Radius No Valves No Valves

Table 4-2 Container Storage Areas Summary

Container Storage Area	Maximum Waste Volume (US Gallons)_1	Approximate Dimensions $(L \times W \times H, \text{ in feet})^2$
HLW Vitrification Plant		
IHLW Canister Storage Storage AreaCave (H-0132)	245,50 4 <u>162,589</u>	$\frac{(67 \times 23 \times 27) + (67 \times 34 \times 27)\underline{63} \times}{23 \times 15}$
HLW Container Storage Area No. 1East Corridor El. 0' (HC-0108/09/10)	266,65 4 <u>310,291</u>	122 × 34 × 37 <u>10</u>
HLW Container Storage Area No. 2Loading Area (H-0130)	71,999 <u>159,185</u> 43,392	56 × 20 <u>38</u> × 27 <u>10</u>
HLW Container Storage Area No. 3	+3,372	4 5 × 15 × 37
Analytical Laboratory	<u>''</u>	
Laboratory Waste Management Area (A-0139 and A-0139A)	119,613	41 × 39 × 10
Other Areas	<u>'</u>	
Central Waste Storage Facility	617,137	80 × 120 × 10
Non-Radioactive Dangerous Waste Container Storage Area	4 8,21 4 <u>56,104</u>	25 × 30 × 10
HLW Failed Melter Out Of Service Storage	202,498 <u>403,947</u>	70 75 × 45 × 35 16
Area Facility LAW Melter Out Of Service Storage Area	216,962	45 × 75 × 35

The conversion factor used to convert from cubic feet to gallons is 7.4805 gal/ft³

The dimension for height (H) is based on the height of the largest waste container stored in the area (i.e., LAW container is 7.5 ft, HLW canister is 15 ft, melters are assumed to be 16 ft, and a B-25 box is 5 ft - stacked a maximum of two high is 10 ft).

Lable	4-3	Pretreatment Plant Tank Sy	stems			
No.	System	Vessel Number	Description	Material of Construction	Maximum Total Volume (US gGallons)	Approximate Dimensions (Diameter [D] × Height or/ Length [H/L] in inchesfeet)
1	FRP	V11020AFRP-VSL-00002	Waste Feed Receipt Vessel	Stainless Steel	388,000<u>474,000</u>	552 × 46847 × 26.75
		<u>A</u>				
2	FRP	\frac{\foating V11020BFRP-VSL-00002}{B}	Waste Feed Receipt Vessel	Stainless Steel	388,000<u>474,000</u>	552 × 46847 × 26.75
3	FRP	V11020C FRP-VSL-00002 C	Waste Feed Receipt Vessel	Stainless Steel	388,000<u>474,000</u>	552 × 468 <u>47 × 26.75</u>
4	FRP	V11020DFRP-VSL-00002 D	Waste Feed Receipt Vessel	Stainless Steel	388,000<u>474,000</u>	552 × 46847 × 26.75
5	FEP	V11001AFEP-VSL-00017 A	Waste Feed Evaporator Feed Vessel	Stainless Steel	59,070 <u>85,557</u>	264 × 336 22 × 22.75
6	FEP	V11001BFEP-VSL-00017	Waste Feed Evaporator Feed Vessel	Stainless Steel	59,070 85,557	264 × 33622 × 22.75
	FEP	<u>B</u>	Waste Feed Evaporator Separator Vessel	Stainless Steel	, ,	132 × 402
	FEP	V11002A V11002B	Waste Feed Evaporator Separator Vessel	Stainless Steel	2 1,240	132 × 402
7	FEP	V11005 <u>FEP-VSL-00005</u>	LAW Feed Evaporator Process-Condensate PotVessel	Stainless Steel	1,190 5,022	60 × 1168 × 10.75
8	UFP	V12015A <u>UFP-VSL-00062</u> A	LAW-Ultrafilter Permeate Hold-Vessel	Stainless Steel	28,390 34,700	$180 \times 31715 \times 21.25$
9	UFP	V12015B <u>UFP-VSL-00062</u> B	Ultrafilter Permeate VesselLAW Permeate Hold Vessel	Stainless Steel	28,390 <u>34,700</u>	180 × 31715 × 21.25
10	UFP	V12015C <u>UFP-VSL-00062</u> C	Ultrafilter Permeate VesselLAW Permeate Hold Vessel	Stainless Steel	28,390 <u>34,700</u>	180 × 317 15 × 21.25
11	UFP	V12010AUFP-VSL-00001 A	Ultrafiltration Feed Preparation Evaporator Concentrate Buffer Vessel	Stainless Steel	62,340 <u>75,593</u>	240 × 39720 × 25.5
12	UFP	V12010B UFP-VSL-00001	Ultrafiltration Feed Preparation	Stainless Steel	62,340 <u>75,593</u>	240 × 39720 × 25.5
		<u>B</u>	VesselEvaporator Concentrate Buffer			
			Vessel			

Table	<u> </u>	retreatment Plant Tank Sy			,	Approximate Dimensions
No.	System	Vessel Number	Description	Material <u>of</u> Construction	Maximum Total Volume (US gGallons)	(Diameter [D] × Height o <u>r/</u> Length [H/L] in inchesfeet)
13	UFP	V12011A <u>UFP-VSL-00002</u> A	Ultrafiltration Feed Vessel	Stainless Steel	26,84040,783	168 × 33514 × 30.75
14	UFP	V12011BUFP-VSL-00002 B	Ultrafiltration Feed Vessel	Stainless Steel	26,840 40,783	168 × 335 14 × 30.75
15	UFP	G12002AUFP-FILT-00001 A	Ultrafilter	Stainless Steel	140	17 × 145 1.5 × 12
16	UFP	G12002BUFP-FILT-00001 B	Ultrafilter	Stainless Steel	140	17 × 1451.5 × 12
17	UFP	G12003AUFP-FILT-00002 A	Ultrafilter	Stainless Steel	140	17 × 145 1.5 × 12
18	UFP	G12003BUFP-FILT-00002 B	Ultrafilter	Stainless Steel	140	17 × 145 1.5 × 12
19	UFP	G12004AUFP-FILT-00003 A	Ultrafilter	Stainless Steel		17 × 145 1.5 × 12
20	UFP	G12004BUFP-FILT-00003 B	Ultrafilter	Stainless Steel		17 × 1451.5 × 12
21	HLP	V12007HLP-VSL-00028	HLW Feed Blending Vessel	Stainless Steel	18,070 <u>142,200</u>	144 × 304 <u>26.5 × 29</u>
22	HLP	V12001A <u>HLP-VSL-00027</u> A	Strontium/transuranie <u>HLW</u> Lag Storage Vessel		96,900 127,260	300 × 415 25 × 29.5
23	HLP HLP	V12001CHLP-VSL-00027 B V12001D	HLW Lag Storage VesselStrontium/transuranic Lag Storage Vessel Lag Storage Vessel	Stainless Steel Stainless Steel	96,900<u>172,260</u> 96,900	300 × 41525 × 29.5 300 × 415
24	HLP	HLP-VSL-00022V12001E	HLW Feed Receipt VesselLag Storage Vessel	Stainless Steel	96,900<u>270,600</u>	300 × 415 38 × 24.25
25	CXP	C13001CXP-IXC-00001	Cesium Ion Exchange Column	Stainless Steel	680	$42 \times 1263.5 \times 10.5$
26	CXP	CXP-IXC-00002C13002	Cesium Ion Exchange Column	Stainless Steel	680	3.5 × 10.542 × 126
27	CXP	CXP-IXC-00003C13003	Cesium Ion Exchange Column	Stainless Steel	680 .	$3.5 \times 10.542 \times 126$

	_			Material of	Maximum-Total Volume (US	Approximate Dimensions (Diameter [D] × Height or Length [H/L] in
No.	System	Vessel Number	Description	Construction	gGallons)	inchesseet)
28	CXP	CXP-IXC-00004C13004	Cesium Ion Exchange Column	Stainless Steel	l	$3.5 \times 10.542 \times 126$
29	CXP	V13001 CXP-VSL-00001	LAW Cesium Ion Exchange Feed Vessel	Stainless Steel	61,200 103,350	228 × 42123 × 28.5
30	CXP	V13008CXP-VSL-00004	Cesium Ion Exchange Caustic Rinse Collection Vessel	Stainless Steel	2,400 11,085	78 × 14210.5 × 14.25
31	CXP	CXP-VSL-00005	Cesium Reagent Vessel	Stainless Steel	1.180	<u>5 × 9</u>
32	CXP	CXP-VSL-00026A	Cesium Ion Exchange Treated LAW Collection Vessel	Stainless Steel	36,480	15 × 24.5
33	CXP	CXP-VSL-00026B	Cesium Ion Exchange Treated LAW Collection Vessel	Stainless Steel	36,480	15 × 24.5
34	CXP	CXP-VSL-00026C	Cesium Ion Exchange Treated LAW Collection Vessel	Stainless Steel	36,480	15 × 24.5
35	CNP	V13073CNP-VSL-00003	Eluate Contingency Storage Vessel	Stainless Steel	11,060 <u>23,200</u>	138 × 21614 × 17.25
36	CNP	V13028CNP-VSL-00004	Cesium Evaporator Recovered Nitric Acid	Stainless Steel	5,410 11,115	96 × 2049.5 × 19
	CNP	V13030	Vessel	Stainless Steel		17×36
	TXP	V43001	Cesium Concentrate Lute Pot	Stainless-Steel	1 7	156 × 270
	TXP	C43006	Technetium Ion Exchange Buffer Vessel	Stainless-Steel		42 × 126
	TXP	C43007	Technetium Ion Exchange Column	Stainless-Steel		42 × 126
	TXP	C43008	Technetium Ion Exchange Column	Stainless-Steel		42 × 126
	TXP	C43009	Technetium Ion Exchange Column	Stainless Steel		42 × 126
	TXP	V43056	Technetium Ion Exchange Column Caustic Rinse Collection Vessel	Stainless Steel	3,300	96 × 137
37	CNP	CNP-VSL-00001	Cesium Evaporator Eluant Lute Pot	Stainless Steel	109	<u>4 × 3</u>
38	TLP	TLP-VSL-00002	Treated LAW Evaporator Condensate Vessel	Stainless Steel	2,300	6 × 9
39	TLP	V45009ATLP-VSL-00009 A	LAW Plant Wash SBS Condensate Receipt Vessel	Stainless Steel	88,920 <u>130,010</u>	264 × 462 26 × 27.25
40	TLP	TLP-VSL-00009BV45009	LAW SBS Condensate Receipt VesselPlant Wash Vessel	Stainless Steel	88,920 130,010	264 × 462 26 × 27.25

1 2016	T-3.	retreatment Plant Lank Sys	1 21GTI12	1	<u> </u>	A A Discount of
				Material of	Maximum-Total Volume (US	Approximate Dimensions (Diameter [D] × Height or/ Length [H/L] in
No.	System	Vessel Number	Description	Construction	gGallons)	inchesfeet)
41	TCP	V41001 <u>TCP-VSL-00001</u>	Treated LAW Concentrate Buffer Storage Vessel	Stainless Steel	117,000 <u>146,740</u>	312 × 45626.5 × 30.25
42	RDP	V43135 A <u>RDP-VSL-00002</u> A	Spent Resin Collection Slurry Vessel	Stainless Steel	8,72 0 <u>15,240</u>	118 × 196 12 × 14
43	RDP	RDP-VSL-00002BV43135	Spent Resin Collection-Slurry Vessel	Stainless Steel	8,720 15,240	118 × 19612 × 14
44	RDP	RDP-VSL-00002CV43136	Spent Resin Flush Collection-Slurry Vessel	Stainless Steel	11,220 15,240	144 × 20612 × 14
45	RDP	RDP-VSL-00004	Spent Resin Dewatering Moisture Separation Vessel	Stainless Steel	TBD	TBD.
46	RLD	¥45028ARLD-TK-00006A	Process Condensate VesselTank	Stainless Steel	321,720 394,000	480 × 492 <u>40 × 45</u>
47	RLD	RLD-TK-00006BV45028B	Process Condensate Vessel Tank	Stainless Steel	321,720 <u>394,000</u>	4 80 × 492 40 × 45
48	RLD	RLD-VSL-00017A	Alkaline Effluent Vessel	Stainless Steel	4 2,950 34,340	16 × 23.25 <u>17.5</u>
49	RLD	RLD-VSL-00017B	Alkaline Effluent Vessel	Stainless Steel	4 2,950 34,340	16 × 23.25 <u>17.5</u>
50	PWD	V15009BPWD-VSL-00033	Ultimate Overflow Vessel	Stainless Steel316L	23,000 41,650	216 × 216 24 × 7.5
51	PWD	V12002PWD-VSL-00043	HLW Effluent Transfer Vessel	316L Stainless Steel	23,000 41,650	216 × 216 24 × 7.5
52	PWD	PWD-VSL-00015V15013	Acid/Alkaline Effluent Vessel	Stainless Steel	93,180 119,150	264 × 480 22 × 34.5
53	PWD	PWD-VSL-00044V15009A	Plant Wash Vessel	Stainless Steel	73,860 103,024	$456 \times 24023 \times 25.5$
54	PWD	PWD-VSL-00046V15319	C3 Floor Drains Collection - Tank Vessel	316L Stainless Steel	4 50 4.982	36 × 728 × 10.5
55	PWD PVP	V15018PWD-VSL-00016 PVPVSL00003V15052	Acid/Alkaline Effluent Vessel Vessel Vent Header Collection Vessel	Stainless Steel Stainless Steel	93,180 <u>119,150</u> 900	264 × 48022 × 34.5 54 × 108
	₽V₽	V15038	Condensate Collection Vessel	Stainless Steel	1,230	60 × 120
56	PVPPJ V	PJV-VSL-00002 V15327	PJV HEME Drain Collection Vessel	Stainless Steel	2,760 <u>8,975</u>	72 × 18010 × 12
57	PVP	PVP-VSL-00001	Vessel Ventilation HEME Drain Collection Vessel	Stainless Steel	820 1,969	<u>6 × 7.25</u>

Table 4-3	Pretreatment Plant Tank Systems
-----------	---------------------------------

		TOTAL DESCRIPTION OF THE PROPERTY OF	Judalio		· ·	
	•					Approximate Dimensions
					Maximum Total	(Diameter [D] × Height
				Material of	Volume (<u>US</u>	or/ Length [H/L] in
No.	System	Vessel Number	Description	Construction	gGallons)	inchesfeet)
58	<u>SHR</u> PV	V15326SHR-TK-00009	HEME Drain Collection VesselFeed Line	Stainless Steel	820 14,900	$48 \times 12015 \times 13.75$
	Þ		Flush Tank			
59	PIH	PIH-TK-00001	Decontamination Soak Tank	Stainless Steel	TRD	TBD

Table 4-4 LAW Vitrification Plant Tank Systems

No.	System	Vessel Number	Description	Material	Maximum Total Volume (US Ggallons)	Approximate Dimensions ({Diameter (D) × Height./or_Length-(H/L) in feet})
1	LCP	V21001 LCP-VSL-00001	Melter 1 Concentrate Receipt Vessel	Stainless Steel	14,392 18,130	13 × 17 14 × 12.75
2	LCP LCP	V21002 LCP-VSL-00002 V21003	Melter 2 Concentrate Receipt Vessel Melter 3 Concentrate Receipt Vessel	Stainless Steel Stainless Steel	14,392 <u>18,130</u> 14,392	13 × 17 14 × 12.75 13 × 17
3	LFP	V21101LFP-VSL-00001	Melter 1 Feed Preparation Vessel	Stainless Steel	6,221 9,123	10 × 12 11 × 10.5
4	LFP	V21102 LFP-VSL-00002	Melter 1 Feed Vessel	Stainless Steel	6,221 9,123	10 × 12 <u>11 × 10.5</u>
5	LFP	V21201 LFP-VSL-00003	Melter 2 Feed Preparation Vessel	Stainless Steel	6,221 9,123	10 × 1211 × 10.5
6	LFP LFP LFP	V21202LFP-VSL-00004 V21301 V21302	Melter 2 Feed Vessel Melter 3 Feed Preparation Vessel Melter 3 Feed Vessel	Stainless Steel Stainless Steel Stainless Steel	6 ,221 9 <u>,123</u> 6 ,221 6 ,221	$10 \times 1211 \times 10.5$ 10×12 10×12
7	LVP	V22001 LVP-TK-00001	LAW Caustic Scrubber Blowdown VesselCollection Tank	Stainless Steel	12,191 14,579	14 × 1414.3 × 13
8	LOP	V22101 LOP-VSL-00001	Melter 1 SBS Condensate Vessel	Hastelloy	6,833 <u>9,056</u>	8 × 2012 × 8.2
9	LOP LOP	V22201 LOP-VSL-00002 V22301	Melter 2 SBS Condensate Vessel Melter 3 SBS Condensate Vessel	Hastelloy Hastelloy	6,833 9,056 6,833	8 × 2012 × 8.2 8 × 20
10	RLD	V25001RLD-VSL-00003	Plant Wash Vessel	Stainless Steel	25,130 <u>25,780</u>	14 × 2616 × 14.6
11	RLD	V25002 RLD-VSL-00004	LAW C3/C5 Effluent Drains/Sump Collection Vessel	Stainless Steel		10 × 13 10 × 11
12	RLD	V25003RLD-VSL-00005	SBS Condensate Collection Vessel	Stainless Steel	24,704 <u>25,780</u>	16 × 18 16 × 14.6

Table 4-5 HLW Vitrification Plant Tank Systems

Labie	4-0 1	LW Vitrification Plant Ta	nk Systems		·	
No.	Criston	Vessel Number	Deganintion	Madadal	Maximum Total Volume	Approximate Dimensions (Diameter [D] × Height / in Length [H/L]
110.	System		Description	Material	(US Ggallons)	in feet)
1	НСР	V31001 HCP-VSL-00001	Concentrate Receipt Vessel 1	Stainless Steel	17,900 <u>20,0612</u> 0,229	14 × 18
2	НСР	V31002 HCP-VSL-00002	Concentrate Receipt Vessel 2	Stainless Steel	17,900 <u>20,0612</u> 0,229	14 × 18
3	HOP	V32101 HOP-VSL-00903	SBS Condensate Collection-Receiver Vessel No. 1	Hastelloy	10,000 <u>9,9419,8</u> 91	12 × 14
4	<u>HOP</u>	HOP-VSL-00904	SBS Condensate Receiver Vessel No. 2	<u>Hastelloy</u>	<u>.949,891</u>	12 × 14
5	HDH	V33004HDH-VSL-00001	Canister Rinse Bogie Decontamination Vessel	Stainless Steel	2,500 <u>3,3063,31</u> <u>4</u>	5 × 17 <u>6 × 17</u>
6	HDH	V33002HDH-VSL-00003	Waste Neutralization Vessel	Titanium	5,300 <u>5,3265,27</u> 4	7 × 207 × 17
7	HDH	HDH-VSL-00002 V33001	Melter 1 Canister Decontamination Vessel	Titanium	580<u>642</u>	3 × 16
8.	HDH	HDH-VSL-00004	Melter 2 Canister Decon Vessel	<u>Titanium</u>	<u>642</u>	3 × 16
9	RLD	V35002 <u>RLD-VSL-00007</u>	Acidic Waste Vessel	Stainless Steel	16,700 18,145	13 × 19
10	RLD RLD	RLD-VSL-00008V35003 V35009	Plant Wash and Drains Vessel Decontamination Effluent Collection Vessel	Stainless Steel Stainless Steel	13,200 13,774	13 × 16 10 × 14
11	RLD	V35038 RLD-VSL-00002	Off-gas Drains Collection Vessel	Stainless Steel	280344 366	4×4
12	HFP	V31101 HFP-VSL-00001	Feed Preparation Vessel	Stainless Steel	8,800 8,445	8 × 1111 × 9.5
13	HFP	HFP-VSL-00002 V31102	HLW Melter Feed Vessel		8,800 <u>8,445</u>	8 × 11 11 × 9.5
14	HFP	HFP-VSL-00005	Feed Preparation Vessel		8,445	11 × 9.5
15	HFP	HFP-VSL-00006	HLW Melter Feed Vessel		8,445	11 × 9.5
16	HSH	HSH-TK-00001	Decontamination Tank Melter Cave 1	Stainless Steel	<u>3,718</u>	23 × 6.7
17	HSH	HSH-TK-00002	Decontamination Tank Melter Cave 2	Stainless Steel	<u>3,718</u>	23 × 6.7

	1 able	3-0	anaiyucai Laboratory Tank	Systems			
						Maximum	Approximate Dimensions
·		<u> </u> .				Total Volume	(Diameter [D] -× Height
	No.	System	Vessel Number	Description	Material	(US Ggallons)	or /Length [H/L] in feet)
	1	LAB	RLD-VSL-00164V60001a	Lab Liquid Effluent Laboratory Area Sink	Stainless Steel	12,063 3,1803,2	$11 \times 148.5 \times 8.75$
				Drain Collection Vessel		00	
ı	2	LAB	V60001bRLD-VSL-00165	Lab Liquid Effluent Hot Cell Drain	Stainless Steel	12,063 9,100	$11 \times 1416 \times 8.2$
- 1	,	·		Collection Vessel			

Table 4-7 Analytical Laboratory Sumps

Description	Location
RLD-SUMP-00041	Laboratory sump information for these sumps have been
RLD-SUMP-00042	deleted and superceded by Sump Data for LAB Facility.
	24590-LAB-PER-M-02-002 (DWP, Attachment 51,
	Appendix 11.5)
RLD-SUMP-00043A	A-B007 C5 Pump Pit
RLD-SUMP-00043B	A-B005 C5 Pump Pit
RLD-SUMP-00044	A-B006 C5 Piping Pit
RLD-SUMP-00045	A-B002 C3 Pump Pit

Table 4-8 Pretreatment Plant Sumps

<u>Table 4-8 was deleted and superceded by Sump Data for PT Facility, 24590-PTF-PER-M-02-006 (DWP, Attachment 51, Appendix 8.5) and Sump and Drain Data at 28 Ft Level of the PT Facility, 24590-PTF-PER-M-03-002 (DWP, Attachment 51, Appendix 8.5).</u>

Table 4-9 LAW Vitrification Plant Sumps

<u>Table 4-9 was deleted and superceded by LAW Facility Sump Data, 24590-LAW-PER-M -02-001 (DWP, Attachment 51, Appendix 9.8).</u>

Table 4-10 HLW Vitrification Plant Sumps

Table 4-10 was deleted and superceded by HLW Facility Sump Data, 24590-HLW-PER-M-02-001 (DWP, Attachment 51, Appendix 10.5).

Table 4-11 Secondary Containment Lin	er in Cells and Caves	s in the WTP		
			Volume of Largest Tank Plant Item	Calculated <u>Minimum</u> Secondary
•	Approximate Cell	Miscellaneous Treatment Systems,	in Cell/Cave	Containment
	Dimensions	Subsystems, or Tanks in Cell/Cave	(US	Liner Height
Cell/Cave	(L×W, in feet)	(Largest Plant Item in Bold Type)	Ggallons)	(feet)
Pretreatment Plant				
Ultimate Overflow PitP-B005 HLW Drain	Minimum secondary	containment for these cells/caves has bee	n deleted and sur	erceded by
Vessel Pit	Flooding Volume for	Below Grade and 0 Ft Level in PT Facil	ity, 24590-PTF-P	ER-M-02-005
P-B002 C2/C3 Drain Tank Room		1, Appendix 8.8)22 × 5435 × 49		
Waste Feed Receipt CellP-0102 HLW	V15009B, V12002P	WD VSL 00033, PWD VSL 00043		
Receipt/Storage/Blending Cell	23,000		•	
Waste Feed Evaporation CellP-0102A HLW	2.6<u>23.0</u>		•	
Receipt/Storage/Blending Cell	22 × 49 and 17 × 8			
Waste Feed Ultrafiltration CellP-0104	PWD-VSL 00045, P	WD-VSL-00046		·
<u>Ultrafiltration Cell</u>	4,982			•
HLW Feed Blending and Lag Storage	4.5			
CellP-0106 Feed Evaporator/Ultrafiltration	53 × 217 & 52 × 535			
<u>Cell</u>	V11020A, V11020B	, V11020C, V11020DHLP-VSL-00027A	. HLP-VSL 0002	7B.
Hot-CellP-0108 Feed Receipt Cell	PJV VSL 00002			İ
South-Process Bulge P-0108A Feed Receipt	388,000			
Cell	3.7 <u>1</u>			
Northeast Process BulgeP-0108B Feed	52 × 78 <u>72 × 52</u>			
Receipt Cell	V11001A, V11001B,	, V11002A, V11002B, V12015A, V1201	5B, V12010A <u>HI</u>	P-VSL-00022;
Northwest Process BulgeP-0108C Feed	HLP-VSL-00028, PV	<u>/P-VSL-00001</u>		
Receipt Cell	62,340		•	
Effluent Vessel CellP-0109 Acidic/Alkaline	2.1 1			
Effluent Collection Cell	52 × 94 <u>77 × 52</u>			
Cesium Ion Exchange Removal Support	V12010B, V12015C,	, V12011A, V12011B, V15009A, V1200	7, V15052,	
CellP-0111 Cesium Ion Exchange Cell				

Table 4-11 Secondary Containment Liner in Cells and Caves in the WTP						
			Volume of	Calculated		
			Largest Tank	<u>Minimum</u>		
	· .		Plant Item	Secondary		
	Approximate Cell	Miscellaneous Treatment Systems,	in Cell/Cave	Containment		
	Dimensions	Subsystems, or Tanks in Cell/Cave	<u>(US</u>	Liner-Height		
Cell/Cave	(L×W, in feet)	(Largest Plant Item in Bold Type)	Ggallons)	(feet)		
Cesium Nitrie Acid Recovery CellP-0112	V15038UFP VSL-00	001B, UFP-VSL-00002A, UFP-VSL-00	062C, PWD-VSL	-00044,		
Cesium Effluent Recovery Cell	UFP-VSL-00002B, I	PVP-SCB-00002				
Technetium Eluant Recovery Cell	73,860					
Spent Resin Collection Cell	<u>2.11</u>					
Technetium Ion Exchange Resin/Buffer	52 × 132<u>87 × 52</u>			•		
CellP-0117 Treated LAW Feed Cell	V12001A, V12001C	<u>, V12001D, V12001E, V15326, V15327<u>I</u></u>	EP-VSL-00017A	9		
Technetium Ion Exchange Column	FEP VSL 00017B, U	JFP VSL-00062A, UFP-VSL-00062B, U	FP-VSL-00001A.			
CellP-0117A Treated LAW Feed Cell	FEP SEP 00001A, F	EP-SEP-00001B	•	:		
Treated LAW Buffer StorageP-0118 Alkaline	96,900					
Effluent Collection Cell	1.9 <u>1</u>					
P-0123 Hot Cell						

ColliCorre	Approximate Cell Dimensions	Miscellaneous Treatment Systems, Subsystems, or Tanks in Cell/Cave (Largest Plant Item in Bold Type)	Volume of Largest Tank Plant Item in Cell/Cave (US	Calculated Minimum Secondary Containment Liner-Height (feet)
Cell/Cave	(L×W, in feet)	(Largest Plant Item in Boid Type)	<u>G</u> gallons)	(leet)
AW Buffer Vessel CellP-0105, P-0105A,	:			
-0105B, P-0105C South Process Areas	•			
•				•
	e e e			*
		•		
	e			
			•	
· · · · · · · · · · · · · · · · · · ·			•	
			•	
			·	
	•		•	
	•		•	
				•
				•
		•		
•	·		A	
		51-4-192	٠	

Table 4-11 Secondary Containment L Cell/Cave	Approximate Cell Dimensions (L×W, in feet)	Miscellaneous Treatment Systems, Subsystems, or Tanks in Cell/Cave (Largest Plant Item in Bold Type)	Volume of Largest Tank Plant Item in Cell/Cave (US Ggallons)	Secondary Containment Liner Height (feet)
Southeast, Southwest, and Northwest Proces	s Minimum secondar	y containment for these cells/caves has been	en deleted and su	perceded by
Areas:		or 28 Ft Level in PT Facility, 24590-PTF-I	<u> PER-M-03-001 (</u> 1	DWP Attachment
<u>P-0201.</u>	51, Appendix 8.8)6	<u>0 × 20</u>	•	
P-0201A,				
<u>P-0203.</u>	56 × 18			
P-0203A.	45 × 18			•
P-0203B,	77 × 18			÷
P-0204,	<u>89 × 18</u>			
P-0206,	<u>52 × 18</u>			*
P-0207,	<u>30 × 18</u>			
P-0208.	48 × 18			
P-0209,	<u>51-× 18</u>	• •	•	
P-0210,	<u>51 × 18</u>			
P-0212	<u>30 × 19</u>			
_ 	<u>50 × 19</u>			
	30 × 19		•	
	N/A		•	
	20 minutes of fire v	vater		•
	<u>0.61</u>		1.000	(MATA)
P-0304 Waste Feed Evaporation Room	72×54	FEP-SEP-00001A/B	4,200	TBD
		FEP-DMST-00001A/B		
		FEP-COND-00001A/1B/2A/2B/3A/3B	500	TOD
P-0320 Ion Exchange Evaporator Room	<u>54 × 36</u>	CNP-DISTC-00001	500	TBD
		TEP-DISTC-00001	4.000	TDD
P-0325 Treated LAW Evaporator Room	<u>54 × 36</u>	TLP-SEP-00001	4,200	TBD
		TLP-COND-00001	NT/A	TOD
P-0410 Utility Area Room	$(90 \times 36) +$	PWD-RK-00001/14/18/20	<u>N/A</u>	TBD

Table 4-11 Secondary Containment Lin			Volume of Largest Tank Plant Item	Calculated Minimum Secondary
	Approximate Cell	Miscellaneous Treatment Systems,	in Cell/Cave	Containment
	Dimensions	Subsystems, or Tanks in Cell/Cave	(US	Liner-Height
Cell/Cave	(L×W, in feet)	(Largest Plant Item in Bold Type)	<u>Gg</u> allons)	(feet)
	(36×18)	CXP-RK-00004		
•		FRP-RK-00013		
	:	CNP-RK-00005		
		PWD-RK-00007/46		
		HPS-RK-00009		
		PWD-RK-00008		
		CXP-RK-00005/6/7		
		RDP-RK-00014/15		
P-0415 Utility Area Room	54 × 54	PWD-RK-00005/09/12	<u>N/A</u>	TBD
		TLP-RK-00005/6/7		
2-0423 Utility Area Room	81 × 54	UFP-RK-00067/68/69/70/71/72/73	<u>N/A</u>	<u>TBD</u>
		PWD-RK-00004/06/13/17/51		
		HLP-RK-00007/8/9		
2-0425 Utility Area Room	54 × 54	PWD-RK-00002/03/11/19	<u>N/A</u>	TBD
		FRP-RK-00012/14/19		
		FEP-RK-00004/5/6/7/8		
P-0430 Process Bulge Area	45 × 36	CNP-HX-00002/3	TBD	TBD
P-0514 PCW Head Tank Room	54 × 54	SHR-TK-00009	15,00014,900	TBD
Analytical Laboratory				
offluent Collection CellA-B003 Lab Area	Minimum secondary	containment for these cells has been dele	ted and superced	led by Flooding
Sink Drain Collection Vessel Cell				· · · · · · · · · · · · · · · · · · ·

	Approximate Cell	Miscellaneous Treatment Systems,	Volume of Largest Tank <u>Plant Item</u> in Cell/Cave	Calculated Minimum Secondary Containment
	Dimensions	Subsystems, or Tanks in Cell/Cave	(US	Liner-Height
Cell/Cave	(L×W, in feet)	(Largest Plant Item in Bold Type)	<u>G</u> gallons)	(feet)
A-B004 Hot Cell Drain Collection Vessel		ility, 24590-LAB-PER-M-02-001 (DWP	<u>, Attachment 51, </u>	Appendix 11.8).
<u>Cell</u>	× 36 <u>27.25 × 13</u>			
	V60001a, V60001BI	RLD-VSL-00164		
	12,0633,200			* *.
e e	4.05.08			
	29,21 × 21			
	RLD-VSL 00165			
	9.100	·		
	4.0			
AW Vitrification Plant	1 <u>- * * X </u>			
-1860123, Melter 1 Process Cell	Minimum secondary	containment for these cells has been dele	ted and superced	ed by Flooding
-1870124, Melter 2 Process Cell		ility, 24590-LAW-PER-M-02-00348 × 3		
-188. Melter 3 Process Cell	V21001, V22101, V2			
-1890126, Effluent Cell	14,392			
-B001B, C3/C5 Drains/Sump Collection	1.4			
essel Room	48-×-38			
Cosci Room	48 × 38			
		01, V21202, V21201		
	V21002, V22301, V2			
	14,392	TEDUM, TERROUK	•	
	14,392 14,392			
	14,392 2.0 1.4		•	•
	2:01:4 1:4			
	38 × 31		•	
	V25001, V25003			
	25,130			•
	3.7 <u>4.5</u>			<u></u>

Table 4-11 Secondary Containment Lin	er-in Cells and Cave	s in the WTP		
			Volume of	Calculated
			Largest Tank	<u>Minimum</u>
			Plant Item	Secondary
	Approximate Cell	Miscellaneous Treatment Systems,	in Cell/Cave	Containment
	Dimensions	Subsystems, or Tanks in Cell/Cave	<u>(US</u>	Liner-Height
Cell/Cave	(L×W, in feet)	(Largest Plant Item in Bold Type)	Ggallons)	(feet)
L-3330218, Caustic Scrub Blowdown	$31 \times 2726 \times 31$	V22001 LVP-VSL-00001	12,191 <u>13,240</u>	3.3 <u>TBD</u>
Collection RoomBerm	<u> </u>		14,579	,
HLW Vitrification Plant	<u> </u>	i	<u></u>	1.11
H-153B014, No. 1 Tank Area Wet Process	Minimum secondary	containment for these cells/caves has been	en deleted and su	perceded by
Cell North		r HLW Facility, 24590-HLW-PER-M-02-	.003 (DWP, Atta	chment 51,
H-B014 Wet Process Cell South	Appendix 10.8).51 ×	←12<u>×</u>		
H-B021 SBS Drains Collection Cell No 1	V31001, V31002_	·		•
H-0500133, Canister Bogie Decontamination	8,800<u>344</u>			
Swab and Monitoring RoomCave	3 .02			
H-051B039A, Canister Rinse Bogie	<u></u> ★		•	
Deon/Maint Tunnel Canister Rinse				
H-059B039B, Canister Decontamination	<u>3.9</u>			
RinseCell_Tunnel	<u>* 8</u>		•	
H-0350304A, SBS Drain Collection Cell	•			
No. 1 Equipment Decontamination Area	-			
H-0270117, Wet-Process Cell (south	<u>6.1</u>			4
section)Melter Cave No. 1 (South)	36 × 235×			
H-0270117, Wet Process-Cell (north		<u>'SL-00004</u>	4.	4
section)Melter Cave No. 1 (West)	2,500<u>26</u>			
H-0310A, Equipment Decontamination Area	1.0.9			
H-106, Melter Cave No. 2 (South)	11 × 54×		i	
H-106, Melter Cave No. 2 (West)	** · · · · · · · · · · · · · · · · · ·			· · · · · · · · · · · · · · · · · · ·

Table 4-11 Secondary Containment Liner in Cells and Caves in the WTP Volume of					Calculated
		Approximate Cell	Miscellaneous Treatment Systems,	Largest Tank Plant Item in Cell/Cave	<u>Minimum</u> Secondary Containment
C	ell/Cave	Dimensions (L×W, in feet)	<u>Subsystems, or Tanks in Cell/Cave</u> (Largest Plant Item in Bold Type)	(<u>US</u> <u>G</u> gallons)	Liner-Height (feet)
H-B005, SBS Drain	ns Collection Cell No. 2	(Extry in 1000)	(Linigate Limite Leville III Dolla L) Dol	<u> </u>	(1000)
<u> </u>	<u> </u>	7.			•
		·			
•					
	. •		•	•	
			•		
		No. of the second			
	÷	·			44
		1			
				•	* .
· '					•
•					
•					÷ .
•	,			•	
$\boldsymbol{\Sigma} = \boldsymbol{\Sigma}$					
					•
					e .
				. *	
		•		•	
			51-4-197	•	

WA 7890008967, Attachment 51
Hanford Tank Waste Treatment and Immobilization Plant
102/20034

Table 4-12 Containment Buildings Summary	
Location	Approximate Dimensions (L × W × H ₃ in feet)
Pretreatment Plant	
P-0123 Pretreatment Hot Cell Containment Building	$414 \times 54 \times 46350 \times 51 \times 52$
Pretreatment Maintenance Containment Building	
PM0124 PretreatmentHot Cell Crane Maintenance Containment	(98 × 56 × 18) +
Building Area	(54 × 5 × 18) +
	(54 × 78 × 18) +
	$(18 \times 98 \times 18)54 \times 51 \times 52$
P-0121A Spend Resin Dewatering	$28 \times 18 \times 28$
P-0122A Waste Packaging Area	$26 \times 51 \times 28$
P-0123A Remote Decontamination Maintenance Cave	55 × 51 × 28
P-0124 C3 Workshop	$24 \times 24 \times 16$
P-0124A C3 Workshop	$(73 + 15 \times 15) + (16 \times 15 + 13)$
P-0125 Filter Cask Airlock	$24 \times 20 \times 28$
P-0125A Filter Cask Area	$28 \times 18 \times 28$
P-0128A MSM Repair Area	$24 \times 18 \times 28$
P-0128 Temporary Storage Room	$24 \times 17 \times 28$
P-0223 Pretreatment Air FiltrationFilter Package Maintenance Containment	$234 \times 54 \times 1940 \times 20 \times 28$
Building	
P-0335 Pretreatment Air Filter Package Containment Building	$118 \times 54 \times 42$
LAW Vitrification Plant	
L-0112 LAW LSM Gallery Containment Building	$151 \times 60 \times 24151 \times 62 \times 25$
ILAW Container Finishing Containment Building	98 × 31 × 25
L-0109B Swabbing Area Line 2	$21 \times 15 \times 24$
L-0109C Decontamination Area Line 2	$18 \times 15 \times 24$
L-0109D Inert Fill Area Line 2	55 × 15 × 24
L-0115B Swabbing Area Line 1	21 × 15 × 24
L-0115C Decontamination Area Line 1	$18 \times 15 \times 24$
,	

Table 4-12 Containment Buildings Summary

Approximate Dimensions
$(L \times W \times H_{\frac{1}{2}} \text{ in feet})$
55 × 15 × 24
19 × 18 × 14
19 × 18 × 14
$35 \times 40 \times 20$
$40 \times 35 \times 19$
16.5 × 20
16.5 × 20
16.5×20
22 x 22 x 7.5
22 x 14 x 7.5
145 × 35 × 55
$35 \times 107 \times 49 \times 145 \times 35 \times 55$
140 × 18 × 48
$10 \times 80 \times 58$
100 05 10
$(30\times27\times19)+$
_(33 × 15 × 19)
104 × 38 × 19
140 × 11 × 21
140 × 11 × 21

Table 4-12 Containment Buildings Summary

	Approximate Dimensions
Location	$(L \times W \times H_{3} \text{ in feet})$
H-0410B, H0411 H-410, H-410A, H-410B, and H-411-HLW Waste	TBD
Handling Area Containment Building	
H-0126A/B and HLW H-B028-Drum Swabbing and Monitoring Area	$52 \times 16 \times 10 + 15 \times 52 \times 10$
H-0126A/B Swabbing and Monitoring Area	52 × 16 × 10
H-B028 Cask Transfer Tunnel	$15 \times 52 \times 10$

```
Categorization of Piping
       Table 4-13
       Table 4-13 has been deleted and superceded by 24590-WTP-PER-PS-02-001, Ancillary Equipment Pipe Support Design (DWP,
  3
       Attachment 51, Appendix 7.5)
  4
                                                                  Seismic-Categories*
                                                               Seismic Category I SC-I
  6
                                                              Seismic Category II - SC-II
                                                             Scismic Category III - SC-III
                                                             Seismic Category IV SC IV
  9
 10
       Definition
       a Piping important to safety and which has a seismic safety function
 11
       a Piping important to safety, whose failure during a seismic event could prevent a Seismic Category I piping components from performing its
 12
         seismic safety function
 13
       a. Piping important to safety, but without seismic safety function
 14
       b Piping not important to safety, but which has an inventory of radioactive or hazardous material in an amount less than an important to safety
 15
          significant quantity
 16
      a Piping not important to safety and without an inventory of radioactive or hazardous material, but require seismic protection.
 17
      (I) Design Code and Analysis Methods for weight effects and thermal expansion or contraction effects
 18
      Pipe and Supports
. 19
      ASME B31.3 Code(Ref 8.1)
20
      ASME B31.3 Code (Ref 8.1)
 21
       ASME B31.3 Code (Ref 8.1)
      ASME B31.3 Code (Ref 8.1)
      (II) Analysis Methods for Seismic Loads
 25
      Pipe
      NC b
 26
      NC/F d
      NC/F-d
 28
      NC/F d
 29
 30
      Supports
      NF.º
.31
      NF.º
 32
      E.º
 33
      ₽.º
 34
       Seismie Method
 35
```

Response Spectrum Response Spectrum UBC UBC (III) Acceptance Criteria Pipe NC */B31.3 F-e F.º F.e Supports 11 NF. 12 NF-13 ₽.º 14 $\mathbf{F}^{\mathbf{B}}$ 15 16 Notes: ^a Seismic Category V (SC-V) do not have any seismic design requirements. No analysis is required. The piping shall be installed per Building Code. 17 b-NC is defined as Section NC-3650 (Analysis of Nuclear Class 2 Piping Systems) of ASME Section III Code. 18 *F is defined as Appendix F (Rules for Evaluation of Service Loadings with Level D service Limits (Faulted Condition)), as defined in ASME Section III Code. 19 4 NC/F is defined to apply Appendix F to meet ASME Section III, NC Code requirements. 20 *NF is defined as Section NF (for Pipe Supports) of ASME Section III Code. 21

	System/			3	<u>Maximum</u> <u>Volume*</u>
No.	Subsystem	Component Number	<u>Description</u>	<u>Material</u>	(gallons)
Preti	reatment Faci	<u> </u>		and the second s	
<u>l</u>	CNP	CNP-EVAP-00001	Separator Vessel	<u>Hastelloy</u>	<u>NA</u>
2	CNP	CNP-HX-00001	Cesium Evaporator Concentrate Reboiler	Stainless Steel	<u>NA</u>
3	CNP	CNP-DISTC-00001	Cesium Nitric Acid Rectifier Column	Stainless Steel	<u>NA</u>
4	CNP	CNP-HX-00002	Cesium Evaporator Primary Condenser	Stainless Steel	<u>NA</u>
<u>5</u>	CNP	CNP-HX-00003	Cesium Evaporator Secondary Condenser	Stainless Steel	<u>NA</u>
<u>6</u>	CNP	CNP-HX-00004	Cesium Evaporator After-Condenser	Stainless Steel	<u>NA</u>
7	CNP	CNP-HEPA-00006	HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>
8	FEP	FEP-SEP-00001A	Waste Feed Evaporator Separator Vessel	Stainless Steel	<u>NA</u>
9	<u>FEP</u>	FEP-SEP-00001B	Waste Feed Evaporator Separator Vessel	Stainless Steel	<u>NA</u>
<u>10</u>	FEP	FEP-RBLR-00001A	Reboiler	Stainless Steel	<u>NA</u> .
11_	<u>FEP</u>	FEP-RBLR-00001B	Reboiler	Stainless Steel	<u>NA</u>
<u>12</u>	FEP	FEP-COND-00001A	Primary Condenser	Stainless Steel	<u>NA</u>
<u>13</u>	FEP	FEP-COND-00001B	Primary Condenser	Stainless Steel	<u>NA</u>
14_	FEP	FEP-COND-00002A	Inter-Condenser	Stainless Steel	<u>NA</u>
15	FEP	FEP-COND-00002B	Inter-Condenser	Stainless Steel	<u>NA</u>
16	FEP	FEP-COND-00003A	After-Condenser	Stainless Steel	<u>NA</u>
17	<u>FEP</u>	FEP-COND-00003B	After-Condenser	Stainless Steel	<u>NA</u>
<u>18</u>	<u>PJV</u>	PJV-FLTH-00001A	Air In-Bleed Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>
19	PJV	PJV-FLTH-00001B	Air In-Bleed Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>
20	PJV	PJV-HEPA-00001A	Primary HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>
21	PJV	PJV-HEPA-00001B	Primary HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>
22	PJV	PJV-HEPA-00001C	Primary HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>
23	PJV	PJV-HEPA-00001D	Primary HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>
24	PJV	PJV-HEPA-00001E	Primary HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>
25	PJV	PJV-HEPA-00001F	Primary HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>
26	PJV	PJV-HEPA-00001G	Primary HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>
27		PJV-HEPA-00002A	Secondary HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>
		PJV-HEPA-00002B	Secondary HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	NA
		PJV-HEPA-00002C	Secondary HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	NA
	PJV	PJV-HEPA-00002D	Secondary HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	NA
		PJV-HEPA-00002E	Secondary HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	NA

No.	<u>System/</u> Subsystem	Component Number	Description	Material	<u>Maximum</u> <u>Volume*</u> (gallons)
32	PJV	PJV-HEPA-00002F	Secondary HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>
33	PJV	PJV-HEPA-00002G	Secondary HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>
34	PJV	PJV-FAN-00001A	Exhaust Fan	Stainless Steel	<u>NA</u>
35	PJV	PJV-FAN-00001B	Exhaust Fan	Stainless Steel	<u>NA</u>
36	PJV	PJV-FAN-00001C	Exhaust Fan	Stainless Steel	<u>NA</u>
37	PJV	PJV-DMST-00002A	Demister	Mesh Pad/ Stainless Steel	<u>NA</u>
38	PJV	PJV-DMST-00002B	Demister	Mesh Pad/ Stainless Steel	<u>NA</u>
39	PJV	PJV-DMST-00002C	Demister	Mesh Pad/ Stainless Steel	<u>NA</u>
40	PVP	PVP-HTR-00001A	Electric Heater	Stainless Steel	<u>NA</u>
41	PVP	PVP-HTR-00001B	Electric Heater	Stainless Steel	<u>NA</u>
<u>42</u> _	PVP	PVP-HTR-00001C	Electric Heater	Stainless Steel	<u>NA</u>
43	PVP	PVP-ABS-00001A	Carbon Bed Adsorber	TEDA/Stainless Steel	<u>NA</u>
44	PVP	PVP-ABS-00001B	Carbon Bed Adsorber	TEDA/Stainless Steel	<u>NA</u>
45	PVP	PVP-CLR-00001	After-Cooler	Stainless Steel	<u>NA</u>
46_	PVP	PVP-OXID-00001	VOC Oxidizer Unit	Stainless Steel	<u>NA</u>
47	PVP	PVP-FILT-00001A	Adsorber Outlet Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>
48	PVP	PVP-FILT-00001B	Adsorber Outlet Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>
49	PVP	PVP-HEME-00001A	HEME Filter	Packed Fiber Bed/Stainless Steel	<u>NA</u>
50.	PVP	PVP-HEME-00001B	HEME Filter	Packed Fiber Bed/Stainless Steel	<u>NA</u>
51	PVP	PVP-HEME-00001C	HEME Filter	Packed Fiber Bed/Stainless Steel	<u>NA</u>
52_	PVP	PVP-HEPA-00001A	Primary HEPA Filters	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>
53	PVP	PVP-HEPA-00001B	Primary HEPA Filters	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>
54	PVP	PVP-HEPA-00001C	Primary HEPA Filters	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>
55	PVP	PVP-HEPA-00002A	Secondary HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>
56	PVP	PVP-HEPA-00002B	Secondary HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>
57	PVP	PVP-HEPA-00002C	Secondary HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>
58	PVP	PVP-HEPA-00023	HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>
59	PVP	PVP-HEPA-00024	HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>
60	PVP	PVP-HEPA-00028	HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>
61	PVP	PVP-HEPA-00029	HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	NA
62	PVP	PVP-HEPA-00030	HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>
63	PVP	PVP-HEPA-00031	HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	NA

Table	able 4-14 WTP Facility Miscellaneous Treatment Systems and Sub-Systems					
No.	System/ Subsystem	Component Number	<u>Description</u>	Material	<u>Maximum</u> <u>Volume*</u> (gallons)	
64	PVP	PVP-HEPA-00032	HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>	
65	PVP	PVP-HEPA-00033	HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>	
<u>66</u>	<u>PVP</u>	PVP-HEPA-00034	HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>	
67	<u>PVP</u>	PVP-HEPA-00035	HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>	
68	PVP	PVP-SCB-00002	Caustic Scrubber	Metal Intalox Packing/ Stainless Steel	<u>3,237</u>	
<u>69</u> .	PVP	PVP-FAN-00001A	Exhaust Fan	Stainless Steel	<u>NA</u>	
70	<u>PVP</u>	PVP-FAN-00001B	Exhaust Fan	Stainless Steel	<u>NA</u>	
71	TLP	TLP-SEP-00001	Treated LAW Evaporator Separator Vessel	Stainless Steel	<u>NA</u>	
72	TLP	TLP-RBLR-00001	Reboiler	Stainless Steel	<u>NA</u>	
73	TLP	TLP-COND-00001	Primary Condenser	Stainless Steel	<u>NA</u>	
74	TLP	TLP-COND-00002	After-Condenser	Stainless Steel	<u>NA</u>	
75	TLP	TLP-COND-00003	Inter-Condenser	Stainless Steel	<u>NA</u>	
<u>76</u>	TLP	TLP-HEPA-00001	HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>	
LAW	Vitrification					
1	LOP	LOP-FCLR-00001	Primary Film Cooler	Stainless Steel	NA	
2	<u>LOP</u>	LOP-FCLR-00002	Secondary Film Cooler	Stainless Steel	<u>NA</u>	
3	LOP	LOP-FCLR-00003	Primary Film Cooler	Stainless Steel	<u>NA</u>	
4	LOP	LOP-FCLR-00004	Secondary Film Cooler	Stainless Steel	<u>NA</u>	
5	<u>LOP</u>	LOP-SCB-00001	Melter 1 Submerged Bed Scrubber	Ceramic Packing/Hastelloy	<u>4,948</u>	
6	LOP	LOP-SCB-00002	Melter 2 Submerged Bed Scrubber	Ceramic Packing/Hastelloy	4,948	
7	LOP	LOP-WESP-00001	Melter 1 Wet Electrostatic Precipitator	6% Molybdenum/Stainless Steel	6,347	
8	LOP	LOP-WESP-00002	Melter 2 Wet Electrostatic Precipitator	6% Molybdenum/Stainless Steel	6,347	
9	<u>LMP</u>	LMP-MLTR-00001	LAW Melter	Stainless Steel/Alloys	<u>1,860</u>	
10_	<u>LMP</u>	LMP-MLTR-00002	LAW Melter	Stainless Steel/Alloys	1,860	
11	LVP	LVP-SCB-00001	Caustic Scrubber	Metal Intalox Packing/Stainless Steel	3,237	
12	LVP	LVP-HEPA-00001A	HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>	
13	LVP	LVP-HEPA-00001B	HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>	
<u>14</u>	LVP	<u>LVP-HEPA-00002A</u>	HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>	
	LVP	LVP-HEPA-00002B	HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	NA	
16	LVP	LVP-SCO-00001	Selective Catalytic Oxidizer	Stainless Steel	<u>NA</u>	
17_	LVP	LVP-SCR-00001	Selective Catalytic Reduction Unit	Stainless Steel	<u>NA</u>	
18_	<u>LVP</u>	LVP-SCR-00002	Selective Catalytic Reduction Unit	Stainless Steel	<u>NA</u>	

No.	System/ Subsystem	Component Number	Description	Material	Maximum Volume* (gallons)
19	LVP	LVP-HTR-00001A		iless Steel	NA
20_	LVP	LVP-HTR-00001B		less Steel	NA
21	LVP	LVP-HTR-00002		iless Steel	NA NA
22	LVP	LVP-HTR-00003A		less Steel	NA
23	LVP	LVP-HTR-00003B	Electric Heater Stain	less Steel	NA
24	LVP	LVP-HX-00001		less Steel	NA
25	LVP	LVP-ADBR-00001	Adsorber Stain	less Steel	NA
26	LVP	LVP-EXHR-00001A	Melter Offgas Exhausters Stain	less Steel	NA
27_	LVP	LVP-EXHR-00001B	Melter Offgas Exhausters Stain	less Steel	<u>NA</u>
28	LVP	LVP-EXHR-00001C	Melter Offgas Exhausters Stain	less Steel	<u>NA</u>
HLW	Vitrification				
1	HMP	HMP-MLTR-00001	Melter 1 Stain	less Steel/Alloys	<u>1,078</u>
2	HMP	HMP-MLTR-00002	Melter 2 Stain	less Steel/Alloys	1,078
3	HOP	HOP-WESP-00001	Wet Electrostatic Precipitators 6% N	/lolybdenum/ Stainless Steel	<u>NA</u>
4	HOP	HOP-WESP-00002	Wet Electrostatic Precipitators 6% N	Nolybdenum/Stainless Steel	<u>NA</u>
5	HOP	HOP-SCO-00001	Offgas Organic Oxidizer Stain	less Steel	<u>NA</u>
6	<u>HOP</u>	HOP-SCO-00004	Offgas Organic Oxidizer Stain	less Steel	<u>NA</u>
7	<u>HOP</u>	HOP-SCR-00001	NOx Selective Catalytic Reducer Stain	less Steel	<u>NA</u>
8	<u>HOP</u>	HOP-SCR-00002		less Steel	<u>NA</u>
9	<u>HOP</u>	HOP-ABS-00002		um Silicate/ Stainless Steel	<u>NA</u>
10_	<u>HOP</u>	HOP-ABS-00003	Silver Mordenite Column Calci	um Silicate/ Stainless Steel	<u>NA</u>
11_	<u>HOP</u>	HOP-FCLR-00001	Film Cooler Stain	less Steel	<u>NA</u>
12_	HOP	HOP-FCLR-00002	Film Cooler Stain	less Steel	<u>NA</u>
13	<u>HOP</u>	HOP-HEPA-00001A		netic Fibrous Materials/Stainless Steel	<u>NA</u>
14	HOP	HOP-HEPA-00001B	HEPA Filter Synth	netic Fibrous Materials/Stainless Steel	<u>NA</u>
15_	HOP	HOP-HEPA-00002A	HEPA Filter Synth	netic Fibrous Materials/Stainless Steel	<u>NA</u>
16	HOP	HOP-HEPA-00002B		netic Fibrous Materials/Stainless Steel	<u>NA</u>
	HOP	HOP-HEPA-00007A	HEPA Filter Synth	netic Fibrous Materials/Stainless Steel	<u>NA</u>
18_	HOP	HOP-HEPA-00007B	HEPA Filter Synth	netic Fibrous Materials/Stainless Steel	<u>NA</u>
19	HOP	HOP-HEPA-00008A	HEPA Filter Synth	netic Fibrous Materials/Stainless Steel	<u>NA</u>
20	HOP	HOP-HEPA-00008B	HEPA Filter Synth	netic Fibrous Materials/Stainless Steel	<u>NA</u>
21	HOP	HOP-HTR-00001B		less Steel	NA

Tabl	Table 4-14 WTP Facility Miscellaneous Treatment Systems and Sub-Systems					
No.	System/ Subsystem	Component Number	Description	Material	Maximum Volume* (gallons)	
22	<u>HOP</u>	HOP-HTR-00002A	HEPA Electric Heater	Stainless Steel	NA	
23	<u>HOP</u>	HOP-HTR-00005A	HEPA Electric Heater	Stainless Steel	NA	
24	<u>HOP</u>	HOP-HTR-00005B	HEPA Electric Heater	Stainless Steel	NA	
25	<u>HOP</u>	HOP-HX-00001	Heat Exchanger	Stainless Steel	<u>NA</u>	
26	<u>HOP</u>	HOP-HX-00002	Heat Exchanger	Stainless Steel	<u>NA</u>	
27	<u>HOP</u>	HOP-HX-00003	Heat Exchanger	Stainless Steel	<u>NA</u>	
28	HOP	HOP-HX-00004	Heat Exchanger	Stainless Steel	<u>NA</u>	
29	HOP	HOP-FAN-00001A	Booster Extraction Fans	Stainless Steel	<u>NA</u>	
30	HOP	HOP-FAN-00001B	Booster Extraction Fans	Stainless Steel	<u>NA</u>	
31	<u>HOP</u>	HOP-FAN-00001C	Booster Extraction Fans	Stainless Steel	<u>NA</u>	
32	<u>HOP</u>	HOP-FAN-00008A	Stack Extraction Fans	Stainless Steel	<u>NA</u>	
33	HOP	HOP-FAN-00008B	Stack Extraction Fans	Stainless Steel	<u>NA</u>	
34	<u>HOP</u>	HOP-FAN-00008C	Stack Extraction Fans	Stainless Steel	<u>NA</u>	
35	<u>HOP</u>	HOP-FAN-00009A	Booster Extraction Fans	Stainless Steel	<u>NA</u>	
36	<u>HOP</u>	<u>HOP-FAN-00009B</u>	Booster Extraction Fans	Stainless Steel	<u>NA</u> .	
37	<u>HOP</u>	HOP-FAN-00009C	Booster Extraction Fans	Stainless Steel	<u>NA</u>	
38	<u>HOP</u>	HOP-FAN-000010A	Stack Extraction Fans	Stainless Steel	<u>NA</u>	
39	<u>HOP</u>	HOP-FAN-000010B	Stack Extraction Fans	Stainless Steel	<u>NA</u>	
40	<u>HOP</u>	HOP-FAN-000010C	Stack Extraction Fans	Stainless Steel	<u>NA</u>	
41	<u>HOP</u>	HOP-ADBR-00001A	Activated Carbon Column	Stainless Steel	<u>NA</u>	
42	<u>HOP</u>	HOP-ADBR-00001B	Activated Carbon Column	Stainless Steel	<u>NA</u>	
43	<u>HOP</u>	HOP-ADBR-00002A	Activated Carbon Column	Stainless Steel	<u>NA</u>	
44	HOP	HOP-ADBR-00002B	Activated Carbon Column	Stainless Steel	<u>NA</u>	
45	HOP	HOP-HEME-00001A	<u>HEME</u>	Packed Fiber Bed/Stainless Steel	<u>NA</u>	
46	HOP	HOP-HEME-00001B	<u>HEME</u>	Packed Fiber Bed/Stainless Steel	<u>NA</u>	
47_		HOP-HEME-00002A	<u>HEME</u>	Packed Fiber Bed/Stainless Steel	<u>NA</u>	
48_		HOP-HEME-00002B	<u>HEME</u>	Packed Fiber Bed/Stainless Steel	<u>NA</u>	
49		HOP-SCB-00001	Submerged Bed Scrubber	Ceramic Packing/Alloy 22	4,516	
50		HOP-SCB-00001	Air Ejector Induced Siphon (located on SBS)	Stainless Steel	<u>NA</u>	
51	HOP	HOP-SCB-00002	Submerged Bed Scrubber	Ceramic Packing/Alloy 22	4,516	
52_	<u>HOP</u>	HOP-SCB-00002	Air Ejector Induced Siphon (located on SBS)	Stainless Steel	<u>NA</u>	
53	PJV	PJV-HEPA-00004A	HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>	

Table	Table 4-14 WTP Facility Miscellaneous Treatment Systems and Sub-Systems					
	System/				Maximum Volume*	
No.	Subsystem	Component Number	<u>Description</u>	<u>Material</u>	(gallons)	
54	PJV	PJV-HEPA-00004B	HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>	
55_	PJV	PJV-HEPA-00005A	HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>	
56	PJV	PJV-HEPA-00005B	HEPA Filter	Synthetic Fibrous Materials/Stainless Steel	<u>NA</u>	
57	PJV	РJV-HTR-00002	Electric Heater	Stainless Steel	<u>NA</u>	
58	PJV	PJV-FAN-00002A	Pulse Jet Fans	Stainless Steel	<u>NA</u>	
50	PIV	PIV-FAN-00002B	Pulse let Fans	Stainless Steel	<u>NA</u>	